# US 85 / Maxwell St Conceptual Design 

Traffic Analysis

Colorado Department of Transportation - Region 2

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## Table of Contents

1. Introduction. ..... 6
2. Study Area ..... 6
3. Existing Traffic Conditions ..... 7
3.1 2021 Traffic Counts ..... 7
3.2 Crash Data Summary ..... 8
4. 2045 Traffic Conditions ..... 9
4.12045 Forecast Traffic Volumes ..... 9
5. Traffic Operational Analysis ..... 10
5.1 Analysis Methodology ..... 10
5.2 2021 Existing Conditions Analysis ..... 12
5.3 Traffic Signal Warrant Analysis ..... 12
5.4 2045 No-Build Traffic Conditions Analysis ..... 14
5.5 Mitigation for 2045 Traffic Conditions ..... 15
5.5.1 2045 Mitigation Analysis: Traffic Signal with Minimal Roadway Improvements ..... 15
5.5.2 2045 Mitigation Analysis: Traffic Signal with Roadway Improvements ..... 17
5.5.3 2045 Mitigation Analysis: Roundabout. ..... 19
5.5.4 2045 Mitigation Analysis: Restriping using the Existing Pavement ..... 21
5.5.5 2045 Mitigation Analysis: Right-in/ Right-out ..... 22
6. Summary ..... 25
Appendix A - 2021 Existing Conditions Traffic Counts ..... 26
Appendix B - Crash Data from 2015 to 2020 ..... 27
Appendix C - 2021 Existing Conditions Synchro Output Reports ..... 28
Appendix D - HCS7 Warrant Output Reports ..... 29
Appendix E - 2045 No-Build Traffic Conditions Synchro Output Reports ..... 30
Appendix F - 2045 Mitigation Synchro \& Sidra Output Reports ..... 31
Figures
Figure 1. Study Intersection Conditions in 2021 ..... 7
Figure 2. 2021 Existing Traffic Volumes ..... 8
Figure 3. 2045 Forecast Traffic Volumes ..... 10
Figure 4. Check of Signal Warrant 2 for 2021 Existing US 85 \& Maxwell St Conditions ..... 13
Figure 5. 2045 Traffic Signal with Minimal Roadway Improvements Intersection Configuration ..... 16
Figure 6. 2045 Traffic Signal with Roadway Improvements Intersection Configuration ..... 17
Figure 7. 2045 Roundabout Intersection Configuration ..... 20
Figure 8. 2045 Restriping Intersection Configuration ..... 21
Figure 9. 2045 Right-in/ Right-out Intersection Configuration ..... 23
Figure 10. Projected Rerouted Travel for Right-in/ Right-out Intersection Configuration ..... 24

## Tables

Table 1. Level of Service Criteria ..... 11
Table 2. 2021 Existing Conditions Level of Service and Delay ..... 12
Table 3. 2045 No-Build Conditions Level of Service and Delay ..... 15
Table 4. 2045 Traffic Signal with Minimal Roadway Improvements Level of Service and Delay ..... 16
Table 5. 2045 Traffic Signal Conditions with Roadway Improvements Level of Service and Delay ..... 18
Table 6. Traffic Signal Level of Service and Delay Comparison ..... 19
Table 7. 2045 Roundabout Conditions Level of Service and Delay ..... 20
Table 8. 2045 Restriping Conditions Level of Service and Delay ..... 22
Table 9. 2045 Right-in/ Right-out Conditions Level of Service and Delay ..... 23
Table 10. Traffic Operations Comparison of 2045 Intersection Options ..... 25
Appendix A-2021 Existing Conditions Traffic Counts
Appendix B - Crash Data from 2015 to 2020
Appendix C-2021 Existing Conditions Synchro Output Reports
Appendix D - HCS7 Warrant Output Reports
Appendix E-2045 No-Build Conditions Synchro Output Reports
Appendix F - 2045 Mitigation Synchro \& Sidra Output Reports

## 1. Introduction

This Traffic Analysis Study is supplemental to the conceptual design for intersection improvements at US 85 and Maxwell Street, in Colorado Springs, Colorado. This study will analyze the traffic operations at the US 85 and Maxwell Street intersection for existing year 2021 and horizon year 2045. This document presents current traffic volumes and estimated horizon year traffic demand in 2045. Based on analysis results of horizon year conditions, this study discusses mitigation measures to ensure acceptable level of service and quantifies the impact of mitigation measures on traffic operations.

## 2. Study Area

The study area for this traffic analysis consists of a single intersection located in Colorado Springs, Colorado in Colorado Department of Transportation (CDOT) Region 2. The study intersection is pictured on Figure 1, which also shows existing intersection lane configuration, traffic control, and posted speed limits as of 2021. The intersection is two-way stop-controlled on Maxwell Street with US 85 being freeflow. Roadways that form this intersection are briefly described below.

## US 85

US 85 is a two lane, undivided roadway classified as a Minor Arterial with a CDOT access control classification of Non-Rural Principal Highway (NR-A) within the project area. The posted speed limit is 45 mph . Both legs of US 85 have a shared left turn-thru lane and a dedicated right turn lane.

## Maxwell Street

The south leg of the intersection is a two lane, undivided roadway that provides access to the residential neighborhood between US 85 and S. Academy Boulevard. Maxwell Street does not provide direct access to South Academy Boulevard. The posted speed limit is 25 mph .

The north leg of the intersection is a local road that provides access to the Stratmoor Valley Trailhead parking lot and to industrial buildings then dead ends.


Figure 1. Study Intersection Conditions in 2021

## 3. Existing Traffic Conditions

### 3.1 2021 Traffic Counts

Turning movement counts were collected from 6:00 a.m. to 6:00 p.m. on Tuesday, November 16, 2021, by All Traffic Data Services at the intersection of US 85 and Maxwell Street. There was no inclement weather when the data was collected, and schools were in session. Traffic counts were collected 20 months into the COVID-19 pandemic. Vehicle travel patterns and number of vehicles traveling in November 2021 may be different than those pre-COVID-19. However, it is assumed that it will be many years before travel patterns return to pre-pandemic conditions, if ever, so the traffic data is considered representative of a typical weekday. Peak hours were determined by summing traffic volumes for four consecutive 15 -minute periods for all movements at the intersection, and then selecting the largest onehour sum of vehicles during the morning and evening hours. The a.m. peak hour was found to be 7:15 to 8:15 a.m. and the p.m. peak hour was found to be 3:30 to $4: 30$ p.m. 2021 existing conditions traffic counts for these peak hours are pictured on Figure 2. Traffic count data is included in Appendix A.


Figure 2. 2021 Existing Traffic Volumes

Heavy vehicle percentages were calculated from the turning movement counts and are the following:

- Northbound Maxwell Street - 4.2\%
- Southbound Maxwell Street - 0.0\%
- Eastbound US 85-0.3\%
- Westbound US 85-1.1\%

Data from the CDOT Online Transportation Information System (OTIS) online platform shows that the truck percentage on US 85 is $1.8 \%$ at Station ID 103648 which is located just west of the US 85 and Maxwell Street intersection.

### 3.2 Crash Data Summary

CDOT provided five years of crash data from July 2015 to June 2020 at the intersection of US 85 and Maxwell Street. There was a total of thirteen (13) crashes reported at the intersection. These crashes are summarized below. The full crash data records are included in Appendix B.

## Summary of crashes by year

- 2015 (July to December): 2 crashes
- 2016: 2 crashes
- 2017: 0 crashes
- 2018: 4 crashes
- 2019: 2 crashes
- 2020 (January to June): 3 crashes


## Summary of severity of crash

- Property Damage Only (PDO): 6 crashes ( $46 \%$ )
- Injury: 7 crashes ( $54 \%$ ), 9 people injured
- Fatal: 0 crashes ( $0 \%$ )


## Summary of type of crash

- Broadside: 8 crashes (60\%)
- Sideswipe, Same Direction: 1 crash (8\%)
- Approach: 1 crash (8\%)
- Rear-End: 1 crash (8\%)
- Guardrail: 1 crash ( $8 \%$ )
- Bicycle: 1 crash (8\%)


## Summary of weather conditions

- Dry: 11 crashes ( $84 \%$ )
- Icy: 1 crash (8\%)
- Snowy: 1 crash (8\%)


## Summary of lighting conditions

- Daylight: 10 crashes (77\%)
- Dark-Unlighted: 2 crashes (15\%)
- Dark-Lighted: 1 crash (8\%)

Three (3) crashes involved a vehicle turning right from eastbound US 85 onto south Maxwell Street and crashing into a vehicle stopped at the intersection. Six (6) crashes involved conflicts with a vehicle on Maxwell Street either trying to go straight through the intersection or turning left onto US 85. One (1) crash involved a bicycle on Maxwell Street trying to cross US 85.

## 4. 2045 Traffic Conditions

### 4.12045 Forecast Traffic Volumes

2045 traffic volumes were calculated by applying an annual growth rate to the 2021 existing traffic counts. CDOT Online Transportation Information System (OTIS) online platform shows that the 20-year growth factor on US 85 is 1.58 at Station ID 103648 which is located just west of the US 85 and Maxwell Street intersection. This growth factor calculates to an annual growth rate of $2.3 \%$. This growth rate on US 85 makes sense today because as $I-25$ is reaching capacity, vehicles are starting to look for alternative routes including US 85 . However, a growth of $2.3 \%$ every year for the next 24 years is unlikely. It is assumed based on roadway characteristics that US 85 has a capacity of 1000 vehicles per hour per lane. US 85 may see the $2.3 \%$ growth for the next few years, but as US 85 reaches capacity, the growth rate
will decrease. Also, it is assumed that improvements to $\mathrm{I}-25$ will occur within 24 years which will increase the capacity on the freeway. Because of these factors, a $2.0 \%$ annual growth rate was applied to represent an average growth over the 24 -year analysis period.

The north leg provides access to a Stratmoor Valley Trailhead parking lot and a built-out industrial area. Maxwell Street dead-ends and does not connect to any other roadways to the north. The south leg of Maxwell Street provides access to an established residential area. The residential area is built-out with minimal space for additional development. Maxwell Street ends just north of Academy Boulevard and does not provide direct access. However, Coventry Drive does provide the only access to the neighborhood from Academy Boulevard at the south via a right-out/right-in only T-intersection and intersects with Maxwell Street approximately 1000 feet north. Maxwell Street does not provide a convenient pass-thru route. For these reasons, it is unlikely that Maxwell Street will see much growth. Instead, an annual growth rate of $0.5 \%$ was applied for all movements to and from Maxwell Street. The annual growth rate of $2.0 \%$ was applied to thru traffic on US 85 only. Forecast 2045 peak hour traffic volumes are pictured on Figure 3.


Figure 3. 2045 Forecast Traffic Volumes

## 5. Traffic Operational Analysis

### 5.1 Analysis Methodology

Traffic operations for stop-control and signal-control at the study intersection were analyzed using Synchro 11, which implements methodologies of the Highway Capacity Manual 6th Edition published in 2016 by the Transportation Research Board. Synchro determines vehicle delay by movement, approach, and for the intersection overall to determine level of service based on roadway geometric data, volume data, type of traffic control, and signal timing parameters if an intersection is signalized.

Traffic operations for the roundabout concept were analyzed using Sidra Intersection 9.0 Plus software (Sidra) which also implements methodologies of the Highway Capacity Manual 6th Edition.

Additionally, a signal warrant analysis was also conducted using Highway Capacity Software 7 (HCS7) developed by McTrans Center at the University of Florida to check if signal warrants are met at the intersection.

Level of service (LOS) is categorized by letter grades ranging from A to F. LOS A represents the best traffic conditions with minimal congestion and vehicle delay, and LOS F represents the worst traffic conditions with potentially extreme congestion and typically high vehicle delay. Criteria for assigning LOS differ based on whether an intersection is signalized or unsignalized as shown in Table 1. For the purposes of analysis, the threshold for acceptable LOS is D or better on each approach representing under-saturated conditions.

Table 1. Level of Service Criteria

| Level of Service | Unsignalized Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Signalized Delay <br> $(\mathrm{s} / \mathrm{veh})$ |
| :---: | :---: | :---: |
| A | $\leq 10$ | $\leq 10$ |
| B | $>10-15$ | $>10-20$ |
| C | $>15-25$ | $>20-35$ |
| D | $>25-35$ | $>35-55$ |
| E | $>35-50$ | $>55-80$ |
| F | $>50$ | $>80$ |

Source: Highway Capacity Manual 6th Edition, 2016, Transportation Research Board

To analyze traffic operations at US 85 and Maxwell Street intersection, the following assumptions were made:

1. Peak hour factors (PHFs) were calculated from the 2021 traffic counts and applied to both existing and future year conditions.
2. Heavy vehicle percentages were assumed to be the following for both existing and future year conditions (Synchro does not allow decimal inputs):
a. Northbound Maxwell Street - 4\% ( $4.2 \%$ calculated from 2021 traffic counts, rounded down)
b. Southbound Maxwell Street - 1\% (0\% calculated from 2021 traffic counts, adjusted to 1\%)
c. Eastbound US $85-2 \%$ ( $1.8 \%$ taken from OTIS, rounded up)
d. Westbound US $85-2 \%$ ( $1.8 \%$ taken from OTIS, rounded up)
3. Cycle lengths were set at 90 seconds for each scenario analyzed that includes traffic signalization.
4. Synchro created optimized splits based on turning movement volumes for each peak hour for each scenario analyzed that includes traffic signalization.
5. Signal controllers are actuated-uncoordinated with 3 seconds yellow time and 2 seconds all-red time.
6. All other software values not explicitly mentioned remain at default values.

### 5.2 2021 Existing Conditions Analysis

Analysis of existing conditions was done using 2021 traffic volumes pictured on Figure 2 using the intersection lane geometry and traffic control pictured on Figure 1. For 2021 existing conditions, LOS, and vehicle delay are summarized in Table 2. Synchro reports for 2021 existing conditions are included in Appendix C.

In 2021 with stop-control on the northbound and southbound approaches only, the US 85 and Maxwell Street intersection operates overall at LOS A during both the a.m. and p.m. peak hours. However, the northbound and southbound approaches operate at LOS F and LOS C during both the a.m. and p.m. peak hours, respectively.

Table 2. 2021 Existing Conditions Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> $(\mathrm{s} /$ /veh $)$ | Level of <br> Service | Delay <br> (s/veh) |
| Overall | A | 9.0 | A | 7.2 |
| Northbound <br> MaxwELL sT | F | 65.7 | F | 68.5 |
| Southbound <br> MAxwELL sT | C | 17.8 | C | 22.2 |
| Eastbound <br> Us 85 | A | 9.1 | A | 8.5 |
| Westbound <br> Us 85 | A | 8.1 | A | 9.3 |

### 5.3 Traffic Signal Warrant Analysis

Given that the US 85 and Maxwell Street intersection northbound approach operates poorly under existing conditions with LOS F, the intersection was evaluated on whether it meets warrant criteria for traffic signal control. Traffic signal control warrant methodologies described in the Manual on Uniform Traffic Control Devices, 2012 Revision (MUTCD), Chapter 4C were used to evaluate the intersection. HCS7 Warrants Version 7.1 software was also used to verify the results. The software also uses the methods described in Chapter 4C of the MUTCD.

Warrants 1 and 2, which are applicable to the intersection, were met under 2021 existing conditions. All warrants and the check process are described below. The HCS7 Warrant output reports are included in Appendix D.

## Warrant 1, "Eight-Hour Vehicular Volume"

This signal warrant addresses situations where large intersecting traffic volumes occur at intersections or high major street traffic volume causes high delay to minor street traffic. Because 85th percentile speed exceeds 40 mph on US 85 (the major street), lower volume thresholds are used to check this signal warrant. Eleven hourly volumes satisfy criteria for Condition B-Interruption of Continuous Traffic for 2021 conditions and, therefore, Warrant 1 is met for 2021 existing conditions. (Refer to MUTCD Section 4C. 02 for additional details about this warrant.)

## Warrant 2, "Four-Hour Vehicular Volume"

This signal warrant addresses situations where the volume of intersecting traffic at intersections is the main reason to consider a traffic signal. Because 85th percentile speed exceeds 40 mph on US 85 (the major street), lower volume thresholds shown on MUTCD Figure 4C-2 are used to check this warrant instead of

MUTCD Figure 4C-1. Figure 4 show 2021 volumes plotted against the threshold for Warrant 2. Eight hourly volumes plot above the threshold for one lane approaches on the major street and one lane approach on the minor street and, therefore, Warrant 2 is met for 2021 existing conditions. (Refer to MUTCD Section 4 C .03 for additional details about this warrant.)


Figure 4. Check of Signal Warrant 2 for 2021 Existing US 85 \& Maxwell St Conditions

## Warrant 3, "Peak Hour"

This signal warrant addresses the condition where minor-street traffic experiences high delay trying to cross or access the major street and when large fluctuations in traffic volume occur over a short time. The MUTCD states that this signal warrant shall be applied only in unusual cases, such as office complexes, manufacturing plants, industrial complexes, or high-occupancy vehicle facilities that attract or discharge large numbers of vehicles over a short time. The intersection does not serve any of these facilities, therefore Warrant 3 does not apply even though HCS7 software states that the intersection meets criteria. (Refer to MUTCD Section 4C. 04 for additional details about this warrant.)

## Warrant 4, "Pedestrian Volume"

This signal warrant addresses the condition where high major street traffic volume causes pedestrians to experience high delay crossing the major street. Pedestrians and bicyclists were observed at the intersection but not enough to meet criteria and warrant signalization at the intersection. (Refer to MUTCD Section 4C. 05 for additional details about this warrant.)

## Warrant 5, "School Crossing"

This signal warrant addresses the condition where safety of school children crossing the major street is of concern. There are no schools in the immediate vicinity which would utilize the intersection of US 85 and Maxwell Street, so this warrant is not considered to be applicable. (Refer to MUTCD Section 4C. 06 for additional details about this warrant.)

## Warrant 6, "Coordinated Signal System"

This signal warrant addresses situations where traffic signals may be needed to maintain proper platooning of vehicles within a coordinated signal system. The US 85 and Maxwell Street intersection is not part of a coordinated signalized corridor, so this warrant is not applicable. (Refer to MUTCD Section 4C. 07 for additional details about this warrant.)

## Warrant 7, "Crash Experience"

This signal warrant addresses a situation where crashes are severe and/or occur frequently and a traffic signal may be able to reduce both frequency and severity of crashes. Crash data indicates that approximately half the reported crashes occurred between cross traffic (north/south vehicle crashes with an east/west vehicle). Signalization of the intersection may have prevented these crashes by providing north/south vehicles a gap in opposing traffic to safely make their desired movements. However, the reported crash data fails to meet all criteria required of this warrant. (Refer to MUTCD Section 4C. 08 for additional details about this warrant.)

## Warrant 8, "Roadway Network"

This signal warrant addresses the condition where traffic flow is not well organized on a road network, and it is desirable to encourage concentration of traffic flow at the intersection of two major routes. Maxwell Road is not considered a major roadway, so this warrant is not applicable. (Refer to MUTCD Section 4C. 09 for additional details about this warrant.)

## Warrant 9, "Intersection Near Grade Crossing"

This signal warrant addresses situations where an at-grade rail crossing exists on or near an intersection approach that is controlled by a stop or yield sign. There is no railroad crossing in the vicinity of the US 85 and Maxwell Street intersection, so this warrant is not applicable. (Refer to MUTCD Section 4C. 10 for additional details about this warrant.)

### 5.4 2045 No-Build Traffic Conditions Analysis

Analysis of unmitigated 2045 traffic conditions was done using 2045 forecast traffic volumes pictured on Figure 3 assuming existing conditions lane geometry and two-way stop-control remain in place at the intersection of US 85 and Maxwell Street. This represents a "No-Build" horizon year scenario in which no intersection improvements are implemented. This is a baseline to compare mitigation options against. 2045 No-Build traffic conditions LOS and vehicle delay are summarized in Table 3. Synchro reports for 2045 No-Build traffic conditions are included in Appendix E.

Overall, the intersection is forecast to operate at LOS E and LOS F for 2045 a.m. and p.m. peak hours, respectively. The northbound movement is forecast to experience significant delay in both peak hours. The southbound movement is forecast to operate at LOS E and F in the a.m. and p.m. peak hours, respectively.

Table 3. 2045 No-Build Conditions Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> (s/veh) | Level of <br> Service | Delay <br> (s/veh) |
| Overall | F | 111.6 | F | 124.2 |
| Northbound <br> MAXwELL st | F | $>300$ | F | $>300$ |
| Southbound <br> mAxweLL st | F | 108.1 | F | 165.3 |
| Eastbound Left-Thru <br> Us 85 | B | 10.9 | A | 9.8 |
| Eastbound Right <br> us 85 | A | 0.0 | A | 0.0 |
| Westbound Left-Thru <br> us 85 | A | 8.7 | B | 11.0 |
| Westbound Right <br> Us 85 | A | 0.0 | A | 0.0 |

### 5.5 Mitigation for 2045 Traffic Conditions

### 5.5.1 2045 Mitigation Analysis: Traffic Signal with Minimal Roadway Improvements

2045 Mitigation Analysis: Traffic Signal with Minimal Roadway Improvements changes the intersection control to traffic signal control while trying to maintain the intersection within the existing pavement footprint. The lane configurations on the US 85 approaches were modified to provide a dedicated left turn lane and a shared thru-right lane for both eastbound and westbound approaches. It is undesirable to have a shared left-thru lane at signalized intersections with large opposing volumes as operations deteriorate for the thru movements if the lane is blocked by a vehicle waiting to turn left. The northbound approach provides a dedicated left turn lane and a shared thru-right turn lane. The width of the existing pavement on the south leg should allow for the additional left turn lane without needing to widen the leg. The southbound approach remains the same as existing with one shared left-thru-right turn lane. Even though the goal of this scenario is to provide an alternative that can be constructed within the existing pavement footprint, this configuration may require some widening of both legs of US 85 to provide adequate left turn lane lengths that meet CDOT design standards.

The signal timing includes a protected+permissive phase for each the eastbound and westbound left turn movements. Since the roadway alignment is on a curve, sight distance should be evaluated if this configuration continues to design. If further evaluation determines that the sight distance is inadequate, then the eastbound and westbound movements should have a left turn protected only phase which will modify forecast traffic operations.

The intersection lane configuration is depicted in Figure 5. 2045 Traffic Signal conditions LOS and vehicle delay are summarized in Table 4. Synchro reports for 2045 Traffic Signal conditions are included in Appendix F.

The intersection is forecast to operate at LOS C overall for both the a.m. and p.m. peak hours. All movements are forecast to operate at LOS D or better.


Figure 5. 2045 Traffic Signal with Minimal Roadway Improvements Intersection Configuration

Table 4. 2045 Traffic Signal with Minimal Roadway Improvements Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> (s/veh) | Level of <br> Service | Delay <br> (s/veh) |
| Overall | C | 33.2 | C | 34.6 |
| Northbound Left <br> maxwELL s s | C | 33.4 | C | 32.2 |
| Northbound Thru-Right <br> MAXwELL sT | C | 28.5 | C | 30.1 |
| Southbound <br> maxwELL s s | C | 28.0 | C | 30.1 |
| Eastbound Left <br> Us 85 | C | 22.2 | B | 11.8 |
| Eastbound Thru-Right <br> Us 85 | B | 10.9 | D | 51.0 |
| Westbound Left <br> Us 85 | A | 8.0 | C | 22.7 |
| Westbound Thru-Right <br> Us 85 | D | 45.3 | B | 16.1 |

### 5.5.2 2045 Mitigation Analysis: Traffic Signal with Roadway Improvements

2045 Mitigation Analysis: Traffic Signal with Roadway Improvements changes the intersection control to traffic signal control and includes additional dedicated turn lanes. The lane configurations on the US 85 approaches were modified to provide a dedicated left turn lane, thru lane and right turn lane for the eastbound approach and a dedicated left turn lane with a shared thru-right lane for the westbound approach. The northbound approach provides a dedicated left turn lane and a shared thru-right turn lane. The width of the existing pavement on the south leg should allow for the additional left turn lane without needing to widen the leg. The southbound approach remains the same as existing with one shared left-thru-right turn lane. Widening of the west leg of the intersection would be required to add the additional left turn lane. The east leg may require widening to provide an adequate left turn lane length that meets CDOT design standards

The signal timing includes a protected+permissive phase for each the eastbound and westbound left turn movements. Since the roadway alignment is on a curve, sight distance should be evaluated if this configuration continues to design. If further evaluation determines that the sight distance is inadequate, then the eastbound and westbound movements should have a left turn protected only phase which will modify forecast traffic operations.

The intersection lane configuration is depicted in Figure 6. 2045 Traffic Signal with Roadway Improvements conditions LOS and vehicle delay are summarized in Table 5. Synchro reports for 2045 Traffic Signal with Roadway Improvements conditions are included in Appendix F.

The intersection is forecast to operate at LOS C overall for the a.m. and p.m. peak hours. All movements are forecast to operate at LOS D or better.


Figure 6. 2045 Traffic Signal with Roadway Improvements Intersection Configuration

Table 5. 2045 Traffic Signal Conditions with Roadway Improvements Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> (s/veh) | Level of <br> Service | Delay <br> (s/veh) |
| Overall | C | 32.8 | C | 20.8 |
| Northbound Left <br> maxwELL st | C | 33.4 | C | 26.7 |
| Northbound Thru-Right <br> MAXWELL sT | C | 28.5 | C | 25.1 |
| Southbound <br> MAxwELL s | C | 28.0 | C | 25.1 |
| Eastbound Left <br> us 85 | C | 22.2 | B | 13.2 |
| Eastbound Thru <br> Us 85 | B | 10.0 | C | 24.1 |
| Eastbound Right <br> Us 85 | A | 7.6 | A | 9.4 |
| Westbound Left <br> Us 85 | A | 7.4 | B | 15.7 |
| Westbound Thru-Right <br> Us 85 | D | 45.3 | B | 18.7 |

Table 6 shows a comparison of the forecast operations between the two signalized options analyzed. Providing the additional right turn lane eastbound US 85 improves the overall intersection operations and operations for the eastbound movement during the p.m. peak hour. Operations during the a.m. peak hour for all movements are similar for both options.

Table 6. Traffic Signal Level of Service and Delay Comparison

| A.M. Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Min Road Improvements |  | Road Improvements |  |
|  | Level of <br> Service | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Level of <br> Service | Delay <br> $(\mathrm{s} /$ veh $)$ |
|  | C | 33.2 | C | 32.8 |
| Northbound <br> MAXWELL sT | C | 32.3 | C | 32.3 |
| Southbound <br> MAXWELL ST | C | 28.0 | C | 28.0 |
| Eastbound <br> Us 85 | B | 11.1 | A | 9.9 |
| Westbound <br> Us 85 | D | 44.5 | D | 44.5 |


| P.M. Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Approach | Min Road Improvements |  | Road Improvements |  |
|  | Level of Service | Delay (s/veh) | Level of Service | Delay (s/veh) |
| Overall | C | 34.6 | C | 20.8 |
| Northbound MAXWELL ST | C | 31.5 | C | 26.2 |
| Southbound MAXWELL ST | C | 30.1 | C | 25.1 |
| Eastbound US 85 | D | 50.4 | C | 21.5 |
| Westbound US 85 | B | 16.4 | B | 18.6 |

### 5.5.3 2045 Mitigation Analysis: Roundabout

2045 Mitigation Analysis: Roundabout changes the intersection to a roundabout with single lane approaches for all legs. The intersection lane configuration is depicted in Figure 7. 2045 Roundabout conditions LOS and vehicle delay are summarized in Table 7. Sidra reports for 2045 Roundabout conditions are included in Appendix F.

The roundabout is forecast to operate at LOS E and LOS C for the a.m. and p.m. peak hours, respectively. In the a.m. peak hour, all approaches are forecast to operate at LOS A or B except the westbound movement which is forecast at LOS F. This is due to the large northbound left turn movement hindering the westbound movement from entering the roundabout. In the p.m. peak hour, all approaches are forecast to operate at LOS C or better.


Figure 7. 2045 Roundabout Intersection Configuration

Table 7. 2045 Roundabout Conditions Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> (s/veh) | Level of <br> Service | Delay <br> (s/veh) |
| Overall | E | 38.3 | C | 19.7 |
| Northbound <br> MAXwELL st | A | 7.7 | B | 12.7 |
| Southbound <br> MAxwELL sT | B | 11.4 | A | 9.6 |
| Eastbound <br> Us 85 | A | 7.4 | C | 23.6 |
| Westbound <br> Us 85 | F | 60.1 | C | 17.0 |

To get the roundabout to operate at acceptable LOS in the a.m. peak hour (LOS A overall and for all movements), the east leg would need to be a two-lane approach with a two-lane exit on the west leg. This would require widening US 85 beyond the intersection. The two lanes exiting the roundabout on the west leg would then have to merge back into one lane to match existing US 85 . This option will require additional ROW beyond the intersection and widening of the bridge to the west over I-25. Additionally, merging traffic on a curve is not ideal.

### 5.5.4 2045 Mitigation Analysis: Restriping using the Existing Pavement

2045 Mitigation Analysis: Restriping using the Existing Pavement reconfigures the intersection lanes without the need for widening the existing roadways. Eastbound US 85 and southbound Maxwell Street remains the same lane configuration as existing. Westbound US 85 would get reconfigured from a shared left turn-thru lane with a right turn lane to a left turn lane with a shared thru-right turn lane. The existing pavement width on the south leg should allow for northbound Maxwell Street to get restriped to provide a left turn lane and a shared thru-right turn lane. The intersection would remain two-way stop-controlled on Maxwell Street with US 85 being free-flow.

The intersection lane configuration is depicted in Figure 8. 2045 Restriping conditions LOS and vehicle delay are summarized in Table 8. Synchro reports for 2045 Restriping conditions are included in Appendix F.

The intersection is forecast to operate overall at LOS F for both the a.m. and p.m. peak hours. The new lane configuration fails to improve the operations for the northbound left turn movement and the southbound movement as they are reporting LOS F for both a.m. and p.m. peak hours.


Figure 8. 2045 Restriping Intersection Configuration

Table 8. 2045 Restriping Conditions Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> $(\mathrm{s} /$ veh $)$ | Level of <br> Service | Delay <br> (s/veh) |
| Overall | F | 72.7 | F | 76.8 |
| Northbound Left <br> MAXWELL sT | F | $>300$ | F | $>300$ |
| Northbound Thru-Right <br> MAXwELL st | D | 33.4 | D | 25.3 |
| Southbound <br> MAXwELL sT | F | 103.1 | F | 156.7 |
| Eastbound Left-Thru <br> Us 85 | B | 10.9 | A | 9.8 |
| Eastbound Right <br> Us 85 | A | 0.0 | A | 0.0 |
| Westbound Left <br> Us 85 | A | 8.7 | B | 11.0 |
| Westbound Thru-Right <br> Us 85 | A | 0.0 | A | 0.0 |

### 5.5.5 2045 Mitigation Analysis: Right-in/ Right-out

2045 Mitigation Analysis: Right-in/ Right-out reconfigures both the north and south leg of the intersection to be right-out movements only. Median islands will need to be constructed to fully restrict the movements. The left turn movement is restricted from westbound US 85 while maintaining the thru and right turn lanes. Left turning vehicles will have to access the residential area from the south at Coventry Drive via Academy Boulevard. Eastbound US 85 remains as existing with a shared left-thru lane and a right turn lane. Due to the existing roadway network, there is not a convenient alternative route to access the north property if traveling south on US 85 if the left turn movement is restricted. It is recommended that the left turn movement remain since the projected traffic volumes making this left turn from US 85 are low (5 a.m. and 10 p.m. peak hour vehicles) and because vehicles would have to travel an additional 4.5 miles to access the property if the left turn is restricted.

The intersection lane configuration is depicted in Figure 9. 2045 Right-in/ Right-out conditions LOS and vehicle delay are summarized in Table 9. Synchro reports for 2045 Right-in/ Right-out conditions are included in Appendix F.

With the restriction of the left turn movements at the intersection, traffic will be forced to reroute through other intersections in the area. This may cause operations at these intersections to deteriorate. The anticipated routes vehicles will travel once left turn movements are restricted is depicted in Figure 10.


Figure 9. 2045 Right-in/ Right-out Intersection Configuration

Table 9. 2045 Right-in/ Right-out Conditions Level of Service and Delay

| Approach | A.M. Peak |  | P.M. Peak |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Level of <br> Service | Delay <br> (s/veh) | Level of <br> Service | Delay <br> (s/veh) |
| Overall | A | 0.7 | A | 1.2 |
| Northbound Right <br> MAxweLL st | B | 11.6 | C | 18.0 |
| Southbound Right <br> MAxweLL st | C | 21.3 | C | 17.9 |
| Eastbound Left-Thru <br> us 85 | B | 11.0 | A | 9.8 |
| Eastbound Right <br> us 85 | A | 0.0 | A | 0.0 |
| Westbound Thru <br> us 85 | A | 0.0 | A | 0.0 |
| Westbound Right <br> us 85 | A | 0.0 | A | 0.0 |



Figure 10. Projected Rerouted Travel for Right-in/ Right-out Intersection Configuration

The intersection is forecast to operate overall at LOS A for both the a.m. and p.m. peak hours with all movements forecast to operate at LOS C or better.

With the rerouting of traffic that will happen with restricting left turn movements, the intersections of US 85/Academy Boulevard, I-25 ramps/Academy Boulevard, Academy Boulevard/Venetucci Boulevard, Academy Boulevard/ B Street, and US $85 /$ B Street as well as the weaving movement between Coventry Drive and $\mathrm{I}-25$ Northbound On-ramp will all see an increase in traffic. The intersections and the weaving movement should be further evaluated to determine the projected effects on traffic operations as a result of the rerouted traffic.

## 6. Summary

Table 10 summarizes the 2045 forecasted levels of service for each intersection configuration discussed in this report. Both the No-Build and Restriping options, which maintains the two-way stop-control at the intersection, is forecast to operate at LOS F overall and for both northbound and southbound approaches. The Roundabout option is forecast to operate during the a.m. peak hour at LOS E overall and LOS F in the westbound direction on US 85. Both Traffic Signal options and the Right-in/ Right-out options are forecast to operate at acceptable LOS overall and for each approach during both a.m. and p.m. peak hours.

Table 10. Traffic Operations Comparison of 2045 Intersection Options

|  | No- Build |  | Traffic Signal with Minimal Road Improvements |  | Traffic Signal with Road Improvements |  | Roundabout |  | Restriping |  | Right-in/ <br> Right- out |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { A.M. } \\ & \text { LOS } \end{aligned}$ | $\begin{aligned} & \text { P.M. } \\ & \text { LOS } \end{aligned}$ |
| Overall | F | F | c | C | C | C | E | C | F | F | A | A |
| Northbound MAXWELL ST | F | F | C | C | C | C | A | B | F | F | B | C |
| Southbound MAXWELL ST | F | F | C | C | C | C | B | A | F | F | C | C |
| Eastbound <br> US 85 | A | A | B | D | A | C | A | C | A | A | A | A |
| $\begin{aligned} & \text { Westbound } \\ & \text { us } 85 \end{aligned}$ | A | A | D | B | D | B | F | C | A | A | A | A |

## Appendix A - 2021 Existing Conditions Traffic Counts

1 MAXWELL ST \& US85 AM
Tuesday, November 16, 2021

## Poak Hour

03:30 PM - 04:30 PM
Peak 15-Minutes
03:45 PM - 04:00 PM
Traffic Counts - All Vehicles

| Trafic Count - All Vehicles | US85 |  |  |  |  | US85 |  |  |  |  | MAXWELL ST |  |  |  |  | MAXWELL ST |  |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  |  |  |
| Time | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR |  |  |
| 6:00 AM | 0 | 0 | 16 | 1 | 0 | 0 | 1 | 58 | 0 | 0 | 0 | 10 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 91 | 470 |
| 6:15 AM | 0 | 0 | 27 | 3 | 0 | 0 | 1 | 59 | 1 | 0 | 0 | 11 | 0 | 3 | 0 | 0 | 2 | 0 | 0 | 0 | 107 | 573 |
| 6:30 AM | 0 | 1 | 28 | 2 | 0 | 0 | 2 | 64 | 1 | 0 | 0 | 11 | 0 | 7 | 0 | 0 | 1 | 0 | 0 | 0 | 117 | 738 |
| 6:45 AM | 0 | 2 | 39 | 3 | 0 | 0 | 1 | 79 | 3 | 0 | 0 | 20 | 0 | 5 | 0 | 0 | 2 | 0 | 1 | 0 | 155 | 897 |
| 7:00 AM | 0 | 0 | 53 | 5 | 0 | 0 | 2 | 96 | 1 | 0 | 0 | 22 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 194 | 1,039 |
| 7:15 AM | 0 | 0 | 52 | 12 | 0 | 0 | 2 | 175 | 1 | 0 | 0 | 25 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 272 | 1,058 |
| 7:30 AM | 0 | 1 | 57 | 14 | 0 | 0 | 2 | 161 | 0 | 0 | 0 | 35 | 0 | 4 | 0 | 0 | 1 | 0 | 1 | 0 | 276 | 1,011 |
| 7:45 AM | 0 | 1 | 75 | 12 | 0 | 0 | 3 | 170 | 1 | 0 | 0 | 32 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 297 | 928 |
| 8:00 AM | 0 | 2 | 75 | 17 | 0 | 0 | 5 | 81 | 2 | 0 | 0 | 22 | 1 | 6 | 0 | 0 | 0 | 0 | 2 | 0 | 213 | 809 |
| 8:15 AM | 0 | 1 | 55 | 18 | 0 | 0 | 4 | 111 | 2 | 0 | 0 | 25 | 1 | 6 | 0 | 0 | 0 | 0 | 2 | 0 | 225 | 750 |
| 8:30 AM | 0 | 6 | 45 | 15 | 0 | 0 | 2 | 89 | 2 | 0 | 0 | 20 | 0 | 7 | 0 | 0 | 2 | 2 | 3 | 0 | 193 | 699 |
| 8:45 AM | 0 | 3 | 46 | 7 | 0 | 0 | 5 | 92 | 1 | 0 | 0 | 17 | 0 | 5 | 0 | 0 | 0 | 0 | 2 | 0 | 178 | 653 |
| 9:00 AM | 0 | 1 | 37 | 11 | 0 | 0 | 6 | 72 | 4 | 0 | 0 | 17 | 0 | 3 | 0 | 0 | 1 | 2 | 0 | 0 | 154 | 644 |
| 9:15 AM | 0 | 0 | 53 | 13 | 0 | 0 | 2 | 80 | 3 | 0 | 0 | 14 | 0 | 5 | 0 | 0 | 1 | 0 | 3 | 0 | 174 | 632 |
| 9:30 AM | 1 | 0 | 58 | 13 | 0 | 0 | 1 | 58 | 2 | 0 | 0 | 10 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 0 | 147 | 621 |
| 9:45 AM | 0 | 1 | 48 | 10 | 0 | 0 | 1 | 83 | 1 | 0 | 0 | 18 | 0 | 4 | 0 | 0 | 1 | 0 | 2 | 0 | 169 | 613 |
| 10:00 AM | 0 | 1 | 59 | 6 | 0 | 0 | 3 | 53 | 3 | 0 | 0 | 10 | 0 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 142 | 626 |
| 10:15 AM | 0 | 0 | 50 | 8 | 0 | 0 | 3 | 77 | 0 | 0 | 0 | 21 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 163 | 656 |
| 10:30 AM | 0 | 1 | 51 | 8 | 0 | 0 | 3 | 65 | 1 | 0 | 0 | 8 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 139 | 664 |
| 10:45 AM | 1 | 2 | 61 | 15 | 0 | 0 | 1 | 85 | 2 | 0 | 0 | 10 | 0 | 2 | 0 | 0 | 1 | 0 | 2 | 0 | 182 | 677 |
| 11:00 AM | 0 | 2 | 69 | 15 | 0 | 0 | 1 | 58 | 1 | 0 | 0 | 18 | 0 | 6 | 0 | 0 | 1 | 0 | 1 | 0 | 172 | 655 |
| 11:15 AM | 0 | 0 | 66 | 9 | 0 | 0 | 2 | 69 | 0 | 0 | 0 | 16 | 1 | 5 | 0 | 0 | 1 | 0 | 2 | 0 | 171 | 673 |
| 11:30 AM | 0 | 2 | 50 | 11 | 0 | 0 | 7 | 69 | 0 | 0 | 0 | 9 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 152 | 701 |
| 11:45 AM | 1 | 1 | 55 | 19 | 0 | 0 | 3 | 63 | 0 | 0 | 0 | 14 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 160 | 743 |
| 12:00 PM | 0 | 3 | 75 | 16 | 0 | 0 | 4 | 64 | 2 | 0 | 0 | 15 | 0 | 5 | 0 | 0 | 3 | 0 | 3 | 0 | 190 | 789 |
| 12:15 PM | 0 | 3 | 66 | 22 | 0 | 0 | 3 | 79 | 2 | 0 | 0 | 16 | 1 | 2 | 0 | 0 | 2 | 0 | 3 | 0 | 199 | 784 |
| 12:30 PM | 0 | 2 | 56 | 16 | 0 | 0 | 3 | 84 | 2 | 0 | 0 | 24 | 0 | 4 | 0 | 0 | 1 | 0 | 2 | 0 | 194 | 772 |
| 12:45 PM | 0 | 1 | 68 | 15 | 0 | 0 | 11 | 77 | 0 | 0 | 0 | 23 | 0 | 6 | 0 | 0 | 4 | 0 | 1 | 0 | 206 | 778 |
| 1:00 PM | 0 | 5 | 66 | 16 | 0 | 0 | 3 | 67 | 1 | 0 | 0 | 18 | 1 | 5 | 0 | 0 | 0 | 0 | 3 | 0 | 185 | 766 |
| 1:15 PM | 0 | 3 | 63 | 19 | 0 | 0 | 5 | 76 | 2 | 0 | 0 | 15 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 0 | 187 | 757 |
| 1:30 PM | 0 | 2 | 85 | 23 | 0 | 0 | 4 | 61 | 2 | 0 | 0 | 12 | 0 | 6 | 0 | 0 | 3 | 0 | 2 | 0 | 200 | 762 |
| 1:45 PM | 0 | 1 | 80 | 18 | 0 | 0 | 3 | 69 | 2 | 0 | 0 | 14 | 2 | 3 | 0 | 0 | 1 | 0 | 1 | 0 | 194 | 761 |
| 2:00 PM | 0 | 4 | 64 | 16 | 0 | 0 | 5 | 65 | 0 | 0 | 0 | 17 | 1 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 176 | 817 |
| 2:15 PM | 0 | 1 | 75 | 18 | 0 | 0 | 3 | 72 | 2 | 0 | 0 | 15 | 2 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 192 | 869 |
| 2:30 PM | 0 | 1 | 72 | 28 | 0 | 0 | 5 | 67 | 2 | 0 | 0 | 16 | 3 | 2 | 0 | 0 | 1 | 0 | 2 | 0 | 199 | 927 |
| 2:45 PM | 0 | 1 | 97 | 19 | 0 | 0 | 5 | 88 | 4 | 0 | 0 | 29 | 0 | 3 | 0 | 0 | 1 | 0 | 3 | 0 | 250 | 1,032 |
| 3:00 PM | 0 | 1 | 83 | 19 | 0 | 0 | 8 | 91 | 1 | 0 | 0 | 21 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 228 | 1,104 |
| 3:15 PM | 0 | 2 | 86 | 27 | 0 | 0 | 6 | 103 | 1 | 0 | 0 | 19 | 0 | 5 | 0 | 0 | 0 | 0 | 1 | 0 | 250 | 1,169 |
| 3:30 PM | 0 | 2 | 137 | 31 | 0 | 0 | 9 | 88 | 2 | 0 | 0 | 25 | 0 | 4 | 0 | 0 | 1 | 0 | 5 | 0 | 304 | 1,223 |
| 3:45 PM | 0 | 1 | 112 | 35 | 0 | 0 | 9 | 132 | 2 | 0 | 0 | 24 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 322 | 1,214 |
| 4:00 PM | 0 | 1 | 124 | 25 | 0 | 0 | 8 | 101 | 3 | 0 | 0 | 21 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 293 | 1,199 |
| 4:15 PM | 0 | 1 | 142 | 39 | 0 | 0 | 4 | 87 | 0 | 0 | 0 | 22 | 0 | 6 | 0 | 0 | 3 | 0 | 0 | 0 | 304 | 1,195 |


| 4:30 PM | 0 | 0 | 123 | 34 | 0 | 0 | 10 | 104 | 1 | 0 | 0 | 17 | 0 | 3 | 0 | 0 | 1 | 0 | 2 | 0 | 295 | 1,178 |
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| 4:45 PM | 1 | 0 | 121 | 24 | 0 | 0 | 12 | 110 | 0 | 0 | 0 | 28 | 0 | 8 | 0 | 0 | 1 | 0 | 2 | 0 | 307 | 1,166 |
| 5:00 PM | 0 | 0 | 125 | 29 | 0 | 0 | 12 | 86 | 0 | 0 | 0 | 30 | 0 | 4 | 0 | 0 | 1 | 0 | 2 | 0 | 289 | 1,073 |
| 5:15 PM | 0 | 0 | 120 | 37 | 0 | 0 | 6 | 90 | 3 | 0 | 0 | 27 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 287 | 0 |
| 5:30 PM | 0 | 2 | 115 | 42 | 0 | 0 | 9 | 89 | 0 | 0 | 0 | 22 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 283 | 0 |
| 5:45 PM | 0 | 0 | 77 | 30 | 0 | 0 | 4 | 78 | 1 | 0 | 0 | 20 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 214 | 0 |

Peak Rolling Hour Flow Rates

|  | Eastbound |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  | Southbound |  |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Type | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR |  |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Lights | 0 | 5 | 515 | 128 | 0 | 0 | 30 | 403 | 7 | 0 | 0 | 88 | 0 | 26 | 0 | 0 | 4 | 0 | 5 | 0 | 1,211 |
| Mediums | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Total | 0 | 5 | 515 | 130 | 0 | 0 | 30 | 408 | 7 | 0 | 0 | 92 | 0 | 27 | 0 | 0 | 4 | 0 | 5 | 0 | 1,223 |


| Bicycles on Crosswalk |  |  | 0 |  |  |  |  | 0 |  |  |  |  | 0 |  |  |  |  | 0 |  |  | 0 |
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| Heavy Vehicle Percentage |  |  | 0.3\% |  |  |  |  | 1.1\% |  |  |  |  | 4.2\% |  |  |  |  | 0.0\% |  |  | 1.0\% |
| Heavy Vehicle Percentage | 0.0\% | 0.0\% | 0.0\% | 1.5\% | 0.0\% | 0.0\% | 0.0\% | 1.2\% | 0.0\% | 0.0\% | 0.0\% | 4.3\% | 0.0\% | 3.7\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 1.0\% |
| Peak Hour Factor (PHF) |  |  | 0.89 |  |  |  |  | 0.86 |  |  |  |  | 0.90 |  |  |  |  | 0.79 |  |  | 0.95 |
| Peak Hour Factor (PHF) | 0.25 | 0.50 | 0.91 | 0.82 | 0.00 | 0.00 | 0.83 | 0.86 | 0.63 | 0.00 | 0.00 | 0.81 | 0.67 | 0.53 | 0.00 | 0.00 | 0.63 | 0.50 | 0.83 | 0.00 | 0.95 |

Traffic Counts by Vehicle Type

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| Time | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | U-Turn | Left | Thru | Right | RTOR | Total |
| Articulated Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 10:30 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |



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| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 4:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Bicycles on Crosswalk

| Time | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CCW | CW | Total | CCW | CW | Total | CCW | CW | Total | CCW | CW | Total |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| Pedestrians | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | CCW | CW | Total | CCW | CW | Total | CCW | CW | Total | CCW | CW | Total |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 AM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 |
| 4:45 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

$\begin{array}{lllllllllllll}\text { 5:30 PM } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \text { 5:45 PM } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$

## Appendix B - Crash Data from 2015 to 2020



## ADT: 21,800 Length: 0.18



## ADT: 21,800 Length: 0.18

|  | com | mo | date |  |  |  |  | Enios |  |  | Ioting | weather |  |  |  |  |  | enice |  | ator | sped 1 | ven move |  |  | diver ${ }^{\text {d }}$ |  | beed | vernmo |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{85}$ |  | 1336 | $3 / 39290281$ | 1800 | poo | on | NTresectoon reateo | 2 | Strachrow-rvel | ory | davcort | none | ${ }^{45}$ | 45 | N | Soseriom |  | Pcoup fruckutur |  | Wwnown | 45 | Passuc | s | Passencercarvan |  | Noapdich |  | siownc | Hw 85 | 00224N | MM | Elpaso |
| 85 |  | 1369 | 5 | 1740 | (N) | ov | at mitrection | 2 | stag.tion.grade | DRY | daxught | Nove | 45 | 45 | N | Appooccturen | $s$ | Passencre carvan | cimpan | ${ }_{\text {Nate }}^{\text {Natul }}$ | 25 | makng leftuen | N | sov | Mex | unkown | ${ }^{45}$ | gong stagitr | HWY 9 | ${ }^{\text {at }}$ | maxvellor | eipaso |
| ${ }^{85}$ |  | 1369 | 210120281 | 1530 | poo | on | at mitrection | 2 | Cunveng.arad | Ir | daxuchr | Svowsertheal | 45 | 25 | N | Broasoso | E | Passencercarivan | Smp | unkrown | 5 | makng fight tuen | N | Passenercharvan | Nompanm ent | Cono foparit | 0 |  | Hwr 8 | ${ }_{\text {at }}$ | Maxwels | eipaso |
| ${ }^{85}$ |  | 1369 | $71 / 2018$ | ${ }^{1350}$ | poo | ow | at mitregctow | 2 | stalicion-lyel | Dar | daxuchr | Nove | 35 | 45 | * | Broasose | E | pccup fruccuturivan | Nompaner | contaparinen | 20 | gomg spalcir | 5 | Passencercarva | Nompanen |  | 45 | gong stalatr | HWY 85 | ${ }_{\text {at }}$ | Maxneus | eipaso |
| 85 |  | 1369 | 91272018 | 800 | w | ${ }^{\text {on }}$ | at witregetow | 2 | cunvenvevel | ory | oaxlohr | NoNE | ${ }^{3}$ | 35 | N | spoasose | w | Ssencercarva | No M P PAMM ETT | opver nexererence | 5 | MAxNG Lift tuen | N | $\mathrm{P}_{\text {frucue }}^{\text {VAN }}$ | NomPAREMT | Conta | 5 | manngemt tur | Hwv ${ }^{\text {a }}$ | at | Maxveus | elpaso |
| 85 |  | 1369 | $84 / 2019$ | 740 | w) | on | at interection | 2 | Sralicir on:lvel | ${ }_{\text {ory }}$ | oxucht | Nove | 25 | 45 | N | в8RaOSOE | E | suv |  | daveratitue | 25 | gomg spalgit | N | Passengeraraval | Iompanm ent | contrab | 45 | gong stractit | Hw\% 8 | at | Maxvels | elpaso |
| 85 |  | ${ }^{1369}$ | 21262020 | 635 | w | ov | atm | 2 | stenchiongre | opr | oxuchtr | NoNE | ${ }_{4}$ | 25 | * | BROASOE | E | SSENERCO |  | unkrown | ${ }^{25}$ | Kng R I | N | Passencercarv |  |  | 0 | Topeeo N | Hwr8 | at | M Maxe二s | Elpaso |
| 85 |  | 1369 | $31 / 2020$ | 1390 | poo | ${ }^{\text {ov }}$ | at wrerectow | 2 | Stalatiou.graoe | suowr | Dark.vucurim | WISETTHEL | 45 | 35 | N | Braosose | E | Passenercharvan |  | Daver nexereluc | 20 | Mang Gight tuent | N | UP TRUCK/UTIUTY | NO IM PA SUSPE |  | 0 | тоpepil w Trafic | Hwr 9 | at | MAxWeus | elpaso |
| 85 |  | 1369 | 61251220 1 | 1890 | (1) | ${ }^{\text {ov }}$ | at witerectow | 2 | Cunveng.apal | DRY | oancochr | wove | 45 | 45 | N | Braossog | N | Passenger carvan |  |  | 10 | Gong staligr | E | Passelerecarvan |  | Conirapurim fat | 45 | Gomg | WY85 | ${ }^{\text {at }}$ | MaxwELs | Elpaso |
| 85 |  | 1369 | ${ }^{6 / 22018}$ | 650 | (1) | ov | at weregectow | 2 | Eovgral | DRY | nught | Nove | 45 | 45 | N | ICraz | N | Passenercarvan | Nom | Convepurime fatior | 5 | makno ler | 5 | Bicale |  | conirapurime fat | ${ }^{30}$ |  | HwY8 | ${ }_{\text {at }}$ | maxweus | Elpaso |
| ${ }^{85}$ |  | 1369 | 7 | 190 | poo | T | miterectow | 1 | Stathitom-rvel | Dar | davught | NoNE | 50 | uk | N | SUAapoall | N | Passenger | Nomen | conimburne fatior | 20 | Kng |  |  |  | Conopparer |  |  | HwY ${ }^{\text {S }}$ | at | maxneus | elpaso |
| 85 |  | 1369 | 122422015 | 2088 | w/ | ow | at witerectoon | 2 | то, | der | Dakklichreo | NoNE | 45 | 45 | N | в8Rasose | N | passenger carvar | No\% | orver Peococupel | 15 | maxnc lefturn | E | sov | Nome | unkNown | ${ }^{45}$ | comg | Hwrs 588 | ${ }^{\text {at }}$ | maxweus | elpaso |
| ${ }_{8} 8$ |  | 1369 | ${ }^{111 / 222015}$ |  | poo | on | Wrepection reateo | 2 | stactirov.gre | Der | DAAR.V.WUCHIED | NoNE | 25 | 25 | $N$ | Reare:No | $\cdots$ | Pecaup rocucuturvan | Nompanmen |  | 5 | ${ }_{\text {bacang }}$ | N | sov | Nomparment | Conoppand | 0 | Sорpe: | мגхیట二st | [002025 | Hwr | elpaso |

## Appendix C - 2021 Existing Conditions Synchro Output Reports

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 8.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement E | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\uparrow$ | 「7 |  | ¢ |  |  | $\dagger$ |  |
| Traffic Vol, veh/h | 4 | 259 | 55 | 12 | 587 | 4 | 114 | 1 | 17 | 1 | 0 | 4 |
| Future Vol, veh/h | 4 | 259 | 55 | 12 | 587 | 4 | 114 | 1 | 17 | 1 | 0 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Fre | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 70 | - | - | 65 | - | - | - | - | - | - |
| Veh in Median Storage, \# |  | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 50 | 86 | 81 | 60 | 84 | 50 | 81 | 25 | 71 | 25 | 63 | 50 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 301 | 68 | 20 | 699 | 8 | 141 | 4 | 24 | 4 | 0 | 8 |





## Appendix D - HCS7 Warrant Output Reports



| 7 C. (56\%) Volumes for Warrants 1A, 1B --or-- 4 are satisfied | $\square$ |
| :--- | ---: |
| Warrant 8: Roadway Network | $\square$ |
| 8 A. Weekday Volume (Peak hour total --and-- projected warrants 1, 2 or 3) --or-- | $\square$ |
| 8 B. Weekend Volume (Five hours total) | $\square$ |
| Warrant 9: Grade Crossing | $\square$ |
| 9 A. Grade Crossing within 140 ft --and-- | $\square$ |
| 9 B. Peak-Hour Vehicular Volumes | $\square$ |
| Copyright © 2016 University of Florida, All Rights Reserved $\quad$ HCS7 $^{\text {TM }}$ Warrants Version 7.1 $\quad$ Generated: 15/2022 3:19 PM |  |


|  | Warrants Volume |  |
| :--- | :--- | :--- |
| Information |  |  |
| Analyst | AECOM | US 85/ Maxwell St |
| Agency/Co | CDOT | Intersection |
| Date Performed | 2022 | U.S. Customary |
| Project ID | US 85/Maxwell St | Unisdiction |
| East/West Street | US 85 | Existing |
| Fime Period Analyzed | Maxwell St |  |
| Nroject Description US 85/Maxwell St |  | North/South Street |



Volume Summary

| Volume Summary |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Lanes 2+ |  |  | Minor Street Lanes 1 |  | Speed |  | 45 | Population |  | 10000+ |
| Hours | Major Volume | Minor Volume | Total Volume | $\begin{gathered} 1 \mathrm{~A} \\ (70 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \mathrm{~A} \\ (56 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \mathrm{~B} \\ (70 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \mathrm{~B} \\ (56 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 2 \\ (70 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 3 \mathrm{~A} \\ (70 \%) \\ \hline \end{gathered}$ | $\begin{gathered} 3 \mathrm{~B} \\ (70 \%) \\ \hline \end{gathered}$ |
| 06-07 | 392 | 72 | 470 | No | No | No | No | No | No | No |
| 07-08 | 896 | 140 | 1039 | Yes | Yes | Yes | Yes | Yes | No | Yes |
| 08-09 | 686 | 110 | 809 | Yes | Yes | Yes | Yes | Yes | No | No |
| 09-10 | 559 | 73 | 644 | No | No | No | Yes | No | No | No |
| 10-11 | 559 | 63 | 626 | No | No | No | Yes | No | No | No |
| 11-12 | 573 | 77 | 655 | No | No | No | Yes | No | No | No |
| 12-13 | 674 | 96 | 789 | No | Yes | Yes | Yes | No | No | No |
| 13-14 | 676 | 78 | 766 | No | No | Yes | Yes | No | No | No |
| 14-15 | 714 | 88 | 817 | No | Yes | Yes | Yes | No | No | No |
| 15-16 | 988 | 108 | 1104 | Yes | Yes | Yes | Yes | Yes | No | No |
| 16-17 | 1075 | 115 | 1199 | Yes | Yes | Yes | Yes | Yes | No | Yes |
| 17-18 | 955 | 113 | 1073 | Yes | Yes | Yes | Yes | Yes | No | No |
| Totals | 8747 | 1133 | 9991 | 5 | 7 | 8 | 11 | 5 | 0 | 2 |

## Appendix E-2045 No-Build Traffic Conditions Synchro Output Reports



| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1135 | 0 | 0 | 568 | 0 | 0 | 1697 | 1693 | 488 | 1747 | 1763 | 1125 |
| Stage 1 | - | - | - | - | - | - | 508 | 508 |  | 1175 | 1175 |  |
| Stage 2 | - | - | - |  | - |  | 1189 | 1185 |  | 572 | 588 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.14 | 6.54 | 6.24 | 7.11 | 6.51 | 6.21 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.14 | 5.54 | - | 6.11 | 5.51 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.14 | 5.54 | - | 6.11 | 5.51 | - |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.536 | 4.036 | 3.336 | 3.509 | 4.009 | 3.309 |
| Pot Cap-1 Maneuver | 616 | - | - | 1004 | - | - | -72 | 92 | 576 | 68 | 85 | 251 |
| Stage 1 | - | - | - | - | - | - | 544 | 535 | - | 235 | 267 | - |
| Stage 2 | - | - | - | - | - | - | 227 | 260 | - | 507 | 498 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 616 | - | - | 1004 | - | - | ~ 59 | 84 | 576 | 49 | 77 | 251 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 59$ | 84 | - | 49 | 77 | - |
| Stage 1 | - | - | - | - | - | - | 531 | 522 | - | 229 | 249 | - |
| Stage 2 | - | - | - | - | - | - | 197 | 242 | - | 453 | 486 | - |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0.2 | $\$ 1040.2$ | 108.1 |
| HCM LOS |  | $F$ | $F$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 69 | 616 | - | -1004 | - | -69 |  |
| HCM Lane V/C Ratio | 3.024 | 0.016 | - | -0.025 | - | -0.55 |  |
| HCM Control Delay (s) | $\$ 1040.2$ | 10.9 | 0 | - | 8.7 | 0 | -108.1 |
| HCM Lane LOS | F | B | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 21.2 | 0 | - | - | 0.1 | - | - |

## Notes

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon



|  | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| Approach | CM |  |  |  |
| HCM LOS | 0.5 | $\$ 1576.4$ | 165.3 |  |
|  |  | $F$ | $F$ |  |



# Appendix F - 2045 Mitigation Synchro \& Sidra Output Reports 

2045 Traffic Signal with Minimal Roadway Improvements Synchro Output Reports
2045 Traffic Signal with Roadway Improvements Synchro Output Reports
2045 Roundabout Sidra Output Reports
2045 Restriping with Existing Pavement Conditions Synchro Output Reports
2045 Right-in/Right-out Synchro Output Reports

|  | - 4 |  | $\rightarrow$ | $\pm$ | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 3 | 4 | 6 | 7 | 8 |
| Movement | NBTL | WBL | EBTL | SBTL | EBL | WBTL |
| Lead/Lag |  | Lead | Lag |  | Lead | Lag |
| Lead-Lag Optimize |  | Yes | Yes |  | Yes | Yes |
| Recall Mode | Max | None | None | Max | None | None |
| Maximum Split (s) | 23 | 10 | 57 | 23 | 10 | 57 |
| Maximum Split (\%) | 25.6\% | 11.1\% | 63.3\% | 25.6\% | 11.1\% | 63.3\% |
| Minimum Split (s) | 23 | 10 | 23 | 23 | 10 | 23 |
| Yellow Time (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| All-Red Time (s) | 2 | 2 | 2 | 2 | 2 | 2 |
| Minimum Initial (s) | 5 | 5 | 5 | 5 | 5 | 5 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) | 7 |  | 7 | 7 |  | 7 |
| Flash Dont Walk (s) | 11 |  | 11 | 11 |  | 11 |
| Dual Entry | Yes | No | Yes | Yes | No | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| End Time (s) | 23 | 33 | 0 | 23 | 33 | 0 |
| Yield/Force Off (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Yield/Force Off 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Local Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| Local Yield (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Local Yield 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |


| Intersection Summary |  |
| :--- | ---: |
| Cycle Length | 90 |
| Control Type | Semi Act-Uncoord |
| Natural Cycle | 90 |

Splits and Phases: 3: Maxwell St \& US 85


|  | 4 | $\rightarrow$ | 7 | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ | $1$ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 个 |  | ${ }^{7}$ | $\uparrow$ |  |  | \$ |  |
| Traffic Volume (veh/h) | 5 | 420 | 65 | 15 | 945 | 5 | 130 | 5 | 20 | 5 | 5 | 5 |
| Future Volume (veh/h) | 5 | 420 | 65 | 15 | 945 | 5 | 130 | 5 | 20 | 5 | 5 | 5 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1841 | 1841 | 1841 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 10 | 488 | 80 | 25 | 1125 | 10 | 160 | 20 | 28 | 20 | 8 | 10 |
| Peak Hour Factor | 0.50 | 0.86 | 0.81 | 0.60 | 0.84 | 0.50 | 0.81 | 0.25 | 0.71 | 0.25 | 0.63 | 0.50 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 4 | 4 | 1 | 1 | 1 |
| Cap, veh/h | 106 | 925 | 152 | 472 | 1118 | 10 | 380 | 145 | 203 | 212 | 87 | 84 |
| Arrive On Green | 0.01 | 0.59 | 0.59 | 0.03 | 0.60 | 0.60 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1781 | 1567 | 257 | 1781 | 1851 | 16 | 1373 | 694 | 972 | 707 | 415 | 401 |
| Grp Volume(v), veh/h | 10 | 0 | 568 | 25 | 0 | 1135 | 160 | 0 | 48 | 38 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1824 | 1781 | 0 | 1867 | 1373 | 0 | 1666 | 1523 | 0 | 0 |
| Q Serve(g_s), s | 0.2 | 0.0 | 15.9 | 0.5 | 0.0 | 52.0 | 6.3 | 0.0 | 2.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.2 | 0.0 | 15.9 | 0.5 | 0.0 | 52.0 | 8.3 | 0.0 | 2.0 | 2.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.14 | 1.00 |  | 0.01 | 1.00 |  | 0.58 | 0.53 |  | 0.26 |
| Lane Grp Cap(c), veh/h | 106 | 0 | 1077 | 472 | 0 | 1128 | 380 | 0 | 348 | 382 | 0 | 0 |
| V/C Ratio(X) | 0.09 | 0.00 | 0.53 | 0.05 | 0.00 | 1.01 | 0.42 | 0.00 | 0.14 | 0.10 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 187 | 0 | 1102 | 529 | 0 | 1128 | 380 | 0 | 348 | 382 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 21.8 | 0.0 | 10.5 | 7.9 | 0.0 | 17.0 | 30.0 | 0.0 | 27.7 | 27.5 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 0.4 | 0.0 | 0.0 | 28.2 | 3.4 | 0.0 | 0.8 | 0.5 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 0.0 | 5.3 | 0.1 | 0.0 | 25.7 | 3.3 | 0.0 | 0.9 | 0.7 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 22.2 | 0.0 | 10.9 | 8.0 | 0.0 | 45.3 | 33.4 | 0.0 | 28.5 | 28.0 | 0.0 | 0.0 |
| LnGrp LOS | C | A | B | A | A | F | C | A | C | C | A | A |
| Approach Vol, veh/h |  | 578 |  |  | 1160 |  |  | 208 |  |  | 38 |  |
| Approach Delay, s/veh |  | 11.1 |  |  | 44.5 |  |  | 32.3 |  |  | 28.0 |  |
| Approach LOS |  | B |  |  | D |  |  | C |  |  | C |  |
| Timer - Assigned Phs |  | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $s$ |  | 23.0 | 7.2 | 55.8 |  | 23.0 | 6.1 | 57.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 18.0 | 5.0 | 52.0 |  | 18.0 | 5.0 | 52.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 10.3 | 2.5 | 17.9 |  | 4.0 | 2.2 | 54.0 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.4 | 0.0 | 3.7 |  | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 33.2 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | $\downarrow$ | 4 | 4 | 4 | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBT |
| Lane Group Flow (vph) | 10 | 568 | 25 | 1135 | 160 | 48 | 38 |
| v/c Ratio | 0.05 | 0.51 | 0.05 | 0.96 | 0.55 | 0.12 | 0.11 |
| Control Delay | 5.4 | 11.6 | 5.0 | 34.5 | 37.2 | 16.2 | 22.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 5.4 | 11.6 | 5.0 | 34.5 | 37.2 | 16.2 | 22.5 |
| Queue Length 50th (tt) | 2 | 122 | 4 | 446 | 71 | 8 | 11 |
| Queue Length 95th (tt) | 3 | 247 | 7 | \#853 | 132 | 1 | 26 |
| Internal Link Dist (tt) |  | 270 |  | 257 |  | 282 | 126 |
| Turn Bay Length ( t ) | 70 |  | 70 |  | 100 |  |  |
| Base Capacity (vph) | 191 | 1165 | 485 | 1183 | 293 | 388 | 353 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.49 | 0.05 | 0.96 | 0.55 | 0.12 | 0.11 |
| Intersection Summary |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |


|  | - 4 |  | $\rightarrow$ | $\pm$ | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 3 | 4 | 6 | 7 | 8 |
| Movement | NBTL | WBL | EBTL | SBTL | EBL | WBTL |
| Lead/Lag |  | Lead | Lag |  | Lead | Lag |
| Lead-Lag Optimize |  | Yes | Yes |  | Yes | Yes |
| Recall Mode | Max | None | None | Max | None | None |
| Maximum Split (s) | 23 | 10 | 57 | 23 | 10 | 57 |
| Maximum Split (\%) | 25.6\% | 11.1\% | 63.3\% | 25.6\% | 11.1\% | 63.3\% |
| Minimum Split (s) | 23 | 10 | 23 | 23 | 10 | 23 |
| Yellow Time (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| All-Red Time (s) | 2 | 2 | 2 | 2 | 2 | 2 |
| Minimum Initial (s) | 5 | 5 | 5 | 5 | 5 | 5 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) | 7 |  | 7 | 7 |  | 7 |
| Flash Dont Walk (s) | 11 |  | 11 | 11 |  | 11 |
| Dual Entry | Yes | No | Yes | Yes | No | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| End Time (s) | 23 | 33 | 0 | 23 | 33 | 0 |
| Yield/Force Off (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Yield/Force Off 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Local Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| Local Yield (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Local Yield 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |


| Intersection Summary |  |
| :--- | ---: |
| Cycle Length | 90 |
| Control Type | Semi Act-Uncoord |
| Natural Cycle | 90 |

Splits and Phases: 3: Maxwell St \& US 85


|  | 4 | $\rightarrow$ | $\geqslant$ | 7 | $4$ | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 个 |  | ${ }^{7}$ | $\uparrow$ |  |  | \& |  |
| Traffic Volume (veh/h) | 10 | 830 | 150 | 35 | 660 | 10 | 105 | 5 | 35 | 5 | 5 | 10 |
| Future Volume (veh/h) | 10 | 830 | 150 | 35 | 660 | 10 | 105 | 5 | 35 | 5 | 5 | 10 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1841 | 1841 | 1841 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 16 | 912 | 181 | 42 | 857 | 17 | 114 | 5 | 51 | 15 | 13 | 40 |
| Peak Hour Factor | 0.63 | 0.91 | 0.83 | 0.83 | 0.77 | 0.58 | 0.92 | 0.96 | 0.68 | 0.33 | 0.38 | 0.25 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 4 | 4 | 1 | 1 | 1 |
| Cap, veh/h | 280 | 893 | 177 | 147 | 1110 | 22 | 367 | 29 | 294 | 96 | 90 | 195 |
| Arrive On Green | 0.02 | 0.59 | 0.59 | 0.04 | 0.61 | 0.61 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1515 | 301 | 1781 | 1828 | 36 | 1330 | 141 | 1440 | 227 | 443 | 956 |
| Grp Volume(v), veh/h | 16 | 0 | 1093 | 42 | 0 | 874 | 114 | 0 | 56 | 68 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 0 | 1816 | 1781 | 0 | 1864 | 1330 | 0 | 1581 | 1625 | 0 | 0 |
| Q Serve(g_s), s | 0.3 | 0.0 | 52.0 | 0.8 | 0.0 | 30.6 | 2.7 | 0.0 | 2.6 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.3 | 0.0 | 52.0 | 0.8 | 0.0 | 30.6 | 5.6 | 0.0 | 2.6 | 2.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.17 | 1.00 |  | 0.02 | 1.00 |  | 0.91 | 0.22 |  | 0.59 |
| Lane Grp Cap(c), veh/h | 280 | 0 | 1071 | 147 | 0 | 1132 | 367 | 0 | 323 | 381 | 0 | 0 |
| V/C Ratio(X) | 0.06 | 0.00 | 1.02 | 0.29 | 0.00 | 0.77 | 0.31 | 0.00 | 0.17 | 0.18 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 348 | 0 | 1071 | 183 | 0 | 1132 | 367 | 0 | 323 | 381 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 11.7 | 0.0 | 18.1 | 21.6 | 0.0 | 12.8 | 30.0 | 0.0 | 29.0 | 29.1 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 32.9 | 1.1 | 0.0 | 3.3 | 2.2 | 0.0 | 1.2 | 1.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 0.0 | 26.8 | 0.5 | 0.0 | 11.0 | 2.3 | 0.0 | 1.1 | 1.3 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 11.8 | 0.0 | 51.0 | 22.7 | 0.0 | 16.1 | 32.2 | 0.0 | 30.1 | 30.1 | 0.0 | 0.0 |
| LnGrp LOS | B | A | F | C | A | B | C | A | C | C | A | A |
| Approach Vol, veh/h |  | 1109 |  |  | 916 |  |  | 170 |  |  | 68 |  |
| Approach Delay, s/veh |  | 50.4 |  |  | 16.4 |  |  | 31.5 |  |  | 30.1 |  |
| Approach LOS |  | D |  |  | B |  |  | C |  |  | C |  |
| Timer - Assigned Phs |  | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $s$ |  | 23.0 | 8.2 | 57.0 |  | 23.0 | 6.6 | 58.6 |  |  |  |  |
| Change Period (Y+Rc), s |  | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 18.0 | 5.0 | 52.0 |  | 18.0 | 5.0 | 52.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 7.6 | 2.8 | 54.0 |  | 4.9 | 2.3 | 32.6 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.4 | 0.0 | 0.0 |  | 0.2 | 0.0 | 5.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 34.6 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | $\rangle$ | $\rightarrow$ | 7 |  | 4 | $\dagger$ | $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBT |
| Lane Group Flow (vph) | 16 | 1093 | 42 | 874 | 114 | 56 | 68 |
| V/c Ratio | 0.05 | 0.99 | 0.23 | 0.72 | 0.38 | 0.15 | 0.18 |
| Control Delay | 4.9 | 43.1 | 7.7 | 15.2 | 34.8 | 11.5 | 17.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 4.9 | 43.1 | 7.7 | 15.2 | 34.8 | 11.5 | 17.0 |
| Queue Length 50th (tt) | 3 | $\sim 671$ | 7 | 252 | 57 | 2 | 13 |
| Queue Length 95th (tt) | 6 | \#915 | 15 | 396 | 108 | 34 | 9 |
| Internal Link Dist (tt) |  | 270 |  | 257 |  | 282 | 126 |
| Turn Bay Length (tt) | 70 |  | 70 |  | 100 |  |  |
| Base Capacity (vph) | 299 | 1109 | 182 | 1209 | 300 | 371 | 373 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.99 | 0.23 | 0.72 | 0.38 | 0.15 | 0.18 |
| Intersection Summary |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |


|  | 4 | $\%$ | $\rightarrow$ | 1 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 3 | 4 | 6 | 7 | 8 |
| Movement | NBTL | WBL | EBTL | SBTL | EBL | WBTL |
| Lead/Lag |  | Lead | Lag |  | Lead | Lag |
| Lead-Lag Optimize |  | Yes | Yes |  | Yes | Yes |
| Recall Mode | Max | None | None | Max | None | None |
| Maximum Split (s) | 23 | 10 | 57 | 23 | 10 | 57 |
| Maximum Split (\%) | 25.6\% | 11.1\% | 63.3\% | 25.6\% | 11.1\% | 63.3\% |
| Minimum Split (s) | 23 | 10 | 23 | 23 | 10 | 23 |
| Yellow Time (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| All-Red Time (s) | 2 | 2 | 2 | 2 | 2 | 2 |
| Minimum Initial (s) | 5 | 5 | 5 | 5 | 5 | 5 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) | 7 |  | 7 | 7 |  | 7 |
| Flash Dont Walk (s) | 11 |  | 11 | 11 |  | 11 |
| Dual Entry | Yes | No | Yes | Yes | No | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| End Time (s) | 23 | 33 | 0 | 23 | 33 | 0 |
| Yield/Force Off (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Yield/Force Off 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Local Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| Local Yield (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Local Yield 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Intersection Summary |  |  |  |  |  |  |


| Cycle Length | 90 |
| :--- | ---: |
| Control Type | Semi Act-Uncoord |
| Natural Cycle | 90 |

Splits and Phases: 3: Maxwell St \& US 85


|  | 4 | $\rightarrow$ | 7 | 7 |  | 4 | $4$ | $\dagger$ | $p$ | $1$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 7 | ${ }^{7}$ | 个 |  | ${ }^{1}$ | $\uparrow$ |  |  | \$ |  |
| Traffic Volume (veh/h) | 5 | 420 | 65 | 15 | 945 | 5 | 130 | 5 | 20 | 5 | 5 | 5 |
| Future Volume (veh/h) | 5 | 420 | 65 | 15 | 945 | 5 | 130 | 5 | 20 | 5 | 5 | 5 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1841 | 1841 | 1841 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 10 | 488 | 80 | 25 | 1125 | 10 | 160 | 20 | 28 | 20 | 8 | 10 |
| Peak Hour Factor | 0.50 | 0.86 | 0.81 | 0.60 | 0.84 | 0.50 | 0.81 | 0.25 | 0.71 | 0.25 | 0.63 | 0.50 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 4 | 4 | 1 | 1 | 1 |
| Cap, veh/h | 106 | 1104 | 936 | 506 | 1118 | 10 | 380 | 145 | 203 | 212 | 87 | 84 |
| Arrive On Green | 0.01 | 0.59 | 0.59 | 0.03 | 0.60 | 0.60 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1781 | 1870 | 1585 | 1781 | 1851 | 16 | 1373 | 694 | 972 | 707 | 415 | 401 |
| Grp Volume(v), veh/h | 10 | 488 | 80 | 25 | 0 | 1135 | 160 | 0 | 48 | 38 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1870 | 1585 | 1781 | 0 | 1867 | 1373 | 0 | 1666 | 1523 | 0 | 0 |
| Q Serve(g_s), s | 0.2 | 12.4 | 1.9 | 0.5 | 0.0 | 52.0 | 6.3 | 0.0 | 2.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.2 | 12.4 | 1.9 | 0.5 | 0.0 | 52.0 | 8.3 | 0.0 | 2.0 | 2.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.01 | 1.00 |  | 0.58 | 0.53 |  | 0.26 |
| Lane Grp Cap(c), veh/h | 106 | 1104 | 936 | 506 | 0 | 1128 | 380 | 0 | 348 | 382 | 0 | 0 |
| V/C Ratio(X) | 0.09 | 0.44 | 0.09 | 0.05 | 0.00 | 1.01 | 0.42 | 0.00 | 0.14 | 0.10 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 187 | 1130 | 958 | 563 | 0 | 1128 | 380 | 0 | 348 | 382 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 21.8 | 9.8 | 7.6 | 7.3 | 0.0 | 17.0 | 30.0 | 0.0 | 27.7 | 27.5 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.4 | 0.3 | 0.0 | 0.0 | 0.0 | 28.2 | 3.4 | 0.0 | 0.8 | 0.5 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 4.2 | 0.5 | 0.1 | 0.0 | 25.7 | 3.3 | 0.0 | 0.9 | 0.7 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 22.2 | 10.0 | 7.6 | 7.4 | 0.0 | 45.3 | 33.4 | 0.0 | 28.5 | 28.0 | 0.0 | 0.0 |
| LnGrp LOS | C | B | A | A | A | F | C | A | C | C | A | A |
| Approach Vol, veh/h |  | 578 |  |  | 1160 |  |  | 208 |  |  | 38 |  |
| Approach Delay, s/veh |  | 9.9 |  |  | 44.5 |  |  | 32.3 |  |  | 28.0 |  |
| Approach LOS |  | A |  |  | D |  |  | C |  |  | C |  |
| Timer - Assigned Phs |  | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $s$ |  | 23.0 | 7.2 | 55.8 |  | 23.0 | 6.1 | 57.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 18.0 | 5.0 | 52.0 |  | 18.0 | 5.0 | 52.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 10.3 | 2.5 | 14.4 |  | 4.0 | 2.2 | 54.0 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.4 | 0.0 | 3.3 |  | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 32.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  | 7 | $\leftrightarrow$ | 4 | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
| Lane Group Flow (vph) | 10 | 488 | 80 | 25 | 1135 | 160 | 48 | 38 |
| v/c Ratio | 0.05 | 0.43 | 0.08 | 0.05 | 0.96 | 0.55 | 0.12 | 0.11 |
| Control Delay | 5.4 | 10.7 | 2.2 | 5.0 | 34.5 | 37.2 | 16.2 | 22.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 5.4 | 10.7 | 2.2 | 5.0 | 34.5 | 37.2 | 16.2 | 22.5 |
| Queue Length 50th (tt) | 2 | 101 | 0 | 4 | 446 | 71 | 8 | 11 |
| Queue Length 95th (ft) | 3 | 205 | 13 | 7 | \#853 | 132 | 1 | 26 |
| Internal Link Dist (t) |  | 270 |  |  | 257 |  | 282 | 126 |
| Turn Bay Length (t) | 100 |  | 150 | 100 |  | 150 |  |  |
| Base Capacity (vph) | 191 | 1183 | 1036 | 546 | 1183 | 293 | 388 | 353 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.41 | 0.08 | 0.05 | 0.96 | 0.55 | 0.12 | 0.11 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |


|  | 4 | $\%$ | $\rightarrow$ | 1 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 3 | 4 | 6 | 7 | 8 |
| Movement | NBTL | WBL | EBTL | SBTL | EBL | WBTL |
| Lead/Lag |  | Lead | Lag |  | Lead | Lag |
| Lead-Lag Optimize |  | Yes | Yes |  | Yes | Yes |
| Recall Mode | Max | None | None | Max | None | None |
| Maximum Split (s) | 23 | 10 | 57 | 23 | 10 | 57 |
| Maximum Split (\%) | 25.6\% | 11.1\% | 63.3\% | 25.6\% | 11.1\% | 63.3\% |
| Minimum Split (s) | 23 | 10 | 23 | 23 | 10 | 23 |
| Yellow Time (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| All-Red Time (s) | 2 | 2 | 2 | 2 | 2 | 2 |
| Minimum Initial (s) | 5 | 5 | 5 | 5 | 5 | 5 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) | 7 |  | 7 | 7 |  | 7 |
| Flash Dont Walk (s) | 11 |  | 11 | 11 |  | 11 |
| Dual Entry | Yes | No | Yes | Yes | No | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| End Time (s) | 23 | 33 | 0 | 23 | 33 | 0 |
| Yield/Force Off (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Yield/Force Off 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Local Start Time (s) | 0 | 23 | 33 | 0 | 23 | 33 |
| Local Yield (s) | 18 | 28 | 85 | 18 | 28 | 85 |
| Local Yield 170(s) | 7 | 28 | 74 | 7 | 28 | 74 |
| Intersection Summary |  |  |  |  |  |  |


| Cycle Length | 90 |
| :--- | ---: |
| Control Type | Semi Act-Uncoord |
| Natural Cycle | 80 |

Splits and Phases: 3: Maxwell St \& US 85


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 |  | \% | 7 |  | 4 | $\dagger$ | $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
| Lane Group Flow (vph) | 16 | 912 | 181 | 42 | 874 | 114 | 56 | 68 |
| v/c Ratio | 0.06 | 0.89 | 0.20 | 0.20 | 0.79 | 0.31 | 0.13 | 0.16 |
| Control Delay | 5.1 | 28.1 | 3.5 | 7.0 | 18.2 | 32.3 | 11.4 | 16.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 5.1 | 28.1 | 3.5 | 7.0 | 18.2 | 32.3 | 11.4 | 16.8 |
| Queue Length 50th (ft) | 3 | 397 | 11 | 7 | 252 | 55 | 2 | 13 |
| Queue Length 95th (ft) | 6 | \#675 | 33 | 15 | 396 | 108 | 34 | 9 |
| Internal Link Dist (ft) |  | 270 |  |  | 257 |  | 282 | 126 |
| Turn Bay Length (ft) | 100 |  | 150 | 100 |  | 150 |  |  |
| Base Capacity (vph) | 251 | 1329 | 1167 | 209 | 1401 | 362 | 428 | 433 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.06 | 0.69 | 0.16 | 0.20 | 0.62 | 0.31 | 0.13 | 0.16 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| \# 95th percentile volur | \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |

## MOVEMENT SUMMARY

$\forall$ Site: 101 [2045 AM US 85 and Maxwell St (Site Folder: US 85 and Maxwell St)]
2045 Rounabout Option
Site Category: Future Conditions
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { IN } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { ICK OF } \\ & =\mathrm{UE} \\ & \text { Dist ] } \\ & \mathrm{ft} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{mph}$ |
| South: Maxwell St |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 130 | 4.0 | 160 | 4.0 | 0.270 | 7.7 | LOS A | 1.2 | 30.5 | 0.60 | 0.58 | 0.60 | 26.6 |
| 8 | T1 | 5 | 4.0 | 20 | 4.0 | 0.270 | 7.7 | LOS A | 1.2 | 30.5 | 0.60 | 0.58 | 0.60 | 26.6 |
| 18 | R2 | 20 | 4.0 | 28 | 4.0 | 0.270 | 7.7 | LOS A | 1.2 | 30.5 | 0.60 | 0.58 | 0.60 | 26.0 |
| Appr | oach | 155 | 4.0 | 209 | 4.0 | 0.270 | 7.7 | LOS A | 1.2 | 30.5 | 0.60 | 0.58 | 0.60 | 26.5 |
| East: US 85 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 15 | 2.0 | 25 | 2.0 | 1.049 | 60.1 | LOS F | 80.9 | 2054.8 | 1.00 | 2.01 | 3.55 | 19.4 |
| 6 | T1 | 945 | 2.0 | 1125 | 2.0 | 1.049 | 60.1 | LOS F | 80.9 | 2054.8 | 1.00 | 2.01 | 3.55 | 19.4 |
| 16 | R2 | 5 | 2.0 | 10 | 2.0 | 1.049 | 60.1 | LOS F | 80.9 | 2054.8 | 1.00 | 2.01 | 3.55 | 19.1 |
| Appr | ach | 965 | 2.0 | 1160 | 2.0 | 1.049 | 60.1 | LOS F | 80.9 | 2054.8 | 1.00 | 2.01 | 3.55 | 19.4 |
| North: Maxwell St |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 5 | 1.0 | 20 | 1.0 | 0.104 | 11.4 | LOS B | 0.4 | 9.1 | 0.75 | 0.75 | 0.75 | 25.9 |
| 4 | T1 | 5 | 1.0 | 8 | 1.0 | 0.104 | 11.4 | LOS B | 0.4 | 9.1 | 0.75 | 0.75 | 0.75 | 25.9 |
| 14 | R2 | 5 | 1.0 | 10 | 1.0 | 0.104 | 11.4 | LOS B | 0.4 | 9.1 | 0.75 | 0.75 | 0.75 | 25.3 |
| Appr | ach | 15 | 1.0 | 38 | 1.0 | 0.104 | 11.4 | LOS B | 0.4 | 9.1 | 0.75 | 0.75 | 0.75 | 25.7 |
| West: US 85 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 5 | 2.0 | 10 | 2.0 | 0.451 | 7.4 | LOS A | 3.2 | 80.6 | 0.26 | 0.11 | 0.26 | 35.3 |
| 2 | T1 | 420 | 2.0 | 488 | 2.0 | 0.451 | 7.4 | LOS A | 3.2 | 80.6 | 0.26 | 0.11 | 0.26 | 35.2 |
| 12 | R2 | 65 | 2.0 | 80 | 2.0 | 0.451 | 7.4 | LOS A | 3.2 | 80.6 | 0.26 | 0.11 | 0.26 | 34.2 |
| Approach |  | 490 | 2.0 | 579 | 2.0 | 0.451 | 7.4 | LOS A | 3.2 | 80.6 | 0.26 | 0.11 | 0.26 | 35.1 |
| All Vehicles |  | 1625 | 2.2 | 1985 | 2.2 | 1.049 | 38.3 | LOS E | 80.9 | 2054.8 | 0.74 | 1.28 | 2.23 | 23.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^0]
## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2045 PM US 85 and Maxwell St (Site Folder: US 85 and Maxwell St)]
2045 Rounabout Option
Site Category: Future Conditions
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE | CK OF UE Dist ] ft | Prop. Que | Effective Stop Rate | Aver. Aver.  <br> No. Speed  <br> Cycles mph |  |
| South: Maxwell St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 105 | 4.0 | 114 | 4.0 | 0.343 | 12.7 | LOS B | 1.5 | 38.3 | 0.72 | 0.79 | 0.88 | 25.3 |
| 8 T1 | 5 | 4.0 | 5 | 4.0 | 0.343 | 12.7 | LOS B | 1.5 | 38.3 | 0.72 | 0.79 | 0.88 | 25.3 |
| 18 R2 | 35 | 4.0 | 51 | 4.0 | 0.343 | 12.7 | LOS B | 1.5 | 38.3 | 0.72 | 0.79 | 0.88 | 24.7 |
| Approach | 145 | 4.0 | 171 | 4.0 | 0.343 | 12.7 | LOS B | 1.5 | 38.3 | 0.72 | 0.79 | 0.88 | 25.1 |
| East: US 85 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 35 | 2.0 | 42 | 2.0 | 0.782 | 17.0 | LOS C | 14.2 | 361.8 | 0.79 | 0.61 | 0.95 | 30.6 |
| 6 T1 | 660 | 2.0 | 857 | 2.0 | 0.782 | 17.0 | LOS C | 14.2 | 361.8 | 0.79 | 0.61 | 0.95 | 30.6 |
| 16 R2 | 10 | 2.0 | 17 | 2.0 | 0.782 | 17.0 | LOS C | 14.2 | 361.8 | 0.79 | 0.61 | 0.95 | 29.8 |
| Approach | 705 | 2.0 | 917 | 2.0 | 0.782 | 17.0 | LOS C | 14.2 | 361.8 | 0.79 | 0.61 | 0.95 | 30.6 |
| North: Maxwell St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 5 | 1.0 | 15 | 1.0 | 0.144 | 9.6 | LOS A | 0.5 | 13.5 | 0.69 | 0.69 | 0.69 | 26.9 |
| 4 T1 | 5 | 1.0 | 13 | 1.0 | 0.144 | 9.6 | LOS A | 0.5 | 13.5 | 0.69 | 0.69 | 0.69 | 26.8 |
| 14 R2 | 10 | 1.0 | 40 | 1.0 | 0.144 | 9.6 | LOS A | 0.5 | 13.5 | 0.69 | 0.69 | 0.69 | 26.2 |
| Approach | 20 | 1.0 | 68 | 1.0 | 0.144 | 9.6 | LOS A | 0.5 | 13.5 | 0.69 | 0.69 | 0.69 | 26.5 |
| West: US 85 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $5 \quad \mathrm{~L} 2$ | 10 | 2.0 | 16 | 2.0 | 0.882 | 23.6 | LOS C | 18.3 | 463.8 | 0.92 | 0.47 | 0.92 | 28.2 |
| 2 T1 | 830 | 2.0 | 912 | 2.0 | 0.882 | 23.6 | LOS C | 18.3 | 463.8 | 0.92 | 0.47 | 0.92 | 28.1 |
| 12 R 2 | 150 | 2.0 | 181 | 2.0 | 0.882 | 23.6 | LOS C | 18.3 | 463.8 | 0.92 | 0.47 | 0.92 | 27.4 |
| Approach | 990 | 2.0 | 1109 | 2.0 | 0.882 | 23.6 | LOS C | 18.3 | 463.8 | 0.92 | 0.47 | 0.92 | 28.0 |
| All Vehicles | 1860 | 2.1 | 2264 | 2.1 | 0.882 | 19.7 | LOS C | 18.3 | 463.8 | 0.85 | 0.56 | 0.92 | 28.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^1]


|  | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| Approach | CM |  |  |  |
| HCM LOS | 0.2 | $\$ 671.1$ | 103.1 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 76.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 | ${ }^{7}$ | F |  | ${ }^{*}$ | $\uparrow$ |  |  | 4 |  |
| Traffic Vol, veh/h | 10 | 830 | 150 | 35 | 660 | 10 | 105 | 5 | 35 | 5 | 5 | 10 |
| Future Vol, veh/h | 10 | 830 | 150 | 35 | 660 | 10 | 105 | 5 | 35 | 5 | 5 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 100 | 100 | - | - | 150 | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 63 | 91 | 83 | 83 | 77 | 58 | 92 | 96 | 68 | 33 | 38 | 25 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 4 | 4 | 1 | 1 | 1 |
| Mvmt Flow | 16 | 912 | 181 | 42 | 857 | 17 | 114 | 5 | 51 | 15 | 13 | 40 |



|  | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| Approach | CM |  |  |  |
| HCM LOS | 0.5 | $\$ 951.8$ | 156.7 |  |
|  |  | $F$ | $F$ |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 32 | 233 | 772 | - | - | 638 | - |
| HCM Lane V/C Ratio | 3.567 | 0.243 | 0.021 | - | -0.066 | - | -0.865 |
| HCM Control Delay (s) | $\$ 1411.9$ | 25.3 | 9.8 | 0 | - | 11 | - |
| HCM Lane LOS | F | D | A | A | - | -156 | - |
| HCM 95th \%tile Q(veh) | 13.4 | 0.9 | 0.1 | - | - | 0.2 | - |


 Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.4 | 0 | 11.6 | 21.3 |
| HCM LOS |  |  | B |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 576 | 616 | - | - | - | - |
| HCM Lane V/C Ratio | 0.049 | 0.032 | - | - | - | - |
| HCM Control Delay (s) | 11.6 | 11 | 0 | - | - | - |
| HCM Lane LOS | B | B | A | - | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 0.1 | - | - | - | - |


 Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0 | 18 | 17.9 |
| HCM LOS |  |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 329 | 772 | - | - | - | - |
| HCM Lane V/C Ratio | 0.156 | 0.031 | - | - | - | -0.223 |
| HCM Control Delay (s) | 18 | 9.8 | 0 | - | - | - |
| HCM Lane LOS | C | A | A | - | - | - |
| HCM 95th \%tile Q(veh) | 0.5 | 0.1 | - | - | - | - |

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