

5

DATE

B-618-1

(use with B-618-2 and B-618-3; also add B-618-7 when horizontal curve is present)

1. Reinforcing that interferes with the prestressing tendon alignment shall be adjusted as approved by the Engineer.

2. Where dead end anchorage and tendons are accessible, the anchorage system and length of projecting prestressing steel shall permit jacking with the same jacking equipment that was used on the live end.

3. Deviations from the duct pattern, duct size, and strand size assumed in the design must be approved by the Engineer. Duct patterns 1 and 2 are the only acceptable patterns.

4. The deflection shown is positive downward. It includes the instantaneous effects of dead load and prestressing, and a factor of three (3) multiplier to account for long term creep. Formed web elevations must be adjusted upward for an indicated positive deflection.

5. Use stress relieved or low-relaxation strands meeting the requirements

Tendons may be jacked from both ends, either simultaneously or sequentially, or  $\frac{1}{2}$  the tendons may be jacked from each end. If  $\frac{1}{2}$  the tendons are jacked from each end, the jacking force shall be increased \_\_\_\_Kip. If jacking force or steel area is greater than assumed in the design, prestressing quantities shall not be adjusted.

No more than  $^{1\!/}_{2}$  of the prestressing force in any web may be stressed before an equal force is stressed in the adjacent webs. At no time during the stressing operations will more than % of the total prestressing force be applied eccentrically about the centerline of the structure.

At the Contractor's option, the prestressing force may vary  $\pm 5\%$  from the theoretical force per web, provided the total P(Jack) force is obtained and is distributed symmetrically about the centerline of the typical section. P(Jack) is the sum of the peak forces reached during jacking in each tendon.

Design is based on K=0.0002 and  $\mu$ =0.25. P(Jack) at the jacking ends includes friction, anchor set of  $0.375^{"}$  at the jacking end, elastic shortening, and provisions for an additional <u>32</u> KSI long term loss in stress.

Duct pattern\_\_, on B\_\_\_, with \_\_\_ inch diameter stress relieved strands in \_\_\_ 0.D. ducts was assumed in the design.

= 4500 psiat 28 days field compressive strength

= 3500 psi at stressing

 $\bigoplus$  Designates critical points for P(Jack). The Contractor shall submit elongation and jacking calculations based on KL+ $\mu$ a (including anchor set if any) and initial stress (initial stress ratio times jacking stress before long-term losses) at the points labeled " $\bigoplus$ " and

RITICAL DINT <del>- </del>	KL+ μα	INITIAL STRESS RATIO
1.0	0.	0.
1.4	0.	0.
2.0	0.	0.
2.5	0.	0.
3.0	0.	0.
3.5	0.	0.
4.0	0.	0.
4.6	0.	0.
5.0	0.	0.

	Project No./Code		
BOX-GIRDER DETAILS			Project Number
ner: XXXXXXXXX	Structure	X-XX-XX	Code
ler: XXXXXXXX	Numbers	X-XX-XX	
t Subset: BRIDGE	Subset Sheets: BXX of XXX		Sheet Number