# EFFECTS OF GEOMETRIC CHARACTERISTICS OF INTERCHANGES ON TRUCK SAFETY 

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## ABSTBACT (Maximum 200 wand)

Relationships between truck accidents and selected geometnc charactenstics of interchanges are examined. Danasets containing information on truck accidents at interchanges, traffic exposure and selected geometric characteristics are analyzed with an amphasis on interchange and ramp configurations. Most of the data in the report was obtained from the Washington State DOT, with limited data obtained from Colorado and Califormia. In order to assess the impact of merging and diverging maneuvers on safety, the limits of ramp influence zones expressed in terms of accident frequencies were defined on the main line alignments. In addition, a procedirte for identifying high-risk locations from the standpoint of truck operations was proposed.

Freeway truck accidents were grouped by ramp type, accident type, and by four conflict areas of each merge or diverge ranap and sompared nin the basis of truck accidents per location and per truck mile of travel. Truck accident frequencies and rate were not found to be significantly different by ramp type alone, but were significantly different by conflict area and accident type, both between and within ramp rypes. Truck accident freçuencies at ramps wete found to be less than proportional to truck volumes, neaning that high volume ramps had lower rates of truck accidents per truck mile of travel. Thus, a ramp's safety risk is related .o accident type and conflict area, but not directly to truck volumes, which affects identifications of high-risk locations.

Selected aspects of the AASHTO Policy on Geometric Design were examined from the standpoim of truck operations. This portion of the report was largely conducted as a literature review. In order to develop greater understanding of the relationship between truck uccidents and geometrics of interchanges, the study conducted a series of truck driver surveys.

## SUEJECT TERMS

geometric design, truck accidents, ramp configurations, truck driver surveys

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## Chapter One

## INTRODUCTION

Nationally, between $20 \%$ and $30 \%$ of freeway truck accidents occur near interchanges, even though these areas comprise less than 5\% of all freeway lane area (Firestine et al., 1989). "Freeways", as we define them here, are all limited access highways (i.e., interstate highways, expressways, tumpikes, and parkways). This percentage increases to $40 \%$ or more if accidents at intersections of ramps and arterial roads are included. These same percentages hold true for many western states. Of nearly 2400 freeway truck accidents in Colorado in the years 1993, 1994, and early 1995, roughly 30\% occurred at interchanges, and another 10\% occurred at intersections associated with interchanges. For accidents of all vehicle types, Sullivan (1990) found the number of interchange ramps along highway sections in California to be a significant explanatory variable of accident frequency per vehicle mile of travel.

Although driver actions (in both cars and trucks) most often cause highway accidents, inadequate interchange designs for large truck operations may contribute to some of them, along with insufficient safety wamings to commercial drivers at certain locations. Many interchange ramps throughout the U.S. were designed for older truck configurations and not for longer combination vehicles carrying much greater weights. Moreover, even some recently designed ramps do not adequately accommodate current truck configurations.

### 1.1 PROJECT OBJECTIVES

The objectives of this study were to:

1. Identify significant relationships between interchange design and large truck accidents in Colorado, Califomia, and Washington State. The discovery of such relationships will lead to proposed safety enhancements of interchanges in these and other states.
2. Critically examine the AASHTO Policy on Geometric Design of Highways and Streets (AASHTO, 1990) from the standpoint of truck operations at freeways.
3. Develop short-term and long-term strategies to mitigate problems at Colorado interchanges identified in the study.

### 1.2 PROJECT NEED AND BENEFITS

Truck accidents are a major consideration for govemment agencies regulating the design of these facilities. Findings from this project pertaining to design standards will be of important value to other states confronting this issue. The primary benefits sought by this project are to reduce accident risk to all motorists, reduce accident related impacts, and provide greater levels of service on the freeway system.

This project offers significant benefits to the general public as well as the trucking industry. In addition to the obvious risk to truckers, truck accidents are a significant safety risk and expense to highway users and nonusers. Truck accidents may involve other vehicles, cause traffic delays, increase insurance costs, reduce economic productivity, and may hurt the environment. Findings from this project, if used to address safety problems, may reduce future accidents, which translates into greater safety and reduced costs to the traveling public and the trucking industry. With increasing traffic congestion in urban areas, findings from this project can help to mitigate this problem, since improvements to interchange design for trucks will improve traffic flow for all highway users, both passengers and freight.

### 1.3 RESEARCH BACKGROUND

Previous studies have indicated that AASHTO design standards provide a slim margin of safety for the operation of large trucks through interchanges (Ervin et al., 1986). This degree of risk is attributed to the fact that some of the current geometric
design and operational criteria are based on the dimensions and operational characteristics of passenger cars. We'll later discuss current and future trends in truck design and technology, and re-evaluate current AASHTO standards pertaining to large truck operation at interchanges (AASHTO, 1990).

The complex relationship between highway geometrics and truck safety has been examined by numerous researchers, generally yielding mixed results. Difficulties with statistical analyses of truck accidents arise because of the large number of factors contributing to a truck accident, and the relative lack of information about "non-events". Some information is generally available from police accident reports about specific truck accidents, but limited data is available about all the non-accident traffic passing through these same locations.

| Surrounding Area |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Section Type | Rural | Suburb | Urban | Total |  |
| With Interchanges | 0.57 | 0.77 | 3.05 | 1.22 |  |
| Without Interchanges | 0.49 | 0.61 | 2.07 | 0.90 |  |

Note: Accident rates are per million vehicle miles, and include all accidents causing fatalities, injuries, and property damage only.

Table 1.1. Accident Rates on Controlled-Access Highway Sections (Pigman, 1981)

Accident rates vary widely by highway type, location, and by the study in which they are found. Table 1 shows some rates compiled by Pigman (1981) for interstate sections with and without bridges and interchanges. Differences in highway sections that affect accident rates are number of lanes, number of interchanges, number of bridges or tunnels, curvature, grade, and the mix of vehicle types. Although differences in these rates are also partly due to the classification of sample highway sections as freeways, expressways, or interstates, and the criteria by which they were defined to be rural, suburban, or urban, the rates are always greater when road sections with bridges and interchanges are included. An analysis by this research team of truck accident data
reported by Goodell-Grivas (1989) also showed that truck accident involvements were significantly higher on freeway sections in the vicinity of interchanges.

General accident rates per vehicle mile of travel (VMT) for all vehicles do not provide an adequate comparison of truck accident rates on different facilities. For both cars and trucks, studies have shown that fewer severe accidents per VMT occur on congested roads of similar design. Thus, on some highways, fewer accidents occur when greater traffic volumes generate greater VMT for some hours of the day. We designed this study to differentiate between accident rates for highways with different geometric designs and traffic characteristics.

### 1.4 OVERVIEW OF TASKS

Work on this study included (1) a review of past research on truck accident rates in general and truck accidents at interchanges in particular, (2) processing and manipulation of available data into tabulations needed to perform the above tasks, (3) description of altemative relationships to be evaluated, (4) presentation of statistical results, and (5) application of statistical results to procedures for identifying problem locations. The tasks were to:

### 1.4.1 Task A: Review Past Studies and Assess Available Data

Review literature on past research related to truck safety and highway geometrics.
Review Colorado accident data to identify potential study sites to examine.
Review Colorado traffic reporting system to identify truck exposure data (e.g., volumes, types, and primary routes).

Review HSIS, HPMS and other national data bases for additional truck exposure data and accident information.

Contact state DOT's and research institutes in other states to identify more detailed datasets.

### 1.4.2 Task B: Design Analysis Approach and Gather Needed Data

Develop list of key questions we sought to answer regarding truck accidents that we could investigate with data known to be available or obtainable within project resources and time.

Design database and statistical analyses to be performed once the data was assembled.

Develop survey form and survey procedure of truck drivers operating in Colorado to gain additional knowledge of truck safety issues at interchanges from the operators perspective and experience.

Distribute survey and follow-up requests in order to speed returns and ensure a sufficient return rate

Compile results and perform initial interpretation and assessment.

### 1.4.3 Task C: Assemble Databases and Perform Analyses

Select interchanges in each state where truck accidents were to be examined and used in statistical analyses.

Obtain geometric design drawings and truck accident reports at each selected interchange.

Input and process truck accident data pertaining to truck exposure, roadway characteristics, and traffic volumes for these sites.

Develop statistical companisons of truck accidents at interchange ramps of different geometric designs and traffic characteristics.

Produce preliminary report of findings, which described the sample design and data gathering process, methods of statistical analysis applied, and development of statistical comparisons.

### 1.4.4 Task D: Implementation

Apply the statistical findings to identify future accidents risk at selected sites.

Evaluate selected elements of the AASHTO geometric design criteria.

Develop short-term and long-term mitigation measures for select sites.

Produce Final Report describing the principal findings of the project.

An early task of this study was to assess whether national or state databases contained the detailed information on truck accidents needed perform the desired analyses. The Fatal Accident Reporting System (FARS), the National Accident Sampling System (NASS), and the General Estimates System (GES) from NHTSA were the first datasets we examined. Also, a survey of accidents in mid-1985 was collected for FHWA by seven states that may have included more detailed data on truck accidents and the locational attributes where these accidents occurred. We found that none of the national databases contained the detailed data we needed to investigate our questions conceming truck accidents as later described in Chapter 3.

We then surveyed the reports of several safety research institutes (e.g., the University of Michigan, the University of North Carolina, Midwest Research Institute, etc.) and State DOT's to identify more detailed datasets. Of the states we contacted, Washington State had assembled the most comprehensive truck accident database, with coded route mile point locations to cross-reference data files of highway geometrics and traffic volumes, including truck volumes on the ramps and in the freeway lanes. Colorado was able to provide limited data on truck accident at interchanges that we supplemented with data from police accident reports, but no traffic volumes. Califomia provided a dataset of truck accidents at interchanges with traffic volumes and interchange diagrams, but with no information on truck volumes.

In order to fit statistical models of large truck accident rates related to interchange geometrics and traffic charactenistics, we created a truck accident database for Washington State that included information about "safe travel" through
the same interchanges where truck accidents had occurred. We were not able to gather comparable information for Colorado and Califomia, but we were able to make some overall comparisons as shown at the end of Chapter 5.

## Chapter Two

## REVIEW OF TRUCK ACCIDENT STUDIES

The complex relationship between interchange geometrics and truck safety has been examined by numerous studies, generally yielding mixed results. The difficulties normally associated with statistical analysis of this relationship are attributed to the large number of interrelated factors contributing to accidents. These factors generally include human behavior, environmental conditions, and vehicle and roadway characteristics. The problem is further complicated by the lack of reliable exposure data on truck traffic at interchanges coupled with difficulties of obtaining detailed geometric design information. Earlier research efforts examined this relationship using different approaches and statistical techniques and yet because of the complexity of the issue and problems with obtaining reliable data no conclusive results have been drawn.

### 2.1 TRUCK ACCIDENT STUDIES IN GENERAL

A research group at Oak Ridge National Laboratory (Miau, et al., 1993) conducted extensive study of the relationship between truck accidents and roadway geometrics using Highway Safety Information System (HSIS) data base. The objective of the study was to determine the truck accident involvement rate and truck accident probability of a road section, given its geometric design, and other relevant characteristics. The authors of the study made a convincing case for using Poisson and Negative Binomial regression models to capture the relationship between accidents and geometric design variables, instead of conventional multiple linear regression models utilized by earier studies of similar relationships. It was found that HSIS was a comprehensive and well prepared data base containing useful information on accidents, vehicles, drivers, traffic and roadway geometrics. Each record of the road inventory file represents a homogeneous road section in terms of its cross-sectional characteristics, such as number of lanes, lane width, median type and width, annual average daily traffic (AADT)
and percentage of trucks. Each accident record contains information from accident reports which include information on accident type, severity, vehicle type, time of accident and drivers' condition. The database structure of HSIS makes it possible to link truck accident files with road inventory files and conduct various types of analysis. Although some encouraging relationships were developed for horizontal curvature, vertical grade, and shoulder width, using the Poisson regression models, the uncertainties associated with these models are still quite large, especially for the models for urban Interstate and freeway and rural two-lane undivided arterials. The authors of the study stress that these models are considered preliminary and need further refinements.

A 1989 study by Goodell-Grivas Inc. (Bowman, et al.,) concentrated on truck accidents on urban freeways. Although this study is not specifically focused on the question of large truck safety at interchanges it offers useful insights into the question of exposure and data accuracy which are in many ways applicable to the interchange environment. It also provided relevant statistics in classifying truck accidents by freeway area, which was subdivided into 5 (five) different categories:

Freeway Proper-76.9\%
Ramps-5.7\%
Right Hand Merge-9.2\%
Right Hand Exit-5.5\%
Left Hand Merge/Exit-2.7\%

This break down of truck accidents by the freeway area shows that $23.9 \%$ of all truck accidents take place around interchanges. This data corresponds well with other studies which isolated truck accidents at interchanges.

### 2.2 TRUCK ACCIDENT STUDIES AT INTERCHANGES

A recent study by Garber et al., 1992 examined large truck accidents on ramps in Virginia. This study concentrated on identifying vanables that are of statistical
significance to occurrence of large truck accidents on ramps. A major deficiency in the data compiled, according to the authors, was the unavailability of the Average Annual Daily Traffic (AADT) and truck volumes on ramps. The difficulty with ascertaining truck exposure on ramps is not unique to the State of Virginia or the latest study by Garber et al., as this kind of information is not systematically collected by the Departments of Transportation and is generally not readily available. The question posed by Garber et al., was-what is a representative measure of truck exposure at interchanges in the absence of truck volumes on ramps, and what information should be collected in order to diagnose safety problems for trucks?

In order to identify problem areas Garber conducted detailed investigation of 16 interstate routes and 21 primary routes. As a result of this investigation a route was identified with the highest number of truck-related accidents on ramps. It is of interest to note that the selected route had neither more interchanges nor truck exposure as measured in truck Vehicles Miles of Travel (VMT) than some of the other routes in Virginia. Garber concluded that this overrepresentation might be attributed to restrictive geometrics coupled with the design speed differential between the main line and the ramp; however this inference was not conclusively proven in the study. It is also difficult to find a reasonable explanation as to why the entire route rather than isolated locations display unusually high number of truck accidents. This study offers an innovative measure of assessing truck safety on ramps by introducing the involvement ratio of truck accidents on a ramp to total number of accidents in the same section where the ramp is located. Garber et al., showed that the involvement ratio of trucks on ramps increases with the speed differences between the average speed of trucks approaching the ramps and the posted speed limits. Some of the other significant findings of this study are as follows:

- A higher percentage of truck accidents on the interstate highways occur at exit ramps. On primary highways, a greater percentage occur on entry ramps.
- Trucks at interchanges are not significantly involved in non-collision accidents, such as jacknifing, rollovers and run-off-the-roads accidents.
- Sideswipe-same direction collisions were predominant at entry ramps on the interstate system.
- At the exit ramps on the interstate system, rear-end and sideswipe same direction collisions were predominant.

Probably the most interesting finding of this study was the fact that a high occurrence of ramp accidents on the selected route was not due to either the truck VMT or the number of interchanges located on the highway. This finding presents some unique possibilities for further and more detailed study of this route in the future.

A major work examining the relationship between specific geometric features of interchanges and loss-of-control accidents involving large trucks was done at UMTRI in 1986. (Ervin et al.,). This thorough and innovative study of the relationship between geometrics and large truck accidents integrated statistical analysis with computer simulation of the interaction between the roadway and the vehicle. It is relevant to note however that this research effort concentrated on single vehicle rollovers, jackknifing and run-off-the-road accidents which constitute less than 6\% of all large truck accidents at interchanges.

In the absence of the reliable truck exposure data on ramps, the UMTRI team used the files from the FHWA Office of Motor Camiers as a convenient data set for comparing States. The proportion of truck accidents which occurred on ramps was used as a measure of overrepresentation or ramp-related truck accidents. However, this did not account for the proportion of travel which was on ramps or the relative number of interchanges per mile of highway. A number of regressions were used to examine measures of overrepresentation of ramp accidents among the States using the highway mileage and population. Ten candidate States were selected as a result of this analysis. The DOT in each State was asked to identify approximately six ramps which have had a substantial involvement of large trucks in ramp accidents. The selection was to be based on overinvolvement relative to average daily traffic, or on large number of accidents if the truck ADT were not available. The responses of the States were
positive but varied in details and led to the selection of 15 ramps at 11 interchanges in 5 States.

Ervin et al., used a simulation model developed by UMTRI to represent the dynamic response of the trucks along each of the selected ramps. The UMTRI model, which is capable of representing the behavior of commercial vehicles ranging from straight trucks to triple combinations, was used to diagnose specific problems which led to the loss-of-control of the vehicle. Dynamic simulation of commercial vehicle responses to ramps with a history of accidents showed that the leading vehicle-related causes of loss-of-control are as follows:

- Low roll stability
- High speed offtracking
- Limitations in braking control
- Difficulties in controlling speed on short downgrades
- Limited acceleration ability for effective merging and weaving

Geometric design features of the ramps identified in the UMTRI study which precipitated conditions leading to a loss-of-control are as follows:

- Poor superelevation transition on curves creates high levels of side friction demand that increase the threat of rollover.
- Abrupt changes of curvature in compound curves which often places excessive demands on the driver leading to rollovers.
- Short deceleration lane leading to tight-radius exit also places excessive demands on the driver and increases the possibility of jackknifing because of excessive braking or rollovers due to loss of control.
- Curbs placed on the outside of a ramp curve found to serve as a tripping agent in rollover accidents.
- Downgrade leading to a tight curve may lead to rollovers due to inability to decelerate adequately prior to negotiating a curvature.
- Reduced pavement friction on high-speed curves in wet weather leads to hydroplaning of lightly loaded trucks and subsequent loss-of-control problems.

A 1993 study Ramp Signing for Trucks by Knoblauch and Nitzburg addressed methods for identification and treatment of ramps with geometric characteristics that can cause trucks to overturn. The emphasis of this study is on ramp signing design which would alert the drivers of rollover potential. The study showed that although many States have developed specific treatments for locations with truck rollover problems, there are no specific procedures to identify those locations except waiting for truck rollover accidents to occur. The authors make an assertion that this approach is not as irresponsible as it may first appear because serious truck rollover problems are relatively rare. Unlike other studies this effort directly involved truck drivers in the process to obtain their perception of the problem and identify solutions. The authors conducted the "design-a-sign" experiment with 61 professional drivers to identify most effective sign design features which convey waming of potentially dangerous ramps. This experiment suggests that signs which perform best include the following elements:

- Rear silhouette of a tipping truck
- Diagrammatic curve arrow
- Advisory speed limit
- Word legend - "ROLLOVER HAZARD"
- Word legend - "TRUCK CAUTION"

The laboratory studies aiso clearly indicate the desirability of using advance signing located well before the ramp and the desirability of using flashing light in combination with these signs.

### 2.3 STUDIES EXAMINING THE RELATIONSHIP BETWEEN DESIGN STANDARDS AND TRUCK CHARACTERISTICS

A 1990 study by Harwood et al., presented the most thorough examination to date of Truck Characteristics for Use in Highway Design and Operation. The objectives of this study were as follows:

- Identify those highway design and operational criteria that are sensitive to truck performance characteristics.
- Determine the adequacy of those criteria for trucks.
- Develop and assess new criteria for those situations where the current criteria do not adequately address the current or future truck population.

The study was primarily analytical in nature with only occasional measuring or testing of the vehicles. Harwood et al., identified 16 highway design criteria based on vehicle characteristics. Each criterion was then evaluated to assess its adequacy for the fleet of large trucks. In the process of evaluation, the authors presented a sensitivity analysis for each criterion to the changes in truck characteristics associated with vehicle evolution.

Some of the selected findings from this study related to the criteria used in interchange design are presented below:

Current AASHTO criteria are not adequate to accommodate trucks with conventional braking systems and poor performance drivers. Many drivers have little experience with the proper procedures for controlled braking in emergency situations.

Trucks may require 100 to 400 ft more decision sight distance than passenger cars at a design speed of 70 mph , and lesser amounts of additional decision sight distance at lower design speeds.

The higher driver eye height for trucks offsets the increased decision sight distance requirements in most cases at vertical sight restrictions, but not at horizontal sight restrictions.

A change in decision sight distance criteria to accommodate trucks by using longer vertical curves on the approach to major decision points would be cost effective only in unusual situations with extremely high accident rates.

Based on the Gillespie (1986) model for intersection clearance times, the larger trucks currently on the road require up to 17.5 percent more sight distance for an intersection crossing maneuver than the current AASHTO criterion based on a WB-50 truck.

Trucks with conventional brake systems may require sag vertical curves up to 670 ft longer than current AASHTO criteria.

Current AASHTO criteria for horizontal curve radius and superelevation at particular design speeds are adequate to accommodate trucks. The existing criteria provide margins of safety against skidding off the road and against rollover that are substantially lower for trucks than for passenger cars.

Current superelevation transition methods appear adequate to accommodate trucks. Use of spiral transitions is preferable to the traditional 2/3-1/3 rule.

Increased emphasis is needed on the realistic selection of design speeds for horizontal curves, particularly on freeway ramps. It is critical that design speeds selected for off-ramps are consistent with the design speed of the main line highways. It is recommended that the lower range values of ramp design speeds presented in the AASHTO Green Book not be used for roadways that carry substantial volumes of truck traffic.

Revised criteria for pavement widening on horizontal curves are needed to accommodate STAA single 48 -ft semitrailer trucks.

Advance warning sign criteria for trucks with conventional brake systems should be longer than the current criteria which are based on consideration of passenger cars.

The highway design and operational criteria examined in the study included geometric design policies based on the 1984 AASHTO Green Book and the 1988 edition of the Manual on Uniform Traffic Control Devices for Streets and Highways (MUTCD). Since the publication time of the Harwood et al., study there were 2 new editions of the Green Book, in 1990 and in 1994. While the 1994 edition primarily addressed the question of metrification, the 1990 Green Book introduced additional design vehicles for incorporation into the geometric design criteria. These design vehicles have longer wheel bases and greater minimum tuming radii. They include tractor-trailer combinations listed below:

- Interstate Semitrailer WB-62, Design vehicle with 48' trailer as adopted in 1982 Surface Transportation Assistance Act (STAA).
- Interstate Semitrailer WB-67, Design vehicle with 53' trailer as grandfathered in 1982 (STAA).
- Triple Semitrailer WB-96
- Tumpike Double Semitrailer WB-114

The Green Book states that the facility must be designed to accommodate the largest vehicle likely to use it with considerable frequency, but it leaves a great deal to the discretion of the individual design engineer by not defining what a considerable frequency is. Although tumpike doubles and triple trailers are not permitted on many highways, their occurrence warranted inclusion of these vehicles in the Green Book. Inclusion of these vehicles into the 1990 edition of Policy on Geometric Design of Highways and Street does not automatically spell out the retrofit of older interchanges which present most of the problems for larger trucks.

According to a survey jointly conducted by AASHTO and DOT (The Feasibility of a Nationwide Network of LCV's, FHWA 1986) "...a majority of interchange ramps had inadequate geometry to accommodate the off-tracking of some larger combinations. State DOTs estimated that approximately 43 percent of the Interstate interchanges could safely accommodate triples, 34 percent could accommodate Rocky Mountain doubles and only 25 percent could accommodate tumpike doubles. State DOTs also estimate that only one half of all Interstate Interchanges can safely accommodate WB-62 Interstate Semitrailer with 48 ft trailer."

Another significant development which influences the relationship between vehicle performance and highway design standards is recently passed legislation proposed by NHTSA on the antilock braking system and maximum stopping distance requirements for heavy trucks. 49 CFR Part 571 requires medium and heavy vehicles to be equipped with an antilock brake system to improve directional stability control of these vehicles while braking. By improving directional stability and control, these requirements will significantly reduce deaths and injuries caused by jackknifing and other losses of directional stability and control during braking. It also specifies distances in which different types of medium and heavy vehicle configurations must come to a complete stop from 60 mph on a surface with peak friction coefficient (PFC) of 0.9 . These requirements are designed to reduce the number and severity of crashes involving trucks and buses.

The requirements set forth in the 49 CFR Part 571 pertaining to ABS and maximum braking distances apply only to new trucks and buses and will not require retrofit of the existing vehicle fleet. While these changes will go a long way in improving truck safety it is important to realize that this change will take place gradually and over time.

## Chapter Three

## STUDY DESIGN AND ANALYSIS APPROACH

### 3.1 OVERVIEW OF ANALYSIS APPROACH

Taking into account data availability and previous research, the primary objectives we sought to achieve in the data gathening and statistical analysis steps of this project were to:

1. Identify requirements of a comprehensive truck accident database to be used for highway improvement studies as part of a state's safety management system.
2. Statistically compare truck accident experiences of many different ramp designs in three states (Colorado, Califomia, and Washington) so as to examine the effects of their design on interchange safety and recommend possible design improvements.
3. Develop a procedure to identify "high risk" locations for remedial action to improve safety using this truck accident database.
4. Include the experiences and observations of truck drivers and fleet managers to identify and assess problem locations, and to develop candidate safety improvements and risk mitigation strategies.

We tackled several research issues during the study such as (i) how to best estimate missing data from available information, and (ii) how to best use the available and estimated data to validly compare and contrast the accident experiences of different ramp geometric designs and traffic charactenistics. We later explain the methods used in this study to address these issues.

We identified the following data as the minimum requirements of a truck accident database needed to make statistical companisons of ramp accident experiences and to
recommend potential improvements. We then obtained these data (to the extent possible) for truck accidents at interchanges in each state.

1. General Location Identifiers
interchange type (e.g., diamond, directional, etc.).
ramp type (e.g., diamond, loop, directional, etc.).
ramp connection type (freeway-to-freeway, freeway-to-arterial, etc.).
conflict area (e.g., merge, diverge, upstream, downstream, etc.).
accident location-(route mile post) and direction of travel.
main and secondary route identifiers (perhaps both freeways).
highway lane or ramp section in which accident occurred.
2. Traffic, Road, and Accident Characteristics
numbers and types of vehicles involved.
fatalities, injuries, and property damage.
date, time-of-day, road and weather conditions.
accident type (e.g., sideswipe, rearend, rollover, etc.).
length of merge/diverge area from taper to gore (or vice-versa). length of ramp from secondary connection to merge/diverge area. distance of accident upstream from center of merge/diverge area. distance of accident downstream from center of merge/diverge area. average daily traffic and truck percentage on the main line (MADT). average daily traffic and truck percentage on the ramp (RADT).

We needed "ramp truck ADT" (RTADT) as a measure of truck exposure at each ramp in order to compare truck accident rates by ramp design. Although ramp truck ADT's are not generally available, WSDOT was able to provide ramp truck ADT's that coincided with the study period for over 250 ramps. This sample allowed us to estimate ramp truck ADT's where missing based on the ramp ADT's of all vehicles. We explain our estimation of ramp truck ADT's further in Chapter 4.

### 3.2 ACCIDENT COMPARISONS OF INTEREST

Below are listed the key questions that we investigated on truck accidents at interchanges for Colorado, California, and Washington.

1. Do numbers of truck accidents or truck accident rates per truck trip or truck VMT (vehicle miles of travel) differ by ramp type, conflict area, or the combination of these two classifications?
2. Do these findings differ significantly by accident type?
3. Do these findings differ significantly by high, medium, or low ADT of trucks or all vehicles on the ramps or in the main freeway lanes due to greater lane-changing difficulties at higher volumes or the risks of greater speeds at lower volumes?
4. Do these findings differ significantly both upstream and downstream of the merge/diverge area?
5. Do these findings differ significantly for different lengths of the accelddecel lanes plus tapers?

We'll discuss data availability from each state in explaining our data collection procedures in Chapter 4. Because some required data elements were unavailable from both Colorado and Califomia, we were only able to investigate all the above questions for Washington, and still needed to estimate some data elements such as ramp truck ADT's. In Chapter 7, we recommend future data collection by state DOT's for safety management systems.

In our analyses, we were careful to distinguish between accidents either (1) on the ramps, or (2) on the main freeway lanes near the ramps. In preparing our truck accident database, we distinguished all accidents at intersections connecting ramps to arterials, and excluded all intersection accidents from our accident companisons.

We compare accident frequencies and rates by (i) numbers of ramp locations, (ii) truck trips on these ramps, and (iii) truck travel distances at these locations by (a) ramp type, (b) conflict area, and (c) accident type. These multiple comparisons allow us to examine the separate effects of location, truck use, and travel distance. Comparing truck accidents per ramp truck trip (RTT) is similar to comparing intersection accidents per "vehicle entered" where types and numbers of conflict points are more important than travel distances. Although ramps involve greater travel distances than intersections, most accidents occur near conflict points, where numbers of vehicles passing may be more critical than vehicle miles of travel. To examine travel distance effects, we compare accident rates per ramp truck trip and per ramp truck VMT. We discuss this point further in Chapter 4.

### 3.3 TRUCK DRIVERS' SURVEY AND FOCUS GROUP

High percentage of truck accidents concentrating in and around relatively small areas of interchange influence identified a need for additional information relating to difficulties of navigating a large truck through an interchange. In the opinion of the study team, important insight into this phenomenon can be gained from discussing this issue with truck drivers and safety managers themselves. In order to develop greater understanding of the relationship between truck accidents and the geometric design of interchanges the study team has developed and administered a series of surveys targeting truck drivers and safety managers operating in Colorado.

The first survey was administered at the annual Truck Rodeo in Denver and provided input from 84 truck drivers. The drivers filled out a survey form asking them to identify five interchanges most difficult to travel, and indicate reasons why using a rating scale of 1 through 5.

The second survey was administered at the monthly safety managers meeting of the Colorado Motor Carrier Association (CMCA). The second survey form itself was somewhat modified to better reflect the specifics of the group and to incorporate the knowledge gained in the survey administration at the Truck Rodeo. Only 13 safety
managers filled out the second survey. Survey forms, a statistical summary of responses and focus group results are available in the appendix.

The results of both surveys identified a very broad spectrum of factors contributing to truck accidents as well as a long list of "difficult" interchanges as perceived by the drivers and safety managers. It is apparent from the statistical summaries of both surveys that opinions expressed by the participants were highly divergent and did not identify well pronounced trends in truck accident causality, nor did they exhibit locational consistency. The study team attributes this diversity of opinions to the heavy routespecific bias of survey participants. In other words, there is a natural tendency to have the best recollection of the most recent accident event or most recently traveled route. This phenomenon is known as availability bias. Furthermore little correlation was found between the "worst" interchange locations identified in the surveys and "worst" accident locations identified through statistical analysis of the accident history by the study team. In order to overcome the availability bias the study team used a Focus Group approach to gathering information from truck drivers and safety managers.

A group of 10 individuals representing a cross section of truck drivers and safety managers was presented with the layouts of 14 "worst" interchanges identified through statistical analysis of large truck accident history at interchanges in Colorado over the last 3 years. The focus group was then asked to point out the difficulties of driving a large truck through each interchange and identify possible strategies for improvement. The focus group's input and design drawings of problem interchanges are included in the appendix with the summary list of the improvements recommended by the focus group participants provided below:

- Improve maintenance of striping in high volume areas
- Provide more advanced signing
- Provide recommended speed signs on ramps directed at truck traffic
- Improve clanity of overhead signs
- Provide brighter sign panels with flashing lights
- Include schematic diagrams of interchange configurations on signs
- Redirect trucks to easier ramps if possible
- Provide additional education to truck drivers with respect to interchanges and ramps
- Install rumble strips in gore areas to alert drivers
- Improve overall visibility and communication through signing

As is evident from the above summary list, the most frequently expressed concem during the focus groups' session pointed to the inadequacy of waming and guidance provided to the truck drivers in problem areas. This observation can be interpreted as such: accidents often are not attributed to some specific geometric design features or feature which when present are sure to cause a crash involving a large truck at an interchange, but rather to a discrepancy between what the driver expects and what he actually encounters on the road. This phenomenon is known as the driver expectancy violation. Expectancy relates to driver's readiness to respond to situations, events, and information in predictable and successful ways. Aspects of the highway situation that match prevalent expectancies aid the driving task, while expectancies that are violated lead to longer reaction times, confusion and driving error. Violations of driver expectancies effect trucks even more adversely than passenger cars because of their dimensions and operating characteristics.

The case history at a rural interchange in northem Colorado illustrates this point rather well. At this location restrictive geometrics not expected in the open rural environment led to a series of single truck rollovers. Having identified this problem using statistical analysis and following the discussion with the focus group, the CDOT designed and installed waming signs to alert the truck drivers. In order to evaluate the effectiveness of the countermeasures applied at this location an observational before-and-after study was conducted. The results of the study are available in the appendix.

Another example of the driver expectancy violation can be observed at an interchange in an urban area of Colorado where the truck drivers are presented with a left-hand merge onto the freeway. Although a continuous lane is provided the truckers are anxious to change lanes in anticipation of a lane drop, which leads to an unusually high number of sideswipes.

Another problem identified by the focus group participants was signing and striping at interchanges. In response to this concern the study team initiated review of signing at selected interchanges with the CDOT Staff Traffic Branch. Following the review we observed that inadequate interchange spacing at the selected interchange sites complicates signing and often leads to accidents. As a result, interchange spacing was introduced into the data-set of geometric characteristics for further analysis.

In the process of review of selected interchange locations by the CDOT Staff Traffic Branch, it has been discovered that a substantial number of accidents were influenced by the on-going construction in the areas adjacent to interchanges as well as temporary phase-construction conditions. The presence of these factors affected the degree of significance we can attribute to these observations.

The focus group session combined with statistical analysis of accidents involving large trucks made it more apparent that the effects of specific geometric design features are better understood within the context of an interchange environment. in order to capture driver expectancy violations future research efforts should focus on interchanges with similar configurations operating in similar environments. This comparative analysis represents an important area of future research and may explain why one location is safer than the other by concentrating on specific features, which may include geometric characteristics as well as signing.

## Chapter Four

## DATA ACQUISITION AND PREPARATION

### 4.1 TRUCK ACCIDENT DATA SOURCES

The primary source of truck accident data in most any state is the state DOT, although it may be necessary to supplement the DOT data with data from police accident reports. Of the states we contacted, Washington State DOT (WSDOT) had compiled the most complete accident database, with location codes to cross-reference their computer files for traffic and geometric data. The accident recording systems in Colorado and Califomia were not as advanced or complete at the time.

It's important to know an accident's location so as to identify its roadway and traffic characteristics. However, it's often difficult or impossible to determine exactly where an accident occurred from some accident databases. Accidents in interchange areas can occur:

1. On a ramp away from a merge/diverge area or intersection.
2. On a secondary road to which the interchange connects.
3. On a ramp, but at the junction of multiple ramps.
4. At an intersection of the ramp with a secondary road.
5. In the accel/decel lane of a merge/diverge area.
6. In the freeway through-lane adjacent to the accel/decel lane.
7. In the other freeway through-lanes of a merge/diverge area.
8. In the freeway lanes upstream of a merge/diverge area.
9. In the freeway lanes downstream of a merge/diverge area.

Once an accident's location has been identified, then other roadway data must be obtained for the same location. Invariably, the route mile post of an accident (to
whatever accuracy it is known) must be used to "match" traffic and geometric data (if available) with the accident's location. It can require much time to match and compile data for each accident, even if data are in electronic form. Until state DOT's have more automated safety management systems, linking data in existing files is quite often difficult because of how the data is indexed and recorded.

### 4.2 DISCUSSION OF DATA DEFICIENCIES

The current situation in most state DOT's is that much data either doesn't exist or is not in computer files. Using (i) interchange drawings with route mile points, (ii) a concurrent file of highway geometrics, and (iii) police accident reports, it may be possible to identify the basic highway geometrics of each accident location such as lane widths, shoulder widths, ramp lengths, and taper lengths. We were able to identify these basic geometrics for most truck accident locations in Washington, but only for select locations in Colorado and Califomia. We were not able to obtain several other important highway geometrics such as grades, curvatures, and sight distances for any state.

Due to data deficiencies, the issue of defining and obtaining the appropriate truck exposure measure was quite difficult to resolve. Ideally, we would like to know truck and car volumes passing the accident location at the time of the accident. Hourly volumes are generally not available, but WSDOT did provide us with ADT's for most roads and ramps where truck accidents occurred. Thus, we used ADTs to estimate exposure, assuming that time-of-day traffic volume and mix variations do not significantly effect accident rates. We have limited evidence from another FHWA truck accident database that time-of-day traffic variations have some, but less-than-significant effects on accident rates per vehicle passing.

Collecting a comprehensive truck accident database for Colorado and Califomia comparable to the WSDOT data was far beyond the resources of this study. Without performing our own on-site surveys, the data available from those states is much less complete regarding accident locations, traffic volumes on the main lanes or ramps, and geometric characteristics of the ramp area. Our efforts to identify and obtain the data
we needed from Colorado and Califomia helped us to design and assemble our dataset for Washington more efficiently.

We decided to emphasize the use of Washington State data because it contained (i) ADT's on the main lanes and ramps at each interchange, (ii) truck ADT's for some ramps, and (iii) computerized drawings with route mile points, accident locations, and the general geometry of each interchange. Other accident characteristics such as number of vehicles, actions of drivers, weather conditions, and extent of injuries were linked by accident ID number to another data file.

A paramount concem was to obtain ramp truck ADT's for a sufficient number and variety of ramps where truck accidents did not occur so as not to underestimate the truck exposure of any ramp type. It was beyond the scope of this study to obtain ramp truck ADT's for all Washington ramps via a special collection effort. However, the ramp truck ADT's that we did obtain or estimated to satisfy our study design automatically included a sufficient coverage of conflict areas at ramp locations where accidents did not occur to control for this potential bias.

The next section describes our compilation of a truck accident database for Washington. We summarize our preparation of datasets for Colorado and Califomia at the end of this chapter, emphasizing what we did differently because of data availability. We were not able to obtain any ramp truck ADT's for Colorado or Califomia with which to compare truck accident rates per ramp truck trip or VMT, and instead compare truck accidents per ramp location in these states. Since ramp truck ADT's are not generally available from most states, we explain in Chapter 6 how accident frequencies per location can be used to identify high-risk locations.

### 4.3 PREPARATION OF THE WASHINGTON DATABASE

This section describes the truck accident database that we compiled from information sent to us by WSDOT. Section 3.2 listed the key questions regarding truck accidents that we sought to answer with this data. This database includes data for all
truck accidents at all interchanges in Washington over the 27 months from January 1, 1993 to March 31, 1995.

WSDOT maintains very comprehensive accident and traffic data for their state highways. Except for ramp truck ADT's, very few data elements pertinent to this study were missing for any truck accidents near interchanges. The route mile point of each accident is provided to within ten feet accuracy. Using interchange drawings with route mile points and a corresponding file of highway geometrics, we were able to identify the basic highway geometrics of each truck accident location such as lane and shoulder widths, ramp and taper lengths, and lengths of accel/decel lanes. As mentioned earlier, we were not able to obtain other highway geometrics such as grades, curvatures, or sight distances.

We assembled our dataset from five basic data files provided by WSDOT. These were:

1. A computer listing of truck accident characteristics at interchanges containing the data elements listed in Table 4.1 (approximately half of the data elements in WSDOT's database listed here).
2. A computer listing of freeway ADT's by route mile post (see Table 4.2 for an example page of this listing).
3. A computer listing of ramp ADT's by route mile post (see Table 4.3 for an example page of this listing).
4. A computer listing of geometric design characteristics by route mile post (see Table 4.4 for an example page of this listing).
5. Computer drawings of each interchange with truck accident locations indicated by route mile post (see Figure 4.1 for an example of these drawings).

Using each accident's route mile post as its common identifier in each computer file, we were able to combine the data in the above files into one database. We
excluded all accidents on secondary roads or ramps at intersections, but included all freeway-to-freeway accidents. If the route mile posts of two or more accidents were very close, then their traffic characteristics and highway geometrics were similar. However, based only on route mile posts, it was often difficult to determine whether an accident specifically occurred in the freeway lane or the accel/decel lane of a ramp connection area. Although the WSDOT dataset did include a lane identifier for each accident, we decided for this study to group all accidents into four separate conflict areas as defined in Chapter 5. Hence, we grouped all accidents in or adjacent to accel/decel lanes as being in ramp connection areas as defined in Chapter 5.

Merging data from the above five files into one file is more easily done if available in electronic form. We re-entered the data from hardcopy listings due to some format difficulties. Although this effort was labor intensive, we were able to verify and crosscheck the data as we entered it. In select cases where a piece of data (such as an ADT value) was missing, the process often allowed us to obtain the missing value from another accident record previously entered for the same location.

In summary, the accident data that we directly extracted from the WSDOT computer files and coded into our database for each accident were:

1. Accident location (route mile post) and direction of travel.
2. Main and secondary route identifiers (perhaps both freeways).
3. Accident type (e.g., sideswipe, rearend, rollover, etc.).
4. Freeway lane number or place on ramp where accident occurred.

Accident data that were not directly available from the WSDOT computer files, but which we added to our database based on our interpretation of the WSDOT data and drawings of interchanges, were:

1. Interchange type (e.g., diamond, directional, etc.).
2. Ramp type (e.g., diamond, loop, directional, etc.).
3. Ramp connection type (freeway-to-freeway, freeway-to-arterial, etc.).
4. Conflict area (e.g., merge, diverge, upstream, downstream, etc.).

We started with detailed differences in interchange and ramp design, and then condensed our classification into fewer categories so as to disregard small differences and not have too few observations in any one crossclassification. Our accident comparisons in Chapter 5 are mainly made between different ramp types and conflict areas. Figure 4.2 shows the four basic ramp types by which we classified all truck accidents, and we define the conflict areas of each ramp by which we also classified these accidents in Chapter 5.

Lastly, using a printout of traffic counts and geometric drawings by route mile post, and a supplemental list of 250 ramp counts with truck percentages, we added to our database the additional accident characteristics listed below.

1. Length of merge/diverge area from taper to gore (or vice-versa).
2. Length of ramp from secondary connection to merge/diverge area.
3. Distance of accident upstream from center of merge/diverge area.
4. Distance of accident downstream from center of merge/diverge area.
5. Main road average daily traffic (MADT) and truck percentage.
6. Ramp average daily traffic (RADT) and truck percentage.

| Field ${ }^{\text {\% }}$ | Accident Data Elenents |
| :---: | :---: |
| 1 | Year |
| 2 | Month |
| 3 | Day of Month |
| 4 | Day of Week |
| 5 | Hour |
| 6 | Minute |
| 7 | County Number |
| 8 | City Number |
| 9 | State Route Number |
| 10 | State Route Milepost |
| 11 | WSDOT District Number |
| 12 | UrbanRural Location |
| 13 | Functional Class of Road |
| 14 | Accident Severity |
| 15 | Number of injuries |
| 16 | Number of Fatalites |
| 17 | Most Severe Injury of Accident |
| 18 | Number of Vehteles tr Acoident |
| 18 | Amount of Propery Damage (\$) |
| 20 | Character of Roadway |
| 21 | Location of Roadway |
| 22 | Roadway Surface Conditions |
| 23 | Weather Conofitions |
| 24 | Light Conditions |
| 25 | Ramp Location |
| 26 | Vehicle 1's Movement |
| 27 | Diagram Accident Type |
| 28 | Vehicle 2's Movement |
| 29 | Impact Location |
| 30 | Colision Type |
| 31 | Object Stuck |
| 32 | Acodent Occumed On or Off Road |
| 33 | Driver 1's 1st Contributing Cause |
| 34 | Diver 1's and Contributing Cause |
| 35 | Driver 2's ist Contributing Cause |
| 36 | Driver 2's 2nd Contributing Cause |
| 37 | Diver 5 s ist Contributing Cause |
| 38 | Ditver 3's 2nd Contributing Cause |
| 39 | Driver 1\% Vehicle Actions |
| 40 | Driver 2 's Vehicle Actions |
| 41 | Drver 3's Vehlide Actions |
| 42 | Vehide 1's Type |
| 43 | Vericle 2's Type |
| 44 | Vehicle 3's Type |
| 45 | Most Alcohol impaired Driver |
| 46 | Driver 1\% Age |
| 47 | Oriver 2's Age |
| 48 | Driver 3's Age |
| 49 | Hazardous Materials Being Transported |
| 50 | Fuel Spilage Due to Comision |
| 51 | Pedestrian/Pedalcyclist 1's injury |
| 52 | Pedestrian/Pedalcyclist 1's Age |
| 53 | PedestrianPedalcyelist 1\% Actions |

Table 4.1: Listing of Washington State Accident Data elements
state de hashingiton

| sTATE <br> MTLEPOST <br> LOCATIOn |  | couplet class |  |  |  |  | AYERAGE OAILY TRAPFIC VOLUME |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | tauck percentages SNGL OBL TRIPLE TOTAL | $\begin{array}{r} 1991 \\ \text { UNITS } \end{array}$ | 1992 UMITS | UNITS | UNITS |
| 016.31 | after mamp SR 900 |  | 5 |  |  |  |  | 47000 | 49000* | 50000 | 57000* |
| 017.69 | after mamp 220 th ave se | 8 |  |  |  |  | 28000 | 33000* | 33000 | $35000 \cdot$ |
| 018.38 | after ramp e sunset way | 5 |  |  |  |  | 32000 | 35000 * | 38000 | 37000 * |
| 020.79 | after ramp mioh moint ro | 5 |  |  |  |  | 33000 | 34000* | 35000 | 38000* |
| 023.34 | at ade lotation sbzo | 5 |  |  |  |  | 29000* | 31000 - | $31000 *$ | 33000* |
| 026.11 | after mamp sp to | 5 |  |  |  |  | 40000 | 44000 * | 48000 | 45000* |
| 030.23 | DEPORE RAMP 5R 202 | 5 |  |  |  |  | 370004 | 33000* | 34000 | 35000* |
| 031.00 | APTER RAMP SR 202 | 5 |  |  |  |  | 27000* | 32000* | 33000 | $31000 *$ |
| 033.56 | at ade location rose | 5 |  |  |  |  | 240Q0* | 25000* | 28000* | 27000* |
| 035.00 | aFter ramp todewtck rd | 5 |  |  |  |  | 20000* | 26000* | 24000* | 28000* |
| 041.75 | before ramp tinkham ro | 5 |  |  |  |  |  |  |  | 28000* |
| 047.98 | after mamp tinkham ho | 5 |  |  |  |  | 23000 | 20000* | 21000 | 25000* |
| 091.8日 | BEFDRE RAMP SR 906 | 5 |  |  |  |  | 20000* | 21000 | 22000 | 22000 |
| 051.00 | after ramp sh 906 | 5 |  |  |  |  | $19000{ }^{\circ}$ | 20000 | 20000 | 23000* |
| 082.61 | Defder mamp e summit ro | 5 |  |  |  |  | 22000 | 24000 | 24000 | $23000 *$ |
| 081.34 | BEFORE PRICE CREEK REST AREA | 5 | 04 | 13 | 04 | 21 |  | $21000+$ | 23000 | 25000 |
| 084.23 | after mamp cadin creek ro | 5 |  |  |  |  | 18000* | 19000 | 20000 | 21000 |
| 070.60 | After ramp west easton ro | 5 |  |  |  |  | 17090* | 18000 | 21000* | 23000 |
| 073.04 | defore ramp w helson no | 5 | 04 | 14 | 04 | 22 | 16000 | 19000* | 20000 | 22000 |
| 078.80 | at yakima river briose | $B$ | 05 | 12 | 04 | 21 | 210004 | 22000 | 22000 | 24000 |
| 082. 70 | at moc location boa | 5 |  |  |  |  |  | 20000* | 21000* | 22000* |
| O84. 20 | at oakes ave | 5 |  |  |  |  |  |  | 20000* | 21000 |
| 088.06 | at anc location moob | 5 |  |  |  |  | 17000* | 18000* | 18000* | 19000* |
| 086.10 | AFtER RAMP SA 970 | 6 | 05 | 14 | 05 | 24 | 13000 | 17000* | $21000 *$. | 20000* |
| 094.02 | APtER RAmp ELK meiohts | 5 | 05 | 18 | 05 | 26 | 18000 | 16000* | 18000 | 17000 |
| 101.48 | after ramp thorf ro | 5 | 04 | 14 | 0.5 | 23 | 18000 | 18000* | 18000 | 19000 |
| 106.33 | AFtEA Ramp 38 97 | 5 | 04 | 13 | 05 | 21 | 18000 | 18000 | 19000* | 20000 |
| 109.89 | after ramp s majn st | 5 |  |  |  |  | 18000 | 20000* | 20000 | 21000 |

STATE OF WASHINGTDH - DEPARTY
INTERSTATE - ISSH COUNIY KITTITAS

DOT DISTRICT 5



Figure 4.1: Sample Interchange Drawing with Truck Accident Locations by Mile Post


Figure 4.2: Four Basic Ramp Types

### 4.4 DEFINING THE RAMP INFLUENCE ZONE

An important issue concerning accidents that were possibly affected by facility design characteristics is to define the area boundaries within which such effects are thought to be significant. To study ramp design effects, we defined this influence zone
to (i) exclude intersections with arterials, (ii) be mainly confined to accidents either on the ramp, in the accel/decel lane of the ramp, or in the highway lane adjacent to the accel/decel lane of the ramp, and (iii) be within a certain upstream or downstream distance from the ramp that we next define.

One question posed in Section 3.2 concemed the effects on truck accident frequencies of upstream and downstream distances from a ramp. Figure 4.3 shows truck accident frequencies upstream and downstream from merge and diverge ramps in Washington. Upstream distances are measured in 0.05 mile increments from the tip of the merge gore or the beginning of the diverge taper. Downstream distances are also measured in 0.05 mile increments from the end of the merge taper or from the tip of the diverge gore. In the center of each figure is the frequency of accidents in the ramp connection area, which is the accel/decel lane plus adjacent freeway lanes. Note that the average length of the ramp connection area for merge ramps was 0.219 miles, but only 0.107 miles for diverge ramps.

We performed a simple test of frequency differences in successive sections of 0.05 miles either upstream or downstream from the ramp connection area for all truck accidents in our database, which were only accidents that occurred on the ramp itself, in the accel/decel lane, or in lane 1 nearest the ramp. We found that truck accident frequencies stopped changing significantly (i.e., leveled off to a similar number per 0.05 mile section) beyond 0.25 miles upstream for both merge and diverge ramps, beyond 0.2 miles downstream for diverge ramps, and beyond 0.15 miles downstream for merge ramps. The shorter downstream distance for merge ramps seems counterintuitive, but when added to the 0.219 mile average length of a merge area, the total length of 0.369 miles exceeds the combined downstream distance of 0.307 miles for diverge ramps ( 0.107 mile average length of a diverge area plus 0.2 miles).


Figure 4.3: Washington Truck Accidents by Distance from Ramp Area

Figure 4.4 separates the accidents in Figure 4.3 by ramp type for lane 1 (lane adjacent to accel/decel lane) and shoulder accidents only. In comparison to other ramp types, truck accidents occur most frequently both upstream and downstream of diamond ramps relative to the frequency of accidents in the ramp connection area for both merge and diverge ramps. However, since differences in the frequencies of accidents by ramp type were found to be significant (see Chapter 5), we defined the influence zone to be the same for all ramp types as follows in order that later comparisons be consistent:
0.25 miles upstream of the tip of a merge ramp gore
0.25 miles upstream of the start of a diverge ramp taper
0.15 miles downstream of the end of a merge ramp taper
0.20 miles downstream of the tip of a diverge ramp gore

Figure 4.5 shows these influence zone distances for both merge and diverge ramps. The length of each ramp's merge/diverge connection area from the tip of its gore to the start or end of its taper was recorded and kept in our database for each ramp as indicated by its geometric drawing.

### 4.5 ESTIMATING TRUCK EXPOSURE MEASURES

In the next chapter, we compare accident frequencies and rates by ramp type, conflict area, and accident type in three ways so as to reveal the location, volume, and travel distance effects. We first compare average accidents per ramp location without accounting for truck volumes or travel distances. We then compare accidents per ramp truck trip (RTT) to account for the number of trucks passing.

A required data element that we estimated for locations where it was not recorded was ramp truck ADT, which we convert to ramp truck trips for the study period. Ramp truck ADT is not generally available, but WSDOT provided us with a sufficient number of ramp truck ADT's with which to estimate missing values based on the ramp ADT's of all vehicles. Figures 4.6 and 4.7 show estimated versus observed ramp truck ADT's for on and off ramps respectively, where the estimation equations are:


Figure 4.4
Washington Truck Accidents by Distance from Ramp Area by Ramp Type


Figure 4.5: Influence Zone Distances


Figure 4.6
Washington On-Ramp Truck Volumes versus Total On-Ramp Volumes


Figure 4.7
Washington Off-Ramp Truck Volumes versus Total Off-Ramp Volumes


#### Abstract

RTADT $=$ RADT $^{0.69}$ for on ramps

R-squared $=0.826$, parameter's t-statistic $=131.2$ RTADT $=$ RADT $^{0.71}$ for off ramps

R-squared $=0.683$, parameter's $t$-statistic $=106.2$ where, RTADT = ramp truck average daily traffic

RADT = ramp (all vehicle) average daily traffic

The above equations indicate that ramp truck ADT is a decreasing fraction of total ramp ADT as total ramp ADT increases. We fit several other equations to estimate ramp truck ADT including (i) a constant, (ii) main road ADT of all vehicles, (iii) truck ADT on the main road, and (iv) secondary road ADT of all vehicles. We also tried linear models rather than exponential models. However, the t-statistics of the other vanables were not significant at the $95 \%$ confidence level for any of the other models, and the Rsquared values were not much improved. Note that two independent datasets (onramps versus off-ramps) produced nearly the identical equation ( 0.69 versus 0.71 ) as the fitted parameter. Hence, RADT raised to the 0.7 power seems to be a fairly robust predictor for all ramps.


We believe an important predictor of ramp truck ADT would be truck ADT on the secondary road, but this data was not available for any interchange location. Certain facilities near an interchange, such as industrial plants, trucking terminals, truck stops, warehouses, and distribution centers will tend to increase ramp truck ADT as a proportion of total ADT. Absence of any such facilities, such as an interchange serving mainly residential areas, will tend to decrease ramp truck ADT as a proportion of total ADT. Examination of these specific interchange activities would require substantial surveying.

Despite their simplicity and lack of accuracy for some specific ramp locations, these equations do provide usable estimates of ramp truck ADT given the lack of better
data. Ideally, state DOT's will sample ADT's and truck ADT's for a greater proportion of their ramps in the future. Only then will more accurate ramp truck ADT's be available to studies like ours without the need for estimation.

In order to not underestimate truck exposure for any ramp type, we needed to have truck ADT's for a sufficient number and variety of ramps where accidents did not occur. The ramp truck ADT's that we obtained or estimated automatically included a sufficient coverage of ramp locations and conflict areas where accidents did not occur. Hence, we were able to control for this potential bias.

### 4.6 PREPARATION OF COLORADO AND CALIFORNIA DATASETS

We compiled data on truck accidents at interchanges in both Colorado and Califomia for the years 1991-1993. Since the required data was not available in electronic form from either state (including police report data, route mile points, highway geometrics, and drawings), we could not include all truck accidents at all interchanges within the analysis period as we had for Washington. Hence, we were only able to compile accident data on several hundred accidents in each state (more in Califomia than in Colorado).

In both Colorado and Califomia, we used three sequential criteria to identify relatively hazardous interchanges for trucks among all interchanges in each state. We first selected all interchanges with an accident seventy index of 30 or greater. The severity index weighs the number of accidents over three years involving at least one truck according to the foliowing formula:

Severity index $(\mathrm{SI})=\left(12^{*}\right.$ number of fatal accidents $)+\left(5^{*}\right.$ number of injury , accidents) + (1 * number of property damage only accidents)

The above formula does not distinguish accidents by the number of vehicles involved, the number of injured persons or fatalities, or the extent of damage. Although such considerations could be made, the objective was to select a cross-section of interchanges, so a more specific index was not needed.

In addition to interchanges that surpassed the severity index, we also included interchanges with more than 15 accidents of any type involving trucks over three years. The first criterion considered both frequency and severity, whereas this criterion considers only frequency.

Finally, we used freeway truck ADT as an approximate measure of truck exposure through the entire interchange in order to identify interchanges that had high truck accident frequencies relative to exposure. If the interchange connected two freeways, we used the average truck ADT of the two freeways. Thus, our third criterion was whether the number of truck accidents over three years divided by freeway truck ADT exceeded 0.003 . This value of the criterion was used because it identified a reasonable variety of additional interchanges beyond the first two criteria.

In summary, our interchange selection criteria for Colorado and Califomia were:

1. Severity index of all truck accidents over three years $\geq 30$
2. Number of truck accidents of all types over three years $\geq 15$
3. Number of truck accidents of all types over three years divided by
freeway truck $A D T \geq 0.003$

Tables 4.5 and 4.6 list the interchanges we identified in Colorado and Califomia for further analysis. Also shown is the interchange type, freeway ADT, truck percentage, and numbers of accidents by severity (fatal, injury, property damage only) for each location.

The data that we were able to assemble for Colorado and Califomia directly from police reports and design drawings included:

1. Accident location (route mile post) and direction of travel.
2. Main and secondary route identifiers (perhaps both freeways).
3. Accident type (e.g., sideswipe, rearend, rollover, etc.).
4. Lane in which accident occurred.
5. Interchange type (e.g., diamond, directional, etc.).
6. Ramp type (e.g., diamond, loop, directional, etc.).
7. Ramp connection type (freeway-to-freeway, freeway-to-arterial, etc.).
8. Conflict area (e.g., merge, diverge, upstream, downstream, etc.).

Our datasets for Colorado and Califormia are not comparable to our database for Washington in a number of ways. First, we could not obtain ramp truck ADT's or total ramp ADT's with which to estimate ramp truck ADT's. Second, we could not obtain reliable geometric measurements for each interchange during the study period. Hence, our between-state comparisons in Chapter 5 are limited to accident frequencies per ramp type, not accidents per ramp truck trip or VMT.

| County | Description | Interch. Type | AVG AADT | AVG <br> TRUCK \% |  |  | $\begin{aligned} & P \\ & D \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline 1 \\ & \mathrm{~N} \\ & \mathrm{~J} \end{aligned}$ |  | KSk |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
| 4 | 1-25 \& Bllou St. | Diamond | 69900 | 3.7 |  | 201033 | 5 | 2 |  |  |
| 4 | 1-25 \& Fillmore St. | Dlamond | 74400 | 3.3 |  |  | 4 | 4 | 0 |  |
| 1 | 1-25 \& Sanfa Fe | Directional | 150400 | 2.5 | 3 $3_{\text {cha }}$ | - S 0038 | 8 | 2 |  |  |
| 1 | 1-25 \& Speer Bivd. | Full Cloverieaf | 167180 | 2.8 |  | 2060653 | 9 | 2 |  |  |
| 1 | 1-25\& Fox/38th Ave. | Pantial Cloverleaf | 180500 | 2.9 |  | 3003043 | 19 | 4 | 0 | 153 |
| 1 | \|-25\&1-70 | Directional $T$ | 139855 | 3.7 |  |  | 60 | 16 |  |  |
| 12 | 1-25\&SH36 | Directional | 147800 | 3.8 |  | - 3 geza | 5 | 6 | 0 | W Whesk |
| 8 | 1-25\&SH 34 | Full Cloverfeaf | 33100 | 9.7 |  | - \% Cusiza | 6 | 5 |  |  |
| 11 | 1-70 \& Ward St. | Partial Cloveriagf | 82000 | 3.8 |  | S SCB44 | 12 | 1 |  |  |
| 1 | 1-70\& Pecos St. | Diamond | 110300 | 3.8 |  | 8, ${ }^{\text {cegag }}$ | 16 | 3 | 0 | 0 \% |
| 1 | 1-70 \& Steele St. | Dlamond | 94900 | 4.6 |  | 36063\% | 9 | 5 | 0 |  |
| $\bigcirc 1$ | 1-70 \& Quebse St. | Diamond | 93300 | 4.6 | 3363学變 | K80035 | 13 | 2 |  |  |
| 1 | 11-7081-225 | Directional | 74000 | 7.2 | Kayd 6 Sisk | - 6 Cobas | 12 | 4 |  |  |
| 12 | 1.70\& Chambers Rd | Diamond | 30000 | 11.1 |  | \% | 7 | 4 |  |  |



Table 4.6: Selected California Interchanges for Accident Analysis

## Chapter Five

## STATISTICAL ANALYSES OF ACCIDENT DATA

### 5.1 ACCIDENTS PER RAMP IN WASHINGTON

Chapter 4 explained the key attributes by which we classified all truck accidents at interchanges in Washington during the 27 months from January 1, 1993 to March 31, 1995. Table 5.1 shows numbers of ramps and accidents per ramp type for merge and diverge ramps. The term "ramp" in Table 5.1 refers to the entire ramp area including both ramp and adjacent freeway lanes. Parts (a-c) of Table 5.1 show separate tabulations by whether accidents occurred (a) on the ramps, (b) on the main lanes upstream, downstream, or adjacent to the ramps, or (c) on the main lanes or the ramps (all accidents). Each ramp is counted only once regardless of how many accidents occurred there. Since many ramps had multiple accidents, numbers of accidents by ramp type differ from the numbers of ramps where these accidents occurred. For all ramp types combined, $63 \%$ had only one accident, $22 \%$ had 2 accidents, and the other $15 \%$ had 3 or more accidents.

In Table 5.1, accidents shown in parts (a) and (b) add up to part (c) because every accident was coded by WSDOT to have occurred either on a ramp or on the main line. However, the numbers of ramps in parts (a) and (b) do not add up to part (c) because many ramp locations had accidents both on the ramp and main line. As noted in Chapter 4, we did not record any data for ramp locations where no accidents occurred. However, these ramps do have many conflict areas (i.e., the ramps themselves, ramp connection areas, upstream areas, and downstream areas) where no accidents occurred. Ramps in part (c) minus ramps in part (a) equal ramps where no accidents occurred specifically on the ramps. Ramps in part (c) minus ramps in part (b) equal ramps where no accidents occurred on the main lanes nearby the ramps. All accidents at intersections of ramps with arterial roads are excluded throughout this analysis.

| RAMP TYPE |  | OF OFF Ramps |  |  | $\begin{array}{r} \text { \#ot } \\ \text { On-Ramp } \\ \text { Acc } \end{array}$ | 禁 <br> OffRamp <br> Acc | $\begin{array}{r} \%=1 \\ \text { On-famp } \\ \text { Acc } \end{array}$ | \%ot Off-Ramp $A \subset C$ | Hof Acc per On-Ramp | $\begin{array}{r} \text { Of } \\ \text { Acc per } \\ \text { Ot-Ramp } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Miamond | 45 | 21 | 37.2 | 23.1 | 56 | 23 | 33.1 | 19.0 | 1.24 | 1.10 |
| Loop | 27 | 20 | 22.3 | 22,0 | 38 | 30 | 22.5 | 24.8 | 1.41 | \$.50 |
| OuterConn | 9 | 10 | 7.4 | 11.0 | 17 | 12 | 10.1 | 9.9 | 1.89 | 1.20 |
| Directional | 36 | 34 | 29.8 | 37.4 | 53 | 48 | 31.4 | 39.7 | 1.47 | 1.41 |
| Other | 4 | 6 | 3,3 | 6.6 | 5 | B | 3.0 | 6.6 | 1.25 | 1.33 |
| $\begin{array}{r} \text { Total } \\ \% \end{array}$ | $\begin{array}{r} 121 \\ 57.1 \end{array}$ | $\begin{array}{r} 91 \\ 42.8 \end{array}$ | 100.0 | 100.0 | $\begin{gathered} 169 \\ 58.3 \end{gathered}$ | $\begin{array}{r} 121 \\ 41.7 \end{array}$ | 100.0 | 100.0 | 1.40 | 1.33 |

Table 6.1.2 Ramp Accidents

| RAMP TYPE | $\begin{array}{r} \text { OI } \\ \text { ON } \\ \text { Ramps } \end{array}$ | OOI OFF Ramps | $\%$ of ON Ramps | $\begin{array}{r} \% 61 \\ \text { OFF } \\ \text { Ramps } \end{array}$ | $\begin{array}{r} \text { Of } \\ \text { Ormamp } \\ \text { Aco } \end{array}$ |  | $\begin{array}{r} \text { OrDf } \\ \text { On-Ramp } \\ \text { Ace } \end{array}$ | $\begin{array}{r} \text { Of of } \\ \text { Act } \end{array}$ | $\begin{array}{r} \text { Acci per } \\ \text { On-Ramp } \end{array}$ | $\begin{array}{r} \text { \# of } \\ \text { Acc per } \\ \text { Of-Ramp } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Oiamond | 140 | 127 | 57.1 | 59.3 | 216 | 195 | 54.3 | 57.0 | 1.54 | 1.54 |
| Loop | 32 | 10 | 13.1 | 4.7 | 51 | 15 | 12.8 | 4.4 | 1.59 | 1.50 |
| OuterCorm | 21 | 22 | 8.6 | 10.3 | 35 | 36 | 8.8 | 10.5 | 1.67 | 1.64 |
| Directional | 41 | 49 | 16.7 | 22.9 | 79 | 89 | 19.8 | 28.0 | 1.93 | 1.82 |
| Other | 11 | 6 | 4.5 | 2.8 | 17 | 7 | 4.3 | 2.0 | 1.55 | 1.17 |
| Totas \% | $\begin{array}{r} 245 \\ 53.4 \end{array}$ | $\begin{array}{r} 214 \\ 46.6 \end{array}$ | 100.0 | 100.0 | $\begin{gathered} 398 \\ 53.8 \end{gathered}$ | $\begin{array}{r} 342 \\ 46.2 \end{array}$ | 100.0 | 100.0 | 1.68 | 1.60 |

Table 5.1.6 Ming Lina Accidents (Lane i)

| RAMP TYPE | $\begin{array}{r} \text { \#ot } \\ \text { ON } \\ \text { Ramps } \end{array}$ |  |  | 807 OFF Ramps |  | $\begin{array}{r} \text { Of } \\ \text { Offrap } \\ \text { Ao } \end{array}$ | $\begin{array}{r} \text { \%or } \\ \text { On-Ramp } \\ \text { Acc } \end{array}$ | $\begin{array}{r} 960 \\ \text { Ofor } \\ \text { ACC } \end{array}$ | $\begin{array}{r} \text { \# of } \\ \text { Accper } \\ \text { On-Plamp } \end{array}$ | Accper Of-Ramp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dramond | 168 | 142 | 49.6 | 46.6 | 272 | 218 | 48.0 | 47.1 | 1.62 | 1.54 |
| Loop | 53 | 28 | 15.6 | 9.2 | 89 | 45 | 15.7 | 27 | 1.68 | 1.61 |
| OuterConn | 28 | 31 | 8.3 | 10.2 | 52 | 48 | 9.2 | 10.4 | 1.85 | 1.55 |
| Directional | 69 | 83 | 20.4 | 27.2 | 132 | 137 | 23.3 | 29.6 | 1.91 | 1.65 |
| Other | 21 | 21 | 6.2 | 6.9 | 22 | 15 | 3.9 | 3.2 | 1.05 | 0.71 |
| Total \% | $\begin{gathered} 339 \\ \mathbf{\$ 2 . 6} \end{gathered}$ | $\begin{array}{r} 305 \\ 47.4 \end{array}$ | 100.0 | 100.0 | $\begin{aligned} & 567 \\ & 55.0 \end{aligned}$ | $\begin{array}{r} 463 \\ 45.0 \end{array}$ | 100.0 | 100.0 | 1.67 | 1.52 |

Table 5.1.c All Accidents

Table 5.1: Washington State Truck Accidents by Ramp type


Figure 5.1: Four Ramp Conflict Areas

As noted in Chapter 4, we only compiled data for truck accidents on the freeway that occurred in the shoulder or in the adjacent lane 1 on the ramp connection side of the freeway as coded by WSDOT, since these are the majority of freeway truck accidents related to ramp conflicts. In Table 5.1, part (a) shows the freeway truck accidents, part (b) shows accidents that occurred in the accel/decel lane or on the ramp itself. In order study the effects of ramp geometrics on truck accidents, we decided it was better to separate accidents into the four conflict areas depicted in Figure 5.1. These four areas are (i) the ramp area away from the main lanes, (ii) the ramp connection including the accel/decel lane and the adjacert lane 1, (iii) lane 1 upstream of the ramp connection, and (iv) lane 1 downstream of the ramp connection. Of the 339 on-ramps and 305 off-ramps listed in Table 5.1c, only a few merged or diverged on the left side of the freeway. Roughly $60 \%$ of the ramps had one accident, $20 \%$ had two accidents, and $20 \%$ had three or more accidents in the study period.

Average accidents per ramp in Table 5.1 do not account for the volumes and distances of truck travel, but we later examine accident rates per ramp truck trip and per ramp truck VMT. These initial comparisons of average accidents per ramp help to separate out these volume and distance effects. As also discussed in Chapter 4, there is no "one best" truck exposure measure to use (e.g., ramp truck ADT, mainline truck ADT, total vehicle ADT, etc.). This section shows accident frequencies before introducing an exposure measure. In addition, since truck ADT's (both reported and estimated) are not precise, and accident frequencies may be so random or dependent on other factors that no significant relationship to truck ADT is found, an initial inspection of the data without truck ADT's is warranted.

Table 5.2 shows numbers of ramps, accidents, and average accidents per ramp in the four conflict areas just explained. Since numbers of ramps by conflict area include all places where accidents may have occurred even if none did, they generally equal the numbers of merge or diverge ramps. There are slightly more specific "on ramps" and "off ramps" due to ramps connecting collector/distributor lanes for which we did not count upstream and downstream areas. Hence, the average frequencies shown are per all conflict area regardless of whether any accidents occurred there.

Table 5.2 shows significant differences in frequencies of accidents per conflict area, which we later examine by ramp and accident type. Accidents occur at significantly lower average frequency on ramp sections away from freeway lanes (Table 5.2a) than in the upstream, downstream, or ramp connection areas of the freeway (Table 5.2b). Accidents that do occur on ramps away from freeway lanes occur more frequently on off-ramps than on on-ramps. We'll see later that loop off-ramps are a main source of this difference.

Accidents specifically on ramps can occur at junctions of multiple ramps (excluding intersections with arterial roads). Ramp junctions occur most often in directional ramps, and clearly contribute to the frequency of ramp accidents. Among 328 on-ramps containing 94 ramp junctions, 45 truck accidents occurred at junctions ( 0.644 accidents per junction). Only 40 other truck accidents occurred on the 328 on-ramps ( 0.122 accidents per ramp). Among 292 off-ramps containing 86 ramp junctions, 25 truck accidents occurred at junctions ( 0.402 accidents per junction). The 70 other truck accidents on off-ramps occurred away from the junctions ( 0.240 accidents per ramp). Beyond these comparisons, we did not separately investigate the effects of ramp junctions in this study, and grouped all accidents that occurred on ramps together, but still separate by merge or diverge ramp.

Table 5.3 shows a two-way frequency table of accidents by ramp and conflict area for both merge and diverge ramps. The third line of each cell shows the accident frequency per conflict area, where we see that accidents occur most frequently in ramp connection areas (merge and diverge areas). However, the average frequencies for all on-ramps, all off-ramps, and all ramps combined are not greatly different. Excluding ramp type "other", a two-way analysis of vanance showed these average accident frequencies to be significantly different by conflict area at the $95 \%$ confidence level, but not by ramp type. This finding suggests the importance of examining accident histories by conflict area rather than differences by ramp type.

| Conflict Area | Accidents | Percent | Conflict <br> Areas | Accidents <br> per <br> Conflict Area |
| :--- | ---: | ---: | ---: | :---: |
| Upstream of Merge | 151 | 26.6 | 331 | 0.46 |
| Merge Ramp | 267 | 47.1 | 331 | 0.81 |
| Downstream of Merge | 74 | 13.1 | 331 | 0.22 |
| On Ramp | 75 | 13.2 | 339 | 0.22 |
|  | 567 | 100.0 | 1332 | 0.43 |

(a) On-Ramp Accidents

| Confict Area | Accidents | Percent | Conflict <br> Areas | Accidents <br> per <br> Conflict Area |
| :--- | ---: | ---: | ---: | :---: |
| Upstream of Diverge | 119 | 25.7 | 294 | 0.40 |
| Diverge Ramp | 131 | 28.3 | 294 | 0.45 |
| Downstream of Diverge | 122 | 26.3 | 294 | 0.41 |
| Off Ramp | 91 | 19.7 | 305 | 0.30 |
|  | 463 | 100.0 | 1187 | 0.39 |

(b) Off - Ramp Accidents

Table 5.2: Washington State Truck Accidents by Conflict Area


Table 5.4 shows a three-way frequency table of accidents by ramp type, accident type, and conflict area. Two observations here are that (i) rollover accidents are prevalent on loop off-ramps, but otherwise (ii) sideswipe accidents are most prevalent for all ramp types, especially in ramp connection areas. Table 5.5 shows a two-way frequency table of accidents by conflict area and accident type by aggregating all ramp types together. Here, numbers of conflict areas where accidents may have occurred always equal the numbers of merge and diverge ramps, allowing for a few ramps without freeway connections.

Values shown in the righthand portion of Table 5.5 show the accident frequencies per conflict area. A two-way analysis of vanance showed these average accident frequencies to be significantly different by accident type at the $95 \%$ confidence level, but not by conflict area, due to these values varying highly within conflict areas. One reason why accident frequencies do not vary significantly by conflict area when grouped by accident type is that some accident types are so easily affected by driver actions (e.g., a sideswipe may result from the driver attempting to avoid a rearend collision on a short ramp). However, two important observations are that sideswipes are most frequent in merge areas, and rollovers are most frequent on ramps themselves, which occur mostly on loop ramps (see Table 5.4).

We next investigate whether stratifying ramps by high, medium, or low ADT of trucks or all vehicles on the ramp shows greater lane-changing difficuities at higher volumes or the risks of greater speeds at lower volumes. In Table 5.6, we grouped conflict areas together by whether ramp truck ADT was low, medium, or high. In Table 5.7, we grouped conflict areas by whether ramp ADT of all vehicles was low, medium, or high. These stratified results, especially in low to middle ADT levels, show accident frequencies on the ramps and in ramp connection areas to increase more consistently with higher ADT's compared to accident frequency in the upstream or downstream areas. This illustrates the effects of traffic volumes on truck accident frequencies on the ramps and in ramp connection areas where most weaving occurs.

### 5.2 ACCIDENTS PER RAMP TRUCK TRIP IN WASHINGTON

This section compares the same truck accident locations examined in the previous section taking ramp truck ADT (RTADT) into account. Table 5.8 shows numbers of ramps, accidents, cumulative ramp truck ADT's, ramp truck trips in millions (RTT), and accidents per RTT for the four conflict areas discussed earlier. To calculate RTT, each ramp truck ADT was divided by one million and multiplied by 820 days in the study period (January 1, 1993 to March 31, 1995).

Ramp truck ADT for each ramp is added just once to its sum for each conflict area regardless of whether none or many accidents occurred there. As explained in Chapter 4, we included ramp truck ADTs for conflict areas without accidents so as to most fully represent truck exposure. Note that $R T T$ is identical for each merge ramp conflict area and for each diverge ramp conflict area, except for RTT of ramps themselves, which are slightly higher because of a few ramp-to-ramp connectors. Thus, accidents per RTT and accidents per conflict area in Table 5.2 compare similarly between conflict areas. Accidents per RTT are less meaningful for upstream areas of on-ramps and downstream areas of off-ramps, since trucks using the ramps do not travel those areas. Although we knew freeway truck percentages, we did not know truck percentages in each freeway lane, and thus could not calculate truck trips through each conflict area involving only lane 1 plus or minus ramp truck trips. By coincidence, there was an average of 1.0 truck accidents per million ramp truck trips through these conflict areas of both merge and diverge ramps. Since each ramp truck trip is counted four times in the total accident rate (once for each conflict area), this total accident rate equals an average of 4.0 accidents per ramp truck trip if the ramp is not subdivided into four parts.

Again, there is no "one best" truck exposure measure to use (e.g., ramp truck trips, mainline truck trips, total vehicles, etc.). We make all companisons per ramp truck trip because this rate indicates the likelihood of a merging or diverging truck to be in an accident within each conflict area. Obviously, accidents upstream of merge ramps


Koy: Sewp = Sidetulpe Rand a Rear-and
Rove a Rollovar
Mer upts = Uisistreem of the Marco Area
Mer -upset pornstream of the Merge Arsa
OV Mps : Uperiream of the Dtwerpe Area
DV - ctunt = Downstream of the Dtverge Area

|  |  | \# ofConflict Area | ACCIDENT TYPE |  |  |  | $\begin{array}{r} \text { Total } \\ \text { \# of } \\ \text { Acc } \\ \hline \end{array}$ | Accidents per Conflict Area |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA |  | SIdeswipe | Rear-end | Rollover] | Other |  | Sideswipe | Rear-end] | Rollover | Other |
| $\left.\begin{array}{ll} \hline & R \\ & a \\ 0 & m \\ n & p \\ & s \end{array} \right\rvert\,$ | Mer_upsMergeOn-RampMer__dwnstTotal | 331 | 79 | 43 | 4. | 25 | 151 | 0.24 | 0.13 | 0.012 | 0.08 |
|  |  | 331 | 170 | 75 | 3 | 19 | 267 | 0.51 | 0.23 | 0.009 | 0.06 |
|  |  | 339 | 36 | 7 | 18 | 14 | 76 | 0.11 | 0.02 | 0.053 | 0.04 |
|  |  | 331 | 38 | 16 | 1 | 19 | 74 | 0.11 | 0.05 | 0.003 | 0.06 |
|  |  | 1332 | 323 | 141 | 26 | 77 | 567 | 0.24 | 0.11 | 0.020 | 0.06 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  $R$ <br> $O$ $a$ <br> $f$ $m$ <br> $f$ $p$ <br>  $s$ <br>   | Div_ups Diverge Off_Ramp Div_dwnst <br> Total | 294 | 68 | 40 | 1 | 20 | 119 | 0.20 | 0.14 | 0.003 | 0.07 |
|  |  | 294 | 72 | 39 | 3 | 17 | 131 | 0.24 | 0.13 | 0.010 | 0.06 |
|  |  | 305 | 33 | 16 | 20 | 22 | 91 | 0.14 | 0.05 | 0.066 | 0.07 |
|  |  | 294 | 70 | 31 | 0 | 21 | 122 | 0.24 | 0.11 | 0.000 | 0.07 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 1187 | 233 | 126 | 24. | 80 | 463 | 0.20 | 0.11 | 0.020 | 0.07 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | Totals | 2519 | 556 | 267 | 50 | 167 | 1030 | 0.22 | 0.11 | $0 . \overline{02} \overline{0}$ | 0.06 |

Key: Sswp = Sideswipe
Rend = Rear-end
Rovr = Rollover
Mer_ups = Upstream of the Merge Area
Mer_dwnst = Downstream of the Merge Area
Div_ups $=$ Upstream of the Diverge Area
Div_ownst = Downstream of the Diverge Area


|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| \# 0 ; Lo | ACCIDENT TYPE |  |  |  |
|  | Sswp | Rend | Rovr\| | Other |
| $\overline{148}$ | $\begin{array}{r} 36 \\ 0.28 \end{array}$ | $\begin{array}{r} 25 \\ 0.17 \end{array}$ | 0.00 | $\begin{array}{r} 8 \\ 0.05 \end{array}$ |
| 148 | $\begin{array}{r} 87 \\ 0.58 \end{array}$ | $\begin{array}{r} 40 \\ 0.27 \end{array}$ | 1 0.01 | $\begin{array}{r} 10 \\ 0.07 \end{array}$ |
| 156 | $\begin{array}{r} 25 \\ 0.16 \\ \hline \end{array}$ | $\begin{array}{r} 3 \\ 0.02 \\ \hline \end{array}$ | $\begin{array}{r} 10 \\ 0.08 \\ \hline \end{array}$ | $\begin{array}{r} 3 \\ 0.02 \\ \hline \end{array}$ |
| 148 | $\begin{array}{r} 16 \\ 0.11 \\ \hline \end{array}$ | $\begin{array}{r} 10 \\ 0.07 \\ \hline \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | $\begin{array}{r} 5 \\ 0.03 \end{array}$ |
| 600 | $\begin{aligned} & \hline 167 \\ & 0.28 \end{aligned}$ | $\begin{array}{r} 78 \\ 0.13 \end{array}$ | $\begin{array}{r} 11 \\ 0.02 \end{array}$ | $\begin{array}{r} 26 \\ 0.04 \end{array}$ |
| 172 | $\begin{array}{r} 36 \\ 0.21 \end{array}$ | $\begin{array}{r} 28 \\ 0.18 \end{array}$ | 0 0.00 | $\begin{array}{r} 9 \\ 0.05 \end{array}$ |
| 172 | $\begin{array}{r} 48 \\ 0.28 \\ \hline \end{array}$ | $\begin{array}{r} 28 \\ 0.15 \end{array}$ | 2 0.01 | $\begin{array}{r} 8 \\ 0.05 \end{array}$ |
| 180 | $\begin{array}{r} 21 \\ 0.12 \end{array}$ | $\begin{array}{r} 13 \\ 0.07 \end{array}$ | $\begin{array}{r} 14 \\ 0.08 \\ \hline \end{array}$ | $\begin{array}{r} 12 \\ 0.07 \end{array}$ |
| 172 | $\begin{array}{r} 50 \\ 0.29 \\ \hline \end{array}$ | $\begin{array}{r} 21 \\ 0.12 \end{array}$ | 0 0.00 | $\begin{array}{r} 8 \\ 0.05 \\ \hline \end{array}$ |
| 698 | $\begin{aligned} & \hline 156 \\ & 0.22 \end{aligned}$ | $\begin{array}{r} 87 \\ 0.13 \end{array}$ | $\begin{array}{r} 16 \\ 0.02 \end{array}$ | $\begin{array}{r} 37 \\ 0.05 \end{array}$ |
| 1298 | $\begin{array}{r} 323 \\ 0.25 \end{array}$ | $\begin{array}{r} 185 \\ 0.13 \end{array}$ | $\begin{array}{r} 27 \\ 0.02 \\ \hline \end{array}$ | $\begin{array}{r} 63 \\ 0.05 \\ \hline \end{array}$ |
|  |  |  |  | 578 |


| Ramp Truck ADT > $=800$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| \# of | ACCIDENT TYPE |  |  |  |
| Loc | Sswp\| | Rend] | Rovr | Other |
| 69 | $\begin{array}{r} 18 \\ 0.26 \end{array}$ | $\begin{array}{r} 11 \\ 0.16 \end{array}$ | $\begin{array}{r} 2 \\ 0.03 \end{array}$ | $\begin{array}{r} 5 \\ 0.07 \end{array}$ |
| 69 | $\begin{array}{r} 44 \\ 0.84 \\ \hline \end{array}$ | $\begin{array}{r} 22 \\ 0.32 \end{array}$ | 0 0.00 | 4 0.06 |
| 69 | $\begin{array}{r} 9 \\ 0.13 \\ \hline \end{array}$ | $\begin{array}{r} 3 \\ 0.04 \end{array}$ | 5 0.07 | 8 0.12 |
| 69 | $\begin{array}{r} 7 \\ 0.10 \end{array}$ | $\begin{array}{r} 1 \\ 0.01 \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | 5 0.07 |
| 276 | $\begin{array}{r} \hline 78 \\ 0.28 \end{array}$ | $\begin{array}{r} 37 \\ 0.13 \end{array}$ | $\begin{array}{r} 7 \\ 0.03 \end{array}$ | $\begin{array}{r} 22 \\ 0.08 \\ \hline \end{array}$ |
| 42 | $\begin{array}{r} 5 \\ 0.12 \end{array}$ | 1 0.02 | 0 0.00 | 2 0.05 |
| 42 | $\begin{array}{r} 11 \\ 0.26 \end{array}$ | $\begin{array}{r} 7 \\ 0.17 \end{array}$ | 0 | 1 0.02 |
| 42 | $\begin{array}{r} 9 \\ 0.29 \\ \hline \end{array}$ | $\begin{array}{r} 1 \\ 0.02 \end{array}$ | 9 0.02 | $\begin{array}{r}3 \\ 0.07 \\ \hline\end{array}$ |
| 42 | $\begin{array}{r} 5 \\ 0.12 \end{array}$ | $\begin{array}{r} 3 \\ 0.07 \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | 1 0.02 |
| 168 | $\begin{array}{r} 30 \\ 0.18 \end{array}$ | $\begin{array}{r} 12 \\ 0.07 \end{array}$ | $\begin{array}{r} 1 \\ 0.01 \end{array}$ | $\begin{array}{r} 7 \\ 0.04 \end{array}$ |
| 444 | $\begin{aligned} & 108 \\ & 0.24 \end{aligned}$ | $\begin{array}{r} 49 \\ 0.11 \end{array}$ | 8 0.02 | 29 0.07 |
|  |  |  |  | 194 |

Key: Sswp $=$ Sldeswipe
Rend $=$ Rear-end
Rove $=$ Rollover
Loc $=$ Location (Conflct Area)
Accident Type Stratified by Total Ramp ADT
Table 5.7: Washington State Truck Accidents by Conflict Area and

|  |  |  | Total Ramp ADT<4000 |  |  |  |  | 4000>2Total Ramp ADT<10000 |  |  |  |  | Total Ramp ADT > $=10000$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { CONFLICT } \\ \text { AREA } \end{array}$ |  |  | $\begin{aligned} & \text { \# } 07 \\ & 1 \infty \\ & -\infty \end{aligned}$ | ACCIDENT TYPE |  |  |  | $\begin{aligned} & \# 07 \\ & \mathrm{Loc} \end{aligned}$ | ACCIDENT TYPE |  |  |  | $\begin{aligned} & \text { \#0t } \\ & 2 \infty \end{aligned}$ | ACCIDENT TYPE |  |  |  |
|  |  |  |  | Sswp | Rend | Rovr | Other |  | Sswp] | Rond | Rovil | Other |  | Sswo | Rend | Rovr | Other |
| R | Mergo upstriam | $\begin{gathered} \text { \# of } A c C \\ A \subset c / L \infty \end{gathered}$ | 114 | 26 0.23 | $\begin{array}{r} 1 \\ 0.08 \\ \hline \end{array}$ | $\begin{array}{r} 2 \\ 0.02 \end{array}$ | $\begin{array}{r} 12 \\ 0.11 \\ \hline \end{array}$ | 119 | $\begin{array}{r} 30 \\ 0.25 \\ \hline \end{array}$ | $\begin{array}{r} 21 \\ 0.18 \\ \hline \end{array}$ | 0.08 | $\begin{array}{r}7 \\ 0.06 \\ \hline\end{array}$ | 98 | $\begin{array}{r} 23 \\ 0.23 \\ \hline \end{array}$ | $\begin{array}{r} 15 \\ 0.15 \end{array}$ | 1 <br> 0.01 | 6 0.08 |
| $\left\|\begin{array}{ll} 0 \\ 0 & \\ n \end{array}\right\|$ | Merge Area | \# Of Acc <br> Acc/ LOC | 314 | 40 0.35 | 10 0.09 | 2 0.02 | $\begin{array}{r}3 \\ 0.03 \\ \hline\end{array}$ | 119 | 68 0.57 | $\begin{array}{r}35 \\ 0.28 \\ \hline\end{array}$ | [ 0 | $\begin{array}{r}10 \\ 0.08 \\ \hline\end{array}$ | 98 | 62 0.83 | 30 0.31 | 1 0.01 | 6 0.06 |
|  | On-Ramp | $\begin{gathered} \text { \# of } A C E \\ \text { Acc/ } L \infty \end{gathered}$ | 114 | 7 0.08 | 0.01 | $\begin{array}{r} 5 \\ 0.04 \end{array}$ | $\begin{array}{r}4 \\ 0.04 \\ \hline\end{array}$ | 126 | 15 0.12 | 1 0.01 | 4 0.03 | $\begin{array}{r}4 \\ 0.03 \\ \hline\end{array}$ | 99 | 14 0.14 | 5 0.05 | 9 0.09 | $\begin{array}{r}6 \\ 0.08 \\ \hline\end{array}$ |
|  | Merge downstream | $\begin{aligned} & \text { \# of Acc } \\ & \text { Aco / LOC } \end{aligned}$ | 114 | $\begin{array}{r} 13 \\ 0.11 \end{array}$ | $\begin{array}{r} 5 \\ 0.04 \end{array}$ | $\begin{array}{r} 7 \\ 0.01 \end{array}$ | $\begin{array}{r} 10 \\ 0.00 \end{array}$ | 119 | $\begin{array}{r} 16 \\ 0.13 \end{array}$ | $\begin{array}{r} 8 \\ 0.07 \end{array}$ | 0.00 | $\begin{array}{r}4 \\ 0.03 \\ \hline\end{array}$ | 98 | 8 0.09 | 3 0.03 | 0 0.00 | $\begin{array}{r}5 \\ 0.05 \\ \hline\end{array}$ |
| p | On-Ramp | $\begin{array}{r} \text { Totals } \\ \text { Acc / Loc } \end{array}$ | 456 | 86 23 10 29 <br> 0.189 0.05 0.022 0.084 |  |  |  | 483 | $\begin{array}{r} 129 \\ 0.267 \end{array}$ | $\begin{array}{r} 65 \\ 0.135 \end{array}$ | $\begin{array}{r} 6 \\ 0.01 \end{array}$ | $\begin{array}{r} 25 \\ 0.052 \end{array}$ | 393 | $\begin{array}{r} 108 \\ 0.275 \end{array}$ | 53 11 <br> 0.135 0.028 |  | $\begin{array}{r} 23 \\ 0.059 \end{array}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  $R$ <br> 0 $a$ <br> 1 $m$ <br> 1 $p$ <br>  $s$ | Divarge upstream Dlverge Area <br> OfR-Ramp <br> Dlvarge downstream |  | 94 | $\begin{array}{r} 16 \\ 0.20 \end{array}$ | $\begin{array}{r} 13 \\ 0.14 \end{array}$ | $\begin{array}{r} 1 \\ 0.01 \end{array}$ | $\begin{array}{r} 8 \\ 0.10 \end{array}$ | 110 | $\begin{array}{r} 24 \\ 0.22 \end{array}$ | $\begin{array}{r} 17 \\ 0.15 \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | $\begin{array}{r} 6 \\ 0.07 \end{array}$ | 80 | $\begin{array}{r} 15 \\ 0.17 \end{array}$ | $\begin{array}{r} 10 \\ 0.11 \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | $\begin{array}{r} 3 \\ 0.03 \end{array}$ |
|  |  |  | 94 | 13 0.14 | 7 0.07 | $\begin{array}{r}1 \\ 0.01\end{array}$ | 10 0.11 | 110 | $\begin{array}{r} 32 \\ 0.29 \end{array}$ | $\begin{array}{r} 18 \\ 0.15 \end{array}$ | $\begin{array}{r} 1 \\ 0.01 \end{array}$ | $\begin{array}{r} 5 \\ 0.05 \end{array}$ | 90 | $\begin{array}{r} 27 \\ 0.30 \end{array}$ | $\begin{array}{r} 16 \\ 0.18 \\ \hline \end{array}$ | $\begin{array}{r} 1 \\ 0.01 \end{array}$ | $\begin{array}{r} 2 \\ 0.02 \end{array}$ |
|  |  |  | 67 | 3 0.03 | 0.3 0.03 | 6 0.08 | 8 0.08 | 116 | $\begin{array}{r} 10 \\ 0.09 \end{array}$ | $\begin{array}{r} 6 \\ 0.04 \end{array}$ | $\begin{array}{r} 10 \\ 0.09 \end{array}$ | $\begin{array}{r} 8 \\ 0.07 \end{array}$ | 82 | $\begin{array}{r} 20 \\ 0.22 \\ \hline \end{array}$ | $\begin{array}{r} 8 \\ 0.09 \end{array}$ | $\begin{array}{r} 4 \\ 0.04 \end{array}$ | $\begin{array}{r} 6 \\ 0.07 \end{array}$ |
|  |  | $\text { \# of } \overline{A C C}$ <br> Acc/Loc | 64 | 18 0.17 | 10 0.11 | 0 0.00 | 14 0.15 | 110 | $\begin{array}{r} 36 \\ 0.33 \\ \hline \end{array}$ | $\begin{array}{r} 15 \\ 0.14 \\ \hline \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | $\begin{array}{r} 4 \\ 0.04 \end{array}$ | 90 | $\begin{array}{r} 18 \\ 0.20 \end{array}$ | $\begin{array}{r} 6 \\ 0.07 \end{array}$ | $\begin{array}{r} 0 \\ 0.00 \end{array}$ | 0.03 |
|  | Of-Ramp | totais <br> $A C c / L O C$ | 379 | $\begin{array}{r} 51 \\ 0.13 \\ \hline \end{array}$ | $\begin{array}{r} 33 \\ 0.09 \\ \hline \end{array}$ | $\begin{array}{r} 8 \\ 0.02 \\ \hline \end{array}$ | $\begin{array}{r} 41 \\ 0.11 \\ \hline \end{array}$ | 448 | $\begin{array}{r} 102 \\ 0.23 \\ \hline \end{array}$ | $0,12$ | 0.02 | $\begin{array}{r}25 \\ 0.06 \\ \hline\end{array}$ | 362 | $\begin{array}{r} 80 \\ 0.22 \\ \hline \end{array}$ | 0.11 | 0.01 | $\begin{array}{r}14 \\ 0.04 \\ \hline\end{array}$ |
| All Ramps Totals <br> Acc/Loc |  |  | 836 | $\begin{array}{r} 137 \\ 0.16 \end{array}$ | $\begin{array}{r} 56 \\ 0.07 \end{array}$ | $\begin{array}{r} 78 \\ 0.02 \end{array}$ | $\begin{array}{r} 70 \\ 0.08 \\ \hline \end{array}$ | 929 | 231 118 16 60 <br> 0.25 0.13 0.02 0.05 |  |  |  | 755 | 188 $\overline{3} 3$ 16 <br> 0.25 0.12 0.02 |  |  | $\begin{array}{r}37 \\ 0.05 \\ \hline\end{array}$ |
|  |  |  | 281 |  |  |  |  | 415 |  |  |  |  |  |  |  |  | 334 |

Key. Sswp = Sideswipe
Rend $=$ Rear-end
Rovr $=$ Rollover
Loc $=$ Locatlon (Conilict Area)

| Conflct Area | Accldents | Conflct Areas | Total <br> RTADT | Total <br> RTT <br> (millions) | Accidents <br> per <br> RTT |
| :--- | ---: | :---: | :---: | :---: | :---: |
| Upstream of Merge <br> Merge Ramp <br> Downstream of Merge <br> On Ramp | 151 | 331 | 175114 | 144 | 1.1 |
|  | 75 | 331 | 17514 | 144 | 1.9 |
|  | 75 | 339 | 175114 | 144 | 0.5 |
|  | 567 | 1332 | 704622 | 578 | 1.0 |

(a) On - Ramps

| Conflict Area | Accidents | Conflict Areas | Total <br> RTADT | Total <br> RTT <br> (millions) | Accidents <br> per <br> RTT |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Upstream of Diverge | 119 | 294 | 145088 | 119 | 1.0 |
| Diverge Ramp | 131 | 234 | 145088 | 119 | 1.1 |
| Downstream of Dlverge | 122 | 294 | 146088 | 119 | 1.0 |
| Off Ramp | 31 | 305 | 149500 | 123 | 0.7 |
|  | 463 | 1187 | 584764 | 480 | 1.0 |

(b) OH - Ramps

RTT (Ramp Truck Trips) in millions for the study perlod = RTADT * 820 days / 1,000,000 Accident rates are per million $R T$.
cannot involve merging trucks, and accidents downstream of diverge ramps cannot involve diverging trucks. Another complication is that accidents on the main lanes may involve trucks other than merging or diverging trucks. We do not compare accidents per other combinations of ramp and freeway ADT's of trucks and all vehicles, partly because we found a strong correlation between each of these ADT exposure measures. Instead, we report accidents per ramp truck trip for all conflict areas including upstream and downstream areas so as to use a consistent denominator for all rates.

Lengths of the upstream, downstream, and ramp connection areas will affect the number of accidents found to occur there. As explained in Chapter 4, the truck accident frequency per 0.05 mile section became very low and did not change significantly beyond 0.25 miles upstream of the diverge taper or merge gore. In the downstream direction, the accident frequency per 0.05 mile section became very low and did not change significantly beyond 0.15 miles downstream of the merge taper, and 0.20 miles downstream of the diverge gore. However, the average length of a merge connection area was 0.219 miles, versus 0.107 miles for a diverge connection area. Hence, it's partly a distance effect as to whether accidents occurred in the ramp connection areas versus downstream, but the sum of these two areas are very comparable. We later compare truck accidents per ramp truck VMT, which compensates for differences in these conflict area lengths.

Table 5.9 shows a two-way frequency table of accidents by ramp and conflict area. Table 5.9 also lists ramp truck trips in millions (RT1) for all conflict areas in the database of a given type where accidents may have occurred, including areas with no accidents. The third line listed for each conflict area shows accidents per RTT by ramp type, which shows that accidents occur most frequently in ramp connection areas (merge and diverge areas).

Table 5.9: Washington State Truck Accidents per Ramp Truck ADT


Key: $\quad$ RTT (Ramp Truck Thps ) In millions for the study perlod = RTADT *820 days $/ 1,000,000$
Acctdent rates are per million RTT.

In comparison to Table 5.3, which ignored differences in truck volumes by ramp type, the accident rate for all directional ramps is now significantly lower ( 0.78 per RTT) than for diamond, loop, or outer connector ramps. Diamond ramps, which had the lowest accident frequency per location in Table 5.3, now have the highest accident rate per ramp truck trip ( 1.26 per RTT) because they serve fewer trucks on average than other ramps. Also note the high rate of accidents on loop off-ramps ( 2.36 per RTT), which is mainly due to rollovers.

Excluding ramp type "other", a two-way analysis of variance showed these average accident rates to be significantly different by conflict area at the $95 \%$ confidence level, but not by ramp type. The average accident rates for diamond, loop, and outer connectors are not very different, and the rates within each ramp type vary a great deal by conflict area. Hence, despite the lower rate for directional ramps, the four average rates again did not vary significantly by ramp type, which is the same test outcome reported for the accident frequencies per conflict area, not taking ramp truck ADT into account. Otherwise, these rates differ by conflict area less than the accident frequencies (i.e., have a lower test power). Hence, some of the variation noted earlier was due to truck volume differences.

Table 5.10 shows accidents rates by accident type and conflict area, and ramp truck trips for all accident types and conflict areas where such accidents may have occurred. A two-way analysis of variance shows these average accident rates to be significantly different by accident type at the $95 \%$ level of confidence, but not by conflict area, which was the same result found for accident frequencies per conflict area, not taking ramp truck $A D T$ into account.

We next investigate whether stratifying ramps by high, medium, or low ADT of trucks or all vehicles on the ramp shows greater lane-changing difficulties at higher volumes or the risks of greater speeds at lower volumes. In Table 5.11, we grouped conflict areas together by whether ramp truck ADT was low, medium, or high. In Table 5.12, we grouped conflict areas together by whether ramp ADT of all vehicles was low,
medium, or high. These stratified results show truck accidents per RTT in all conflict areas to generally decrease with higher ADT's. . While truck accidents per location do increase with greater truck ADT (as indicated by Tables 5.6 and 5.7), the increase is relatively less than the increases in either truck ADT or the ADT of all vehicles.

This finding suggests that greater traffic volumes or truck volumes affect accident rates to only a limited extent. Two reasons may be that (i) lower traffic volumes allow greater speeds, which may lead to more accidents, and (ii) accidents are very random events, with many erroneous driver actions not resulting in accidents because of evasive avoidance maneuvers by that driver and others. One implication of finding that truck accidents and truck ADT's are not directly related is that sites with low accident rates per RTT may not compare so well if their low accident rates are simply due to high truck volumes. In our procedure to identify high-risk sites described in Chapter 6, we use accident frequencies per location to initially "flag" potential problem sites, and use accident rates per RTT and ramp truck VMT to warrant the need for additional investigation, site inspection, data gathering, and possible remedial action.

### 5.3 ACCIDENTS PER RAMP TRUCK VMT IN WASHINGTON

This section compares the same truck accident locations examined in the previous section taking ramp truck VMT into account. Table 5.13 shows numbers of ramps, accidents, cumulative ramp truck ADT's, ramp truck vehicle miles of travel in millions (RTVMT), and accidents per RTVMT for the four conflict areas discussed earlier. To calculate RTVMT, each ramp truck ADT was multiplied by its conflict area length, divided by one million, and multiplied by 820 days in the study period (January 1, 1993 to March 31, 1995). The upstream and downstream conflict area lengths were explained in Chapter 4. We calculated a specific length for each ramp and ramp connection area based on the route mile post data and geometric drawings provided by WSDOT.




Kby:
Mer_ups I Upstream of the Merge Area
Mer_dwnst a Downstream of the Merge Area
Divr ups = Upstream of the Diverge Area
Div_dwnst = Downstream of the Diverge Area
RTT (Ramp Truck Trtps ) in millions for the study period = RTADT *820 days / 1,000,000


Key: Sowp = Sldeswipe
Rend $a$ Rear-and
Rove = Roliove
RTT (Ramp Truck Ttipe) in millilons for the study pertod $=$ RTADT " 820 days / 1,000,000
Aretiant reles are oor mililon RTT.



Key: Soup a Sldermpe
Rend $=$ Rear-and
Rowt = Rolover
RTT( Ramp Truck Ttipa) In milliona lor the etudy perlad a RTAOT •820 deys / 1,000,000
Aocddori ratos ara acoddenta per mililon RTI.

Hence, the truck VMT of each upstream conflict area equals its ramp truck ADT multiplied by 0.25 miles. The truck VMT in each downstream conflict area equals its ramp truck ADT multiplied by 0.15 miles for merge ramps, and by 0.20 miles for diverge ramps. Since ramp lengths and ramp connection lengths (i.e., the accel/decel lane plus taper) vary between ramps, the ramp truck VMT of a ramp or ramp connection area equals its length multiplied by the ramp truck ADT. The length of a ramp is from where it intersects another road to where it joins the ramp connection area. We also calculated the length of each ramp-to-ramp connection, and added its VMT to the corresponding accident group or ramp type. While drawings from WSDOT fully showed each ramp connection area, they did not always fully show the length of every ramp. Hence, the lengths we calculated for some ramps were more approximate than lengths of the ramp connection areas.

Ramp truck VMT for each ramp is added just once to its sum for each conflict area regardless of whether none or many accidents occurred there. As explained in Chapter 4, we included ramp truck VMT's for conflict areas without accidents so as to most fully represent truck exposure. Since the lengths of these areas vary, RTVMT is different for each merge or diverge conflict area which leads to comparatively different accidents per RTVMT or RTT. In comparison to Table 5.8 where the average rate was 1.0 truck accidents per million RTT, the average rate of 4.0 truck accidents per million RTVMT means that the average conflict area length was 0.25 miles.

Table 5.14 shows a two-way frequency table of accidents by ramp and conflict area. Table 5.14 also shows the cumulative ramp truck VMT (RTVMT) for all ramp types and conflict areas in the database where such accidents may have occurred. Companing these accident rates for on-ramps and off-ramps, we see the highest rates in the merge/diverge connection areas of these ramps. Again note the total accident rate for directional ramps is significantly lower than for the other type ramps, and the high accident rate on loop off-ramps.

| Conflict Area | Accldents | Conflct Areas | Conflict <br> Area <br> Length | Total <br> RTADT | Total <br> RTVMT <br> (millions) | Accidents <br> per <br> RTVMT |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Upstream of Merge | 151 | 331 | 0.25 | 175114 | 36 | 4.2 |
| Merge Ramp | 267 | 331 | Vares | 175114 | 27 | 9.9 |
| Downstream of Merge | 74 | 331 | 0.15 | 175114 | 22 | 3.4 |
| On Ramp | 75 | 339 | Varles | 179280 | 55 | 1.4 |
|  | 567 | 1332 |  | 704622 | 140 | 4.1 |

(a) On-Ramps

| Conflict Area | Accidents | Conflict Areas | Conflict <br> Area <br> Length | Total <br> RTADT | Total <br> RTVMT <br> (millions) | Accidents <br> per <br> RTVMT |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Upstream of Diverge | 119 | 294 | 0.25 | 145088 | 30 | 4.0 |
| Dlverge Ramp | 131 | 294 | Varies | 145088 | 15 | 9.0 |
| Downstream of Diverge | 122 | 294 | 0.20 | 145088 | 24 | 5.1 |
| Off Ramp | 91 | 305 | Varies | 149500 | 52 | 1.7 |
|  | 463 | 1187 |  | 584764 | 120 | 3.8 |

(b) Off - Ramps

RTVMT (Ramp Truck VMT) in millions for the study period = RTADT * Conflict Area Length * 820 days / 1,000,000 Accident rates are per millon RTVMT

Table 5.14: Washington State Truck Accidents per Ramp Truck VMT


Key: RTVMT (Ramp Truck VMT) In mililons for the study period =RTADT * coninict area length * B20 / 1,000,000 Accident rates are per million RTVMT

The accident rates shown in Table 5.14 can now be compared by both conflict and ramp type to address the first question of interest listed in Section 3.2. A two-way analysis of variance showed these accident rates per ramp truck VMT to be significantly different by conflict area at the $95 \%$ confidence level, but not by ramp type, which is the same test outcome reported for Tables 5.3 and 5.9, not taking ramp truck VMT into account. However, these rates differ by conflict area more than for Tables 5.3 and 5.9 (i.e., have a higher test power). Hence, when both ramp truck volumes and travel distances are properly accounted for, accident rates per ramp truck VMT most significantly differ by conflict area, with rates in ramp connection areas (merge and diverge areas) being the highest by a significant margin. While this may be an expected outcome, the finding reinforces the need to focus ramp related safety concems on merge and diverge areas.

Table 5.15 shows a two-way table accidents rates by accident type and conflict area, and cumulative ramp truck VMT for all accident types and conflict areas where such accidents may have occurred. A two-way analysis of vaniance shows these accident rates to be significantly different by accident type at the $95 \%$ level of confidence, but not by conflict area, which is the same test outcome reported for Tables 5.5 and 5.10, not taking ramp truck VMT into account. The degree to which accident rates differ by accident type is not significantly affected by whether ramp truck ADT or VMT or neither was taken into account. This small variation in accident rates by accident type indicates that differences are not strongly related to truck travel volumes or distances. Although one may expect more rearend accidents in heavy congestion, accident types are often affected by driver actions (e.g., a sideswipe can result from the driver attempting to avoid a rearend collision on a short ramp).

We next investigate whether stratifying ramps by high, medium, or low VMT of trucks or all vehicles on the ramp shows greater lane-changing difficulties at higher volumes or the risks of greater speeds at lower volumes. In Table 5.16, we grouped conflict areas together by whether ramp truck VMT was low, medium, or high. In Table 5.17, we grouped conflict areas together by whether ramp VMT of all vehicles was low, medium, or high. These stratified results show truck accidents per RTVMT to
consistently decrease in all conflict areas with higher RTVMT's. While truck accidents per location do increase with greater truck exposure (as indicated by Tables 5.6 and 5.7), the increase is much less than the increases in either truck VMT or the VMT of all vehicles. Hence, greater overall VMT or truck VMT affect accident rates to a very limited extent.

Table 5.18 is a summary of Washington truck accident frequencies and rates by conflict area per ramp truck trip and ramp truck VMT. Note that the average accident rates are all nearly equal for merge and diverge ramps when not divided by conflict area, but very different when separated by conflict area. This finding shows the importance of examining the accident history of a ramp by conflict area rather than of the whole ramp in order to identify possible problem spots.

### 5.4 COMPARISON OF ACCIDENTS PER RAMP IN THREE STATES

Since we were not able to obtain ramp truck ADT's for Colorado or Califomia, we limit our comparisons in this section to accident frequencies per ramp type. We did have freeway ADT's and truck percentages for most Califormia interchanges, and for some Colorado interchanges. Thus, we tried with Washington data to estimate both ramp ADTs and ramp truck ADTs from freeway ADT's and freeway truck percentages. The results were far too uncertain to use this approach to estimate ramp truck ADT's in Colorado or Califomia with which to make valid comparisons of accidents per ramp truck ADT between these states.

Tables 5.19 lists numbers of ramps and accidents per ramp type for Colorado, California, and Washington. The accident frequencies for Washington State are the weighted means of the frequencies shown in the last two columns of Table 5.1(c). Since our Washington data was for 27 months but our Colorado and California data was for 36 months, Table 5.20 converts the data in Table 5.19 to a yearly basis.

Table 5.15: Washington State Truck Accidents per Ramp Truck VMT

|  | CONFLICT | RTVMT <br> (mifilons) | ACCIDENT TYPE |  |  |  | $\begin{aligned} & \text { Total } \\ & \text { \# of } \\ & \text { AcC } \end{aligned}$ | Accidents per million RTVMT |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AREA |  | Sldeswipe | Rear-end | Rollover | Other |  | Sideswipe | Rear-end | Rollover | Other |
| $\left\|\begin{array}{cc}  & R \\ & a \\ 0 & m \\ n & p \\ & s \end{array}\right\|$ | Mer_upsMergeOn-RampMer_dwnstTotal | 36 | 79 | 43 | 4 | 25 | 151 | 2.20 | 1.20 | 0.11 | 0.70 |
|  |  | 27 | 170 | 75 | 3 | 19 | 267 | 6.29 | 2.77 | 0.11 | 0.70 |
|  |  | 65 | 36 | 7 | 18 | 14 | 75 | 0.65 | 0.13 | 0.33 | 0.25 |
|  |  | 22 | 38 | 16 | 1 | 16 | 74 | 1.76 | 0.74 | 0.05 | 0.88 |
|  |  | 140 |  |  | 26 | 77 | 567 | 2.31 | 1.01 | 0.19 | 0.55 |
| $\begin{array}{\|ll\|} \hline & R \\ 0 & a \\ 1 & m \\ 1 & p \\ & s \end{array}$ | Div_ups Diverge Oft_Ramp Dlv_dwnst Total | $\begin{aligned} & 30 \\ & 15 \\ & 62 \\ & 24 \\ & \hline \end{aligned}$ | 68 40 |  | $\begin{array}{\|l} \hline 1 \\ \hline 3 \\ \hline \end{array}$ | 20 | 119 | 1.85 | 1.34 | 0.03 | 0.67 |
|  |  |  | 72 | 39 |  | 17 | 131 | 4.93 | 2.67 | 0.21 | 1.16 |
|  |  |  | 33 | 18 | 20 | 22 | $\frac{91}{122}$ | 0.63 | 0.31 | 0.38 | 0.42 |
|  |  |  | 70 | 31 | 0 | 21 |  | 2.94 | 1.30 | 0.00 | 0.88 |
|  |  | 120 | 233 | 128 | 24 | 80 | 463 | 1.94 | 1.05 | 0.20 | 0.67 |
|  | Totals | 260 | 556 | 267 | 50 | 157 | 1030 | 2.14 | 1.03 | 0.19 | 0.60 |

Key: Mer_ups $=$ Upstream of the Merge Area
Mer_dwnst a Downstream of the Merge Area
DN_ups = Upstream of the Diverge Area
Div_dwnst $=$ Downstream of the Diverge Area
RTVMT (Ramp Truck VMT) in millions for the study period =RTADT * connlict area length * $820 / 1,000,000$




Koy: Sowp = Sldoewtpe
Rend = Reaf-end
Rovr = Rollover
RIVMT (Ramp Truck VMT) in minlons for the study perlod -RTADT * conflct ares iength * 820 / 1,000,000
Acelfont rites ars por million RTVMT



Key: Sswp = Sideawipe
Rend $\pm$ Rear-and
Rovt - Roliover
RTVMT (Ramp Truck VMJ) in mitiona for the etudy period -RTADT * conflet area length * 820/1,000,000 Accident rates are par mimion RTVMT


Key: Mer_ups = Upstream of the Merge Area
Mer_dwnst $=$ Downstream of the Merge Area
Dhr_ups = Upstream of the Diverge Area
Dlv_dwnst = Downstream of the Diverge Area
Aceident rates are per million RTT and million RTVMT.

| RAMP TYPE | 1 of Ramps | Percent | of Accidents | Percent | Average Accident Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Diamond | 27 | 30.3 | 49 | 25.9 | 1.81 |
| Loop | 12 | 13.5 | 28 | 14.8 | 2.33 |
| Outercomn | 11 | 12.4 | 17 | 8.0 | 1.55 |
| Directional | 39 | 43.8 | 95 | 50.3 | 2.44 |
| Other | 0 | 0.0 | 0 | 0.0 | 0.00 |
| Total | 89 | 100.0 | 189 | 100.0 | 212 |

Colorado Accidents

| $\begin{aligned} & \text { RAMP } \\ & \text { TYPE } \end{aligned}$ | sof Rampa | Percent | 5 of Acodiends | Peroent | Avernge Acchent Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Diamond | 19 | 3.9 | 59 | 5.6 | 3.11 |
| Loop | 25 | 5.1 | 57 | 5.4 | 228 |
| OuterCom | 23 | 4.7 | 33 | 3.1 | 1.43 |
| Orection: | 324 | 65.9 | 797 | 75.8 | 2.46 |
| Other | 104 | 20.5 | 106 | 10.1 | 1.05 |
| Total | 492 | 100.0 | 1052 | 100.0 | 214 |

Califomia Accidents

| RAap TMPE | Ead Pempat | Percend | tof Acokderds | Percen | Average Acodent Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Dismond | 310 | 48.9 | 490 | 47.6 | 1.58 |
| Loop | 81 | 12.6 | 134 | 13.0 | 1.65 |
| Outercorn | 59 | 0.2 | 100 | 9.7 | 1.69 |
| Dtrectional | 152 | 23.6 | 269 | 26.1 | 1.77 |
| Other | 42 | 6.5 | 37 | 3.6 | 0.88 |
| Totas | 644 | 1000 | 1030 | 100.0 | 1.60 |

Washington Accidents

Table 5.19: Comparison of Truck Accidents in Three States by Ramp Type

| FAMP TYPE | $\begin{aligned} & \text { of } \\ & \text { Rarmps } \end{aligned}$ | Percert | Mof Acciderts peryear | Percent | Average <br> Aceldend <br> Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Diamond | 27 | 30.3 | 16 | 25.9 | 0.60 |
| Loop | 12 | 13.5 | 9 | 14.8 | 0.78 |
| OuterCom | 11 | 124 | 6 | 9.0 | 0.52 |
| Directional | 39 | 43.8 | 32 | 50.3 | 0.81 |
| Other | 0 | 0.0 | 0 | 0.0 | 0.00 |
| Totas | 89 | 100.0 | 6 | 100.0 | 0.71 |

Colorado Accidents

| $\begin{aligned} & \text { RAMP } \\ & \text { TYPE } \end{aligned}$ | $\begin{gathered} \text { Hof } \\ \text { Remps } \end{gathered}$ | Pucent | * of Acclderts per year | Parcert | Averuge Accidert <br> Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Dismond | 19 | 3.9 | 20 | 5.6 | 1.09 |
| Loop | 25 | 5.1 | 19 | 5.4 | 0.76 |
| Outerconn | 23 | 4.7 | 11 | 3.1 | 0.48 |
| Directional | 324 | 65.9 | 266 | 75.8 | 0.82 |
| Other | 104 | 20.5 | 35 | 10.1 | 0.35 |
| Total | 4 | 100.0 | 351 | 100.0 | 0.71 |

Califomla Accidents

| $\begin{aligned} & \text { PARP } \\ & \text { TYPE } \end{aligned}$ | $\begin{gathered} \text { II of } \\ \text { Remps } \end{gathered}$ | Percent | a of Acchterts per yeer | Percent | Avereqe Accident Frequency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Damond | 310 | 48.1 | 218 | 47.5 | 0.70 |
| Leop | B1 | 12.6 | 00 | 13.0 | 0.74 |
| Outerconn | 59 | 92 | 44 | 9.7 | 0.75 |
| Dinectionat | 152 | 23.6 | 120 | 26.1 | 0.78 |
| Other | 12 | 6.5 | 16 | 3.6 | 0.39 |
| Tood | 64 | 1000 | 458 | 1000 | 0.71 |

Washington Accidents

Table 5.20: Comparison of Truck Accidents per Year in Three States by Ramp Type

### 5.5 CONCLUSIONS AND IDENTIFICATION OF HIGH-RISK SITES

It is mostly coincidental that the mean truck accident frequency per ramp for all ramp types was 0.71 per year in each of these states. The data in Colorado and Califomia was for 1991-1993, while the data for Washington was for 1993-early 1995. The ramp types of the analysis interchanges were distributed differently in each state, and although we did not have ramp truck volumes for Colorado and Califomia, these would also be distributed differently from those in Washington.

Yearly accident frequencies per directional ramp were very similar for all three states, and only slightly higher than for loop ramps. Yearly accident frequencies per loop ramp were also very similar for all three states. As shown by the last line of Table 5.14, the accident rate per ramp truck VMT for loop ramps in Washington (5.70) is much greater than for directional ramps (3.36). Relative rates per ramp truck VMT differ from relative frequencies per ramp, since directional ramps are generally longer and more heavily traveled. Because the accident frequencies per directional ramp and loop ramp are so consistent in all three states, we expect loop ramps to have higher accident rates per ramp truck VMT than directional ramps in both Colorado and California as they do in Washington.

The yearly accident frequencies per diamond ramp are less similar between states. If we combine Colorado and Califomia, the average yearly accident frequency is 0.78 per diamond ramp compared to 0.76 per loop ramp. These frequencies are not statistically different from each other or from the comparable frequencies for Washington. As shown by the last line of Table 5.14, the accident rate per ramp truck VMT for diamond ramps in Washington (4.93) is lower than for loop ramps (5.70) but much greater than for directional ramps (3.36). Our sampling of Colorado and Califomia interchanges does not allow us to confidently state how these rates may compare for these states, but we expect that they will compare similarly to Washington if a wider sample were collected.

The yearly accident frequency per outer connector is lowest among ramps in Colorado and Califomia, but is roughly equal to the yearly frequencies for diamond, loop, and directional ramps in Washington. Outer connectors are similar to directional ramps in design and operational characteristics. Hence, it is somewhat surprising that the accident rate per ramp truck VMT in Washington as shown in Table 5.14 is similar for outer connectors (4.84) and diamond ramps (4.93). Since the accident frequency per outer connector is lowest among ramps in Colorado and Califomia, the accident rate per ramp truck VMT for outer connectors is probably similar to directional ramps in these two states if the data to make that calculation were known.

In conclusion, truck accidents per ramp truck VMT are likely to be highest for loop ramps in all three states if the data to make that calculation were known. In Washington where the accident sample is least biased, Table 5.14 shows that accidents per ramp truck VMT are highest for loop ramps by a significant margin. One implication of this finding is that a given loop ramp may have a high accident frequency compared to all ramp types, but not compared to loop ramps. Short of reconstruction, lower cost measures to reduce the accident rate at a loop ramp to be comparable with other nonloop ramps may be limited. Thus, to evaluate the effectiveness of an accident mitigation measure, before and after accident experiences ought to be examined within ramp types.

We have compared truck accident frequencies and rates for different ramp types, accident types, and conflict areas. Although the average accident statistics did not differ significantly by ramp type, there was a great deal of variation by conflict area within each ramp type. As we added more specific information related to ramp truck volumes and travel distances, the differences did become greater by ramp type and conflict area. These findings led us to recommend an incremental stepwise procedure for using accident data to identify hazardous ramps. The procedure is a simple comparison of the accident history for a given ramp to comparable averages for other ramp types, conflict areas, and accident types. We designed the procedure to be straightforward in its simplest application so that it would be easy to implement and use within emerging safety management systems.

Seven comparisons can be made of the accident frequency at a given ramp by one or more of three attributes (accident type, ramp type, and conflict area) to the accident distribution of other ramps in a state. These comparisons can be made:

1. By accident type for all ramp types and conflict areas.
2. By ramp type for all accident types and conflict areas.
3. By conflict area for all ramp types and accident types.
4. By accident type and ramp type for all conflict areas.
5. By accident type and conflict area for all ramp types.
6. By ramp type and conflict area for all accident types.
7. By accident type, ramp type, and conflict area.

Each additional attribute by which accidents are grouped reduces the sample size of accidents and ramps to which a given ramp is compared. Moreover, the likelihood (or ease) of obtaining data to classity accidents by these attributes is greatest for accident type, less for ramp type, and least for conflict area. With those considerations, we recommend performing comparisons $1,2,4,6$, and 7 (in that order) as numbered above. Comparisons 1,2 , and 4 do not require identitying the conflict area, the least obtainable data. Companisons 6 and 7 do require identifying the conflict area, but these comparisons are not necessary to warrant a site inspection and design evaluation. If a ramp is found to have a high frequency of accidents (1) overall, (2) by accident type, and (4) by accident and ramp type, then it probably warrants closer examination. Accident reports for that ramp would be studied, and accidents classified by conflict area and several other attributes such as vehicle type, weather, lighting, road condition, and driver actions. This information would then be used to determine whether improvements to geometric design, signage, or traffic controls are warranted considering various altematives and their costs.

Thus, the high-risk site identification procedure is as follows:

1. First, for a given ramp (all conflict areas combined), compare its frequency of all accident types over a multiyear analysis period to the frequency distribution of all accident types in all conflict areas at all other ramps of a state. If a given ramp lies above the $75^{\text {th }}$ percentile of this distribution, an initial flag is raised. The $75^{\text {th }}$ percentile is suggested by Basha \& Ramsey (1993) as an "initial check" to identify locations that may warrant further investigation. A higher or lower percentile might be considered after experience shows whether this percentile "flags" too many or too few locations that do or do not warrant further attention.
2. Second, for a given ramp (all conflict areas combined), compare its frequency of each accident type over a multiyear analysis period to the frequency distribution of each accident type in all conflict areas at all other ramps of a state. If any accident type of a given ramp lies above the 75th percentile of its distribution, a second flag is raised. Again, a higher or lower percentile might be considered.
3. Third, for a given ramp (all conflict areas combined), compare its frequency of each accident type over a multiyear analysis period to the frequency distribution of each accident type in all conflict areas at all similar type ramps of a state. If any accident type of a given ramp lies above the $75^{\text {th }}$ percentile of its distribution, a third flag is raised.

This first companison indicates whether the ramp has an unusual overall accident history in companison to all other statewide ramps, and requires minimal information. This second companison indicates whether the ramp has an unusual accident history for any particular accident type, knowing that data on conflict area and ramp type may not be available. The third comparison (number 4 in the prior list) indicates whether the ramp has an unusual accident history for any particular accident type in comparison to similar ramps, knowing that data on conflict area may still not be available. If all
comparisons indicate a potential problem, then further evaluation is recommended, leading to comparisons 6 and 7 if conflict area data is available for many other ramps of similar design in the state. If only one or two comparisons indicate a potential problem, then further evaluation may be considered depending on available resources.

The following is an example of applying the above procedure to the interchange of Interstate 25 and State Highway 34 in Colorado, which serves the cities of Greeley and Loveland. As shown by Figure 5.2, this interchange is a full cloverleaf, with four loop ramps and four outer connectors. The entire interchange had experienced 11 truck accidents in the years 1991-1993, of which 6 were overtums, and 4 were overtums on the loop ramp leading from westbound $\mathrm{SH}-34$ to southbound I-25.

Four truck accidents on one ramp in a three year period suggested a problem simply according to the first overall test. Four overtums on one ramp in a three year period more strongly indicated a problem according to the second test. Finally, even compared to other loop ramps, four truck accidents of any type in a three year period gave justification for a site inspection and design evaluation. Actions were taken to improve the lane markings and speed waming signs at this interchange, and the interchange continues to be monitored.

Since we were unable to obtain ramp truck trips or ramp truck VMT in Colorado, we were unable to make comparisons of ramps based on truck accident rates per those denominators. Moreover, since we found that truck accidents in Washington State were not directly proportional to truck trips or truck VMT, we caution the use of those accident rates to identify high-risk locations. We suggest that these rates be used at the next stage of evaluation if a location is found to have a high accident frequency according to tests 1,2 , and 4 , above. One reason may be higher truck volumes, but the extent of that effect at a given site must be further assessed.


Figure 5.2 Interchange Accidents at $\mathrm{I}-25$ and $\mathrm{SH}-34$ in Colorado

## Chapter Six

## CRITICAL EXAMINATION OF AASHTO STANDARDS FROM THE STANDPOINT OF TRUCK OPERATIONS AT INTERCHANGES

### 6.1 OVERVIEW

Devalopment of the highway infrastructure and development of the motor carrier industry are interrelated. Construction of the Interstate System in particular offered unprecedented economic opportunitles for the development of trucking. The need to increase the cargo transporting efficiency of trucks in tum led to the development of larger vehicles capable of carrying heavier loads. Critical dimensions and operational characteristics of these vehicles have a direct effect on highway design criteria. This portion of the report will identify the basic operational characteristics and dimensions of modem large trucks and examine their impact on highway design criteria through literature review and direct contacts with trucking organizations and vehicle manufacturers around the country.

The design philosophy formulated throughout various editions of the AASHTO Policy on Geometric Design always aimed at accommodating the largest design vehicle likely to use the highway facility with considerable frequency or a design vehicle with special characteristics. A "design vehicle" was defined as a selected motor vehicle the weight , dimensions and operating characteristics of which are used to establish highway design controls to accommodate a vehicle of a designated type. Accommodation of the design vehicle is achieved through geometric design standards, which provide a safe and efficient environment for traffic operations. Trucks generally impose greater demands on the highway facilities than passenger cars because they are wider, longer, heavier, less maneuverable, less stable, slower and more difficult to stop. Yet, over the years vehicle designers and manufacturers have made significant improvements to various truck components resulting in a safer and more efficient vehicle fleet. The connections between truck characteristics and related highway
design criteria are illustrated in Fig. 6.1. This self-explanatory drawing illustrates the numerous implications of truck dimensions and operating characteristics on highway design standards. These relationships as well as the trends in vehicle development will be discussed further in the report.

### 6.2 EFFECT OF VEHICLE DIMENSIONS ON ELEMENTS OF GEOMETRIC DESIGN

Over the years the evolution of commercial vehicles driven by the economic stimulus to lower the cost of cargo transport exerted greater and greater demands on the highway infrastructure. The largest design vehicle in the 1965 AASHTO Policy on Geometric Design of Rural Highways was the WB-50 semitrailer combination. The 1973 edition of the Geometric Design Policy introduced two additional design vehicles, one reflecting the dimensions of many buses at the time and another reflecting dimensions of the semitrailer-full trailer combination WB-60. In order to reflect the latest frends in motor vehicle manufacture and represent a composite of the vehicles currently in operation the 1990 edition of the Green Book added four more design vehicles to the design criteria. These vehicles are: WB-62, a design vehicle representative of a larger tractor-semitrailer combination allowed on selected highways by the Surface Transportation Assistance Act of 1982, WB-67 a design vehicle representative of a larger tractor-semitrailer grandfathered on selected highways by the Surface Transportation Assistance Act of 1982, WB-96 a design vehicle representative of tractor-semitrailer full trailer-full trailer combinations (triples) selectively in use, and WB-114 a design vehicle representative of larger tractor-semitraller-full trailer (tumpike doubles) selectively in use ( 1990 Green Book). Although tumpike doubles and triple trailers are not permitted on many highways, their manufacture and use warranted inclusion of these vehicles in the 1990 Green Book. Every successive publication of the AASHTO Policy on Geometric Design incorporated all previous design vehicles and introduced new ones, in an effort to capture present and future trends in vehicle manufacture and design. As a result, the 1990 edition has 15 different design vehicles,


Figure 6.1
eight of which are trucks. Table 6.1 shows design vehicle dimensions and table 6.2 shows minimum tuming radii of design vehicles included in the 1990 Green Book. Vehicle length, width, number of axles, distance between axles, number of articulation points and offtracking are design controls which define geometric design requirements of intersections and horizontal curves.

| Design Vehicte Type | Symbol | Dimersion (t) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Onerall |  |  | Overhang |  | WB1 | $\mathrm{WH}_{2}$ | S | T | W8, ${ }^{\text {S }}$ | $\mathrm{WB}_{4}$ |
|  |  | Hetats | Widh | Lengh | Frant | REAR |  |  |  |  |  |  |
| Prasengerar | P | 4.25 | 7 | 19 | 3 | 5 | 11 |  |  |  |  |  |
| Single wnit truck | SU | 13.5 | 8.5 | 30 | 4 | 6 | 20 |  |  |  |  |  |
| Single onit bus | BUS | 13.5 | 8.5 | 40 | 7 | 8 | 25 |  |  |  |  |  |
| Articutated las | A-bus | 10.5 | 8.5 | 80 | 8.5 | 9.5 | 18 |  | 4* | $20^{4}$ |  |  |
| Combination trucks |  |  |  |  |  |  |  |  |  |  |  |  |
| Intermedine semitrailer | WB-40 | 13.5 | 8.5 | So | 4 | 6 | 13 | 27 |  |  |  |  |
| Lerge semitrailer | WB-50 | 13.5 | 8.5 | 55 | 3 | 2 | 20 | 30 |  |  |  |  |
| "Double Botton" semi-traiker-fult-raiker | WB-60 | 13.5 | 8.5 | 65 | 2 | 3 | 9.7 | 20 | $4^{6}$ | $5.4{ }^{6}$ | 20.9 |  |
| Iruerstme Seavitrailer | WP-62* | 13.5 | 8.5 | 69 | 3 | 3 | 20 | 40-42 |  |  |  |  |
| Interstare Semitraita | WB-67** | 13.5 | 8.5 | 74 | 3 | 3 | 20 | 45-47 |  |  |  |  |
| Triple Semitraile | WB-95 | 13.5 | 8.5 | 102 | 2.3 | 3.3 | 13.5 | 20.7 | $3.3{ }^{\text {d }}$ | 6 | 21.7 | 21.7 |
| Trupike Double Serntrailer | WB-114 | 13.5 | 8.5 | 118 | 2 | 2 | 27 | 40 | $2^{2}$ | 6 | 44 |  |
| Recremion vehicle |  |  |  |  |  |  |  |  |  |  |  |  |
| Monrthome | MH |  | 8 | 30 | 4 | 6 | 20 |  |  |  |  |  |
| Car and carmpar triter | P/t |  | 8 | 49 | 3 | 10 | 11 | 18 | 5 |  |  |  |
| Car and boat wriker | P/B |  | 8 | 42 | 3 | 8 | 11 | 15 | 5 |  |  |  |
| Acoar Home and Boar Trizer | MH/B |  | 8 | 33 | 4 | 8 | 20 | 21 | 6 |  |  |  |

- Detign veticie wilt 48' uraiter ar edopted in 19872 STAA
(Surface Tramportion Arsisarice Act)
-4 - Desigan while widh S3' triler as ymadicthered in
198257 A (Surtice Tranoportinion Acristance Act)
- C Corbined dimerion 24. split es extimetes.
b = Corabined dimesion 9.1. split is exlimated.
$c=$ Combinod dionemsiga 8 , split is extimered.
d - Combined dimention 9.3, uplat is estinested.

$S$ ir the ditionce from die gar effective ave to the tiech poind.
T it the fictonce fron the trich prind to the lond effexive axle of the followieg unit.
Table 6.1: Design Vehicle Dimensions


[^0]Table 6.2: Minimum Tuming Radii of Design Vehicles

The Society of Automotive Engineers (F. Jindra, Scale Models of Offtracking...) defines offtracking as "The difference in the path of the first inside front wheel and the last inside rear wheel as a vehicle negotiates a curve. Figures 6.2 and 6.3 (Heald. Use of WHI Offtracking Formula) illustrate this phenomenon for single and double combinations traveling on a highway ramp where offtracking is fully contained within the roadway width.


Figure 6.2: Schematic of Turning Track Components and Terms


Figure 6.3: Graphic Representation of Steady-State Offtracking

The most important design parameter related to offtracking is the swept path width which is the controlling factor in computing the minimum required pavement width for tuming roadways and intersections. Fig. 6.4 (AASHTO GB) shows the swept path width for low speed offtracking in a 90-degree tum. Offtracking and corresponding swept path width can be determined for various design vehicles using several of the accepted methods. These methods include: a computer simulation program developed by CALTRANS (Fong and Chenu), and the Westem Highway Institute (WHI) offtracking formula (Offtracking Characteristics of Trucks). It is important to understand that WHI formulae provide theoretical steady-state maximum values of offtracking, while the computer simulation model determines the maximum amount of offtracking for a specific degree of tum. The amount of offtracking predicted by the WHI and simulation model match only if the degree of tum is sufficient to allow the vehicle to reach its steady state tuming condition. For smaller angle and shorter radius tums, the differences between the WHI and CALTRANS methods can be substantial. The field tests conducted by CALTRANS (Fong and Chenu) support offtracking values generated by the CALTRANS simulation model. The important advantage of the CALTRANS simulation model is that it can keep track of where the truck is as it negotiates the tum. The amount of offtracking is reported along the tum to and from the point of maximum offtracking.


Figure 6.4: Swept Path Width in a 90 Degree Tum

### 6.3 EFFECT OF OFFTRACKING ON DESIGN OF RAMPS AND INTERSECTIONS

The study by Harwood et al., which evaluated offtracking and swept width requirements for the design vehicles included in the 1984 Green Book stressed the need to include the STAA vehicles. The 1990 edition of the Green Book added WB62, WB-67, WB-96 and WB-114. While the 1990 Green Book included these new design vehicles it did not address the costly and sensitive issue of accommodating them on the highways through extensive retrofitting of interchanges and intersections. Harwood et al., presented estimates of the construction costs associated with widening required to accommodate vehicles larger than WB-50 at intersections (Table 6.3).

| Tuming redius (ft) | Additional paved aree per quadrant (ftz). |  |  | Additional construction cost ${ }^{\text {a }}$ per quadrant |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 45-f t \\ \text { semftrifier } \end{gathered}$ | $\begin{gathered} 48-f t \\ \text { senitrailer } \end{gathered}$ | $\begin{gathered} 53-f t \\ \text { senitrailer } \end{gathered}$ | $\begin{gathered} \text { 45-ft } \\ \text { seuftrafier } \end{gathered}$ | $\frac{4}{48-f t}$ <br> senitrafier | $\begin{gathered} 53 . f t \\ \text { semitrailer } \end{gathered}$ |
| 50 | 900.8 | 1,226.1 | 1,849.6 | \$ 2.620 | \$ 3,570 | \$5,380 |
| 60 | 1,995.6 | 1,423.0 | 2,283.0 | 3.190 | 4.140 | 6.640 |
| 80 | 1,243.4 | 1,673.0 | 2,939,0 | 3,620 | 4.870 | 8,550 |
| 100 | 1,498.1 | 2,085.6 | 3,319.3 | 4,360 | 6,070 | 9,660 |
| 150 | 1,601.8 | 2,242.5 | 3.752 .8 | 4.680 | 6,530 | 10.920 |
| 200 | 1,631.6 | 2,249.6 | 3,732.8 | 4.750 | 6,550 | 10,860 |
| 250 | 1.554.3 | 2.331 .5 | 3,730.3 | 4.520 | 6,790 | 10,860 |
| 300 | 1,403.1 | 2,245.0 | 3,648.1 | 4,020 | 6,533 | 10,620 |

Table 6.3: Cost Estimates for Widening at Intersections

This cost data shows that intersections alone will require very substantial investments. According to a survey of 46 States conducted by the DOT and AASHTO (The Feasibility of a Nationwide Network of LCV's, USDOT, FHWA-1986) "a majority of interchange ramps had inadequate geometry to accommodate the offtracking of some larger combinations. States estimated that approximately 43 percent of the Interstate interchanges could safely accommodate triples, 34 percent could accommodate Rocky Mountain doubles and 25 percent could accommodate tumpike doubles. The States estimated, however, that only about half of all

Interstate interchanges can safely accommodate the tractor-48-foot semitrailer combinations mandated by the 1982 STAA". There is little disagreement as to what $^{\text {n }}$ the steady state offtracking/swept width requirements are regardless of the method employed. The larger question, which remains unaddressed, is who will pay for the infrastructure improvements associated with accommodating these vehicles. Presently, there is no national consensus on this issue.

### 6.4 BRAKING ABILITY OF TRUCKS vs. AASHTO STOPPING SIGHT DISTANCE AND DECELERATION REQUIREMENTS

Stopping sight distance requirements in the 1990 edition of the Green Book are based on the operating characteristics and dimensions of passenger cars as opposed to heavy commercial vehicles. In fact AASHTO does not recommend these standards for truck operations. At the same time however, there is no separate stopping sight distance for trucks, partially because of the elevated seat position which allows the truck driver to see further ahead and partially because of economic considerations. It is relevant to note that truck drivers can only see further if the controlling sight distance is associated with vertical obstructions such as crest vertical curves and not horizontal sight restriction. To circumvent this limitation the Green Book recommends exceeding minimum recommended values and providing a facility with a desirable range of design values. This approach allows flexibility for individual engineers to accommodate trucks based on information on the composition of present and anticipated traffic streams. Table 6.4 shows stopping site distances for various ranges of design values. (AASHTO Green Book, 1990).

| Destgn Speed (mph) | Assumed Speed for Condition (mpha) | Brake Reaction |  | Coefficient of Friction 1 | Braking Distance on Level (f) | Stopping Sight Distance |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Roumded |
|  |  | $\begin{aligned} & \text { Time } \\ & \text { (sec) } \end{aligned}$ | Distance (in) <br> (1) |  |  | Computed (fi) | for Design <br> (i) |
| 20 | 20-20 | 2.5 | 73.3-73.3 |  | 0.40 | 33.3-33.3 | 106.7-106.7 | 125-125 |
| 25 | 24-25 | 2.5 | 88.0-91.7 | 0.38 | 50.5-54.8 | 138.5-146.5 | 150-150 |
| 30 | 28-30 | 2.5 | 102-7-110.0 | 0.35 | 74.7-85.7 | 177.3-195.7 | 200-200 |
| 35 | 32-35 | 2.5 | [17.3-128.3 | 0.34 | 100.4-120.1 | 217.7-248.4 | 225-250 |
| 40 | 36-40 | 2.5 | 132.0-146.7 | 0.32 | 135.0-166.7 | 267.0-313.3 | 275-325 |
| 45 | 40-45 | 2.5 | 146.7-165.0 | 0.31 | 172.0-217.7 | 318.7-382.7 | 325-400 |
| 50 | 44.50 | 2.5 | 161.3-183.3 | 0.30 | 215.1-277.8 | 376.4-461.1 | 400-475 |
| 55 | 48-55 | 2.5 | 176.0-201.7 | 0.30 | 256.0-336.1 | 432.0-537.8 | 450-550 |
| 60 | 52-60 | 2.5 | 190.7-220.0 | 0.29 | 310.8-413.8 | 501.5-633.8 | 525-650 |
| 65 | 55-65 | 2.5 | 201.7-238.3 | 0.29 | 347.7-485.6 | 549.4-724.0 | 550-725 |
| 70 | 58-70 | 2.5 | 212.7-256.7 | 0.28 | 400.5-583.3 | 613.1-840.0 | $625-850$ |

Table 6.4: Stopping Sight Distance (Wet Pavement)

Fancher (Site Distance Problems Related to Large Trucks) has developed a model used to predict the braking distances for trucks under controlled and locked
wheel deceleration with new and worn tires. Figure 6.5 (Site Distance Problems Related to Large Trucks) shows that braking distances predicted by Fancher are substantially longer than distances recommended in AASHTO policy. According to Fancher, ${ }^{a}$ The notion of attempting to design for trucks passing over crest vertical curves at 60 mph or faster may not be economically reasonable. At 60 mph the braking distances for controlled braking exceed the AASHTO policy for 80 mph . At 55 mph , controlled stops of trucks require braking distances that are approximately equal to the AASHTO policy for $80 \mathrm{mph}^{\prime \prime}$.


Figure 6.5: Truck Braking Distance
The discrepancy between the heavy vehicle's ability to come to a controlled stop and AASHTO design standards may be related to accidents involving commercial vehicles. Based on the analysis of national and state accident data, NHTSA (National Highway Traffic Safety Administration) estimates that between 10 percent and 15 percent of the crashes involving heavy combination vehicles involved braking induced instability or loss of control. In order to improve the directional stability, control characteristics and stopping distances of commercial vehicles NHTSA has issued a set of four regulations designed to address this important safety issue. The first one, Stability and Control of Medium and Heavy Vehicles During Braking mandated that new commercial vehicles be equipped with an antilock brake system (ABS) by March 1, 1997. The second one, Stopping

Distance requirements for Vehicles Equipped With Air Brake Systems specified distances in which different types of medium and heavy vehicles equipped with air brakes must come to a controlled stop from 60 mph on a high coefficient of friction surface. The third regulation Stopping Distance Requirements for Vehicles Equipped With Hydraulic Brake Systems is similar to the second but targets vehicles equipped with hydraulic brakes. The proposed braking distances for both air and hydraulic braking systems are presented below (49 CFR Part 571).

| Vehicle Type | Speed | Surface PFC | Stopping Distance |
| :---: | :---: | :---: | :---: |
| Loaded and Unloaded Buses | 60 mph | 0.9 | 280 ft |
| Loaded Truck Tractors with <br> Braked Control Trailer | 60 mph | 0.9 | 280 ft |
| Loaded Truck Tractors with <br> Unbraked Control Trailer | 60 mph | 0.9 | 355 ft |
| Loaded Single-Unit Trucks | 60 mph | 0.9 | 310 ft |
| Unloaded Single-Unit Trucks and <br> Truck Tractors (Bobtail) | 60 mph | 0.9 | 335 ft |

Table 6.5: Stopping Distances from 49 CFR Part 571

Stopping distance is comprised of the distance traveled while the driver recognizes and reacts to a hazard by applying brakes and the actual braking distance required to bring the vehicle to a complete stop. The reaction time t assumed in the AASHTO stopping site distance (Table 6.4) is 2.5 seconds which at 60 mph corresponds to 220 ft . The approximate braking distance of a vehicle on a level roadway is determined by the use of the following formula ( 1990 GB ):

```
\(d=V^{2} / 30 f\) (1)
\(d=\) braking distance
\(V=\) initial speed, mph
\(f=\) coefficient of friction between tires and roadway
```

Assuming that during the tests which resulted in these regulations the test drivers were expecting to stop and their reaction and brake activation time can be reduced to 2.0 seconds which at 60 mph corresponds to a traveled distance of 176 feet. Let's now convert the stopping distances on dry pavement during the tests to stopping distances of the same vehicles on wet pavement and compare with AASHTO criteria. This can be accomplished by multiplying the braking distance on dry pavement by the ratio of $f(d) / f(w)$ and adding it to the distance traveled during the reaction and brake activation period. Where $f(d)=0.9$ represents dry pavement conditions and $f(w)=0.29$ represents wet pavements. Table 6.5 presents the results of this comparison.

|  | New Regulations <br> dry pavement <br> stopping distance | $f(\mathrm{~d}) \mathrm{f}(\mathrm{w})=$ <br> $0.9 / .29$ | New Regulations <br> wet pavement <br> stopping distance | AASHTO wet <br> pavement stopping <br> sight distance |
| :---: | :---: | :---: | :---: | :---: |
| Loaded/unl. buses | 280 ft | 3.1 | 498.4 ft | $525-650 \mathrm{ft}$ |
| Loaded trucks with <br> braked control trailers | 280 ft | 3.1 | 498.4 ft | $525-650 \mathrm{ft}$ |
| Loaded trucks with <br> unbraked control <br> trailers | 355 ft | 3.1 | 730.9 ft | $525-650 \mathrm{ft}$ |
| Loaded single unit <br> trucks | 310 ft | 3.1 | 591 ft | $525-650 \mathrm{ft}$ |
|  <br> Bobtail | 335 ft | 3.1 | 668.9 ft | $525-650 \mathrm{ft}$ |

Table 6.6: Comparison of AASHTO Criteria and New ABS/Stopping Distance Requirements

This exercise shows that these new stopping distances will bring the braking ability of new commercial vehicles in line with AASHTO standards.

The minimum deceleration requirements for exit terminals required by AASHTO for flat grades of $2 \%$ or less are also well within capabilities of most trucks equipped with ABS.

| Highway Design Speed, V (mph) | Average <br> Rumaling <br> Speed, $V_{\text {a }}$ <br> (mph) | Doctieration Length, L (fi) <br> For Destgn Speed of Exilt Curve, V' (mpb) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Stop Coadition | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 5 | 0 |
|  |  | For Arersge Running Speed an Exil Curve, $\mathrm{V}_{\mathrm{a}}^{\prime}$ (mpta) |  |  |  |  |  |  |  |  |  |
|  |  | 0 | 14 | 18 | 22 | 26 | 30 | 36 | 40 | 4 |  |
| 30 | 28 | 235 | 185 | 160 | 140 | - | - | - | - |  |  |
| 40 | 36 | 315 | 295 | 265 | 235 | 185 | 155 | - | - | - |  |
| 50 | 44 | 435 | 405 | 385 | 355 | 315 | 285 | 275 | 175 |  |  |
| 60 | 52 | 530 | 500 | 490 | 460 | 430 | 410 | 340 | 300 | 240 |  |
| 65 | 55 | 570 | 540 | 530 | 490 | 480 | 430 | 380 | 330 | 280 |  |
| 70 | 58 | 615 | 590 | 570 | 550 | 510 | 490 | 430 | 390 | 340 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 6.7: Minimum Deceleration Lengths for Exit Terminals - All Main Highways Flat Grades - 2 Percent or Less

The last NHTSA Regulation on this issue, Parts and Accessories Necessary for Safe Operation; Antilock Brake Systems, addresses maintenance requirements related to ABS. While these requirements will go a long way in improving traffic safety it is important to realize that they apply only to new trucks and buses and will not require retrofitting of the existing fleet, which means that safety improvement is expected to take place gradually and over time.

### 6.5 RELATIONSHIP BETWEEN SUPERELEVATION / CURVATURE AND ROLLOVER THRESHOLD

The maximum degree of curvature for a given speed is determined from the maximum rate of superelevation and the maximum allowable friction factor. This relationship is based on the laws of Newtonian physics and is developed on the assumption that the vehicle is in equilibrium with respect to the superelevated plane of the roadway surface as it travels around the curve. Figure 6.6 shows the forces acting on a vehicle on a horizontal curve section.


Source: Redrawn from Domald R. Drew, Traffic Flow Theory and Control, copyright © 1968, McGrew-Hill Book Company.
where
$a_{c}=$ acceleration for curvilinear motion $=u^{2} / R$
$R=$ radius of the curve
$W=$ weight of the vehicle
$g=$ acceleration of gravity

Figure 6.6: Forces Acting on a Vehicle Traveling on a Horizontal Curve Section

When the vehicle is in a state of equilibrium the sum of all forces projected on the roadway plane is equal to zero. In other words the vehicle is not sliding up and down with respect to the roadway surface as it travels around the curve. As a result, the relationship between speed, curvature, superelevation and side friction can be expressed as follows:

$$
R=V^{2} / 15(e+f)
$$

The AASHTO standard developed on the basis of this relationship has not changed in over 30 years and is presented in Table 6.8 (GB 1990).

| Destgan <br> Speed <br> (mph) | Meximum <br> $\varepsilon$ | $\begin{gathered} \text { Meximum } \\ f \end{gathered}$ | $\begin{aligned} & \text { Toleal } \\ & (c+1) \end{aligned}$ | Maximum <br> Degree of Curve | Ronnded Mocimurn Degree of Curve | Maximam Redius <br> ( At ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | . 04 | . 17 | . 21 | 44.97 | 45.0 | 127 |
| 30 | . 04 | . 16 | . 20 | 19.04 | 19.0 | 302 |
| 40 | . 04 | .15 | . 19 | 10.17 | 10.0 | 573 |
| 50 | . 04 | . 14 | . 18 | 6.17 | 6.0 | 955 |
| 55 | . 04 | . 13 | . 17 | 4.83 | 4.75 | 1.186 |
| 60 | . 04 | . 12 | . 16 | 3.81 | 3.75 | 1,528 |
| 20 | . 06 | .17 | . 23 | 49.25 | 49.25 | 116 |
| 30 | . 06 | . 16 | . 22 | 20.94 | 21.0 | 273 |
| 40 | . 06 | . 15 | . 21 | 11.24 | 11.25 | 509 |
| 50 | . 06 | .14 | . 20 | 6.85 | 6.75 | 849 |
| 55 | . 06 | . 13 | . 19 | 5.40 | 5.5 | 1,061 |
| 60 | . 06 | . 12 | . 18 | 4.28 | 4.25 | 1,348 |
| 65 | . 06 | . 11 | . 17 | 3.45 | 3.5 | 1.637 |
| 70 | . 06 | . 10 | . 16 | 2.80 | 2.75 | 2,083 |
| 20 | . 08 | . 17 | . 25 | 53.54 | 53.5 | 107 |
| 30 | . 08 | . 16 | . 24 | 22.84 | 22.75 | 252 |
| 40 | . 08 | . 15 | . 23 | 12.31 | 12.25 | 468 |
| 50 | . 08 | . 14 | . 22 | 7.54 | 7.5 | 764 |
| 55 | . 08 | . 13 | . 21 | 5.97 | 6.0 | 960 |
| 60 | . 08 | . 12 | . 20 | 4.76 | 4.75 | 1,206 |
| 65 | . 08 | . 11 | . 19 | 3.85 | 3.75 | 1,528 |
| 70 | . 08 | .10 | . 18 | 3.15 | 3.0 | 1,910 |
| 20 | . 10 | .17 | . 27 | 57.82 | 58.0 | 99 |
| 30 | .10 | . 16 | . 26 | 24.75 | 24.75 | 231 |
| 40 | . 10 | . 15 | . 25 | 13.38 | 13.25 | 432 |
| 50 | . 10 | .14 | - 24 | 8.22 | 8.25 | 694 |
| 55 | . 10 | . 13 | . 23 | 8.53 | 6.5 | 877 |
| 60 | . 10 | . 12 | . 22 | 523 | 5.25 | 1,091 |
| 65 | .10 | . 11 | . 21 | 4.25 | 4.25 | 1,348 |
| 70 | . 10 | . 10 | .20 | 3.50 | 3.5 | 1,637 |
| 20 | . 12 | . 17 | . 29 | 62.10 | 62.0 | 92 |
| 30 | . 12 | . 16 | . 28 | 26.65 | 26.75 | 214 |
| 40 | . 12 | . 15 | . 27 | 14.46 | 14.5 | 395 |
| 50 | . 12 | . 14 | . 26 | 8.91 | 9.0 | 637 |
| 55 | . 12 | . 13 | . 25 | 7.10 | 7.0 | 807 |
| 60 | . 12 | . 12 | . 24 | 5.71 | 5.75 | 996 |
| 65 | . 12 | . 11 | 23 | 4.66 | 4.75 | 1206 |
| T0 | . 12 | . 10 | 22 | 3.85 | 3.75 | 1528 |

NOTE: In recognition of grafey considerations, use of ein $=0.04$ chould be limited to urfala conditious. ${ }^{\text {Chended ming romed maximum degree of curve }}$

Table 6.8: Maximum Degree of Curve and Minimum Radius Determined for Limiting Values of e and f, Rural Highways and High-Speed Uban Streets.

The only reference to trucks in relationship to curve/superelevation standards in the 1990 Policy on Geometric Design is on page 142. "Also some trucks have high centers of gravity and some cars are loosely suspended on the axles. When these vehicles travel slowly on steep cross slopes, a high percentage of the weight
is carried by the inner tires." In other words truck characteristics are not explicitly considered in the curvature /superelevation design criteria which is based solely on the vehicle characteristics of passenger cars. Given its low center of gravity the passenger car will slide off the road before a rollover occurs. Because the center of gravity of a loaded truck is located much higher the opposite is often true. Truck rollover occurs when the lateral component of the acceleration exceeds a certain level. This level is called the rollover threshold.

Rollover threshold is usually determined by performing a test under static conditions - a "tilt table" test. The schematic layout of the tilt table experiment is shown in figure 6.7. The vehicle is positioned on a tilt table platform and is subjected to a gradually increase roll angle. The roll rate of the tilt table is very slow to avoid dynamic effects. As the test progresses, axles start to lift off until a point is reached when the vehicle goes unstable and keeps rolling without an increase in the angle of the tilt table. This point is registered as the rollover threshold with a simulated lateral acceleration that is the appropriate component of the earth gravity. (Hugh McGee et al., USDOT 1993)


Figure 6.7: Schematic Layout of a Tilt Table Experiment (from Hugh McGhee et al.)

The rollover threshold for a typical passenger car is 1.2 (H. W. McGee, "Synthesis of Large Tuck Safetv Research"), which is substantially higher than rollover thresholds for loaded truck configurations (Ervin et al.,) Figure 6.8.


Figure 6.8: Rollover Threshold Values for Various Example Vehicles

Ervin, Nisonger, MacAdam and Fancher (Influence of Size and Weight Variables on_Stability and Control Properties of Heavy Trucks) have shown that


Figure 6.9: Rollover Accident Data vs. Calculated Rollover Threshold Value
vehicles with low rollover thresholds are much more likely to be involved in rollover accidents. Figure 6.9 (above) shows a graph of this relationship.

Harwood and Mason (Ramp/Mainline Speed Relationships and Design Considerations) concluded that truck rollovers and run-off-the-road accidents are attributed to vehicles traveling faster than design speed rather than to a flaw in the AASHTO design Policy. Harwood et al. evaluated AASHTO horizortal curve design criteria and found that although it is adequate for passenger cars and trucks it provides a very narrow margin of safety to trucks as compared with that provided to passenger cars. Harwood and Mason developed a table which summarizes vehicle speeds at impending skid and rollover based on the following conditions:

- A minimum-radius curve with a maximum superelevation rate of $.08 \mathrm{ft} / \mathrm{ft}$ as per AASHTO criteria.
- Wet pavement friction levels equivalent to AASHTO stopping sight distance policy.
- A passenger car rollover threshold of 1.2.
- A truck rollover threshold of 0.3 (represents worst-case currently on the road).

| Deskgn speed (mph) | $\underset{e}{\text { Maximum }}$ | Passenger car speed (mph) |  | Truck speed (mph) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ai impending skid (wer) | At impending rollover | At empending skid (wet) | At impending rollover |
| 20 | 0.08 | 32.5 | 45.3 | 26.8 | 24.7 |
| 30 | 0.08 | 47.1 | 69.6 | 39.0 | 37.9 |
| 40 | 0.08 | 61.8 | 94.8 | 51.3 | 51.6 |
| 50 | 0.08 | 76.8 | 121.1 | 63.9 | 66.0 |
| 60 | 0.08 | 85.2 | 152.2 | 79.3 | 82.9 |
| 70 | 0.08 | 118.0 | 181.5 | 98.5 | 104.3 |

Table 6.9: Vehicle Speed at Impending Skid and Rollover

The fact that trucks are traveling faster than is safe can often be attributed to the violation of the driver expectancy expressed in inadequate warning to the drivers as is discussed earlier in the report.

### 6.6 ACCELERATION ABILITY OF TRUCKS vs. AASHTO DESIGN CRITERIA FOR ENTRANCE TERMINALS

According to the AASHTO design criteria, the geometrics of the ramp proper should be such that motorists may attain a speed approximately equal to the average running speed of the freeway less 5 mph by the time they reach the point where the left edge of the ramp joins the traveled way of the freeway. The distance required for acceleration in advance of this point is govemed by the speed differential between the average running speed on the entrance curve on the ramp and the running speed of the freeway. Figure 6.10 (1990 GB) shows the minimum lengths for gap acceptance and Figure 6.11 (1990 GB) shows the minimum length of acceleration distances for entrance temminals.


MOTES:
I. Lo IS The REOUIRED ACCELEARTION LENSTH AS SHORN IM TAECE $X-4$ OA $X-5$.
2. NOINT (D) CONTROLS SAFE SPEED ON TRE RMP. LO SHOLD MOT STAFT EACX ON THE CLRVATLRE OF THE RANP UNLESS THE REDIUS EOUMLS 1000 OR MORE.
3. LG IS REOUIRED EAP RCCEPTAHEE LENGTK LG SHOLLD BE A MINsINN OF S00' TO 500' OEPEMOING ON THE MOSE HIOTR.
4. THE VALLE OF LO OR LA GHICHEYER PRODUCES THE GREATEST OISTAHEE DCONTRFAM FROT RHERE THE NOSE -IDTH EOUALS TRO FEET. IS SUCOESTED FOR USE IN THE DESIGN OF THE RANP ENTRAMEE.

Figure 6.10: Minimum Length for Gap Acceptance


Figure 6.11: Minimum Acceleration Lengths for Entrance Terminals

This standard has not changed in 30 years. Although the gross combination weight of commercial vehicles has been going up steadily over the same period of time, there is a consistent trend toward a decrease in weight-to-power ratios attributed to the design and manufacturing of yet more powerful engines. Figure 6.12 ( 1990 GB ) shows the trend in weight-power ratios from 1949 to 1985 based on average data for all types of vehicles.


Figure 6.12: Trend in Weight-Power Ratios 1949 - 1985 (Average All Vehicles)

Slower acceleration of trucks as compared with passenger cars and the need for longer space during the gap acceptance process makes merging and lane changing for trucks more difficult. Accident statistics presented earlier in this report show that a large portion of truck accidents at interchanges take place in the merge turbulence zone which can be related to a trucks' inability to gain speed on the acceleration lanes designed to meet AASHTO criteria. A representative truck of the modem commercial vehicle fleet will a have a weight-power ratio of $200 \mathrm{LB} / \mathrm{hp}$. A performance curve for such a vehicle is shown in Figure 6.13 (1985 Highway Capacity Manual). In order to reach a running speed of 53 mph , which is needed to merge with through traffic on freeways with 70 mph design speed and $1 \%$ grade, approximately 2 miles of acceleration length is required. Clearly, constructing such a facility may not be economically feasible. The question then becomes - what can be done to address this important safety issue? We should probably concentrate on providing a desirable range of design values when trucks are present along with better signing and a more predictable roadway environment.


Figure 6.13: Performance Curves for a Standard Truck (200 lbs / hp)

### 6.7 CONCLUSIONS OF CRITICAL EXAMINATION OF AASHTO STANDARDS FROM THE STANDPOINT OF TRUCK OPERATIONS AT INTERCHANGES

- There is a definite trend toward longer and heavier trucks, yet it is important to realize that innovations in engine design, brakes, suspension, hitches and truck aerodynamic characteristics made trucks safer and more efficient to operate.
- The development of longer combination vehicles provide increased productivity while reducing exposure. At the same time these vehicles impose greater and greater demands on the roadway infrastructure. Comprehensive truck size and weight study currently in progress provides a forum for this important question at the national level.
- Dimensions of the design vehicles larger than WB-50 and their offtracking/swept width requirements are well defined in the latest edition of the AASHTO Geometric Design Policy. What is not well defined however is who will carry the financial burden of accommodating these vehicles on the roads.
- The new NHTSA regulations mandated maximum braking distances and ABS for all new heavy and medium trucks and buses beginning in March of 1997. These regulations will bring braking ability of commercial vehicles in line with AASHTO standards. While these requirements will go a long way in improving traffic safety it is important to realize that they apply only to the new trucks and buses and will not require retrofitting of the existing fleet, which means that safety improvement is expected to take place gradually and over time.
- AASHTO policy on the design of horizontal curves provides a very narrow margin of safety for the operation of commercial vehicles. It is especially true for the lower range of design speeds. To improve truck safety on curves, highway designers should become more sensitive to truck presence and provide "desirablen range of design values. This approach will increase the margin of
safety available for the operation of commercial vehicles and reduce the probability of rollovers.
- Current AASHTO standards for acceleration at entrance terminals are well beyond the capabilities of loaded commercial vehicles. This disparity between vehicle capability and AASHTO standards is reflected in the high number of accidents in the merge turbulence zone. Yet, constructing facilities to accommodate acceleration abilities of trucks may not be economically feasible. The strategies to address this important issue include: providing desirable range of design values, better signing and predictable roadway environment and driver education.
- It would be highly beneficial for highway engineers to have certain basic knowledge of vehicle design and truck operation to gain greater appreciation of the problem.


## APPENDIX

1. TRUCK DRIVER SURVEY INFORMATION
2. IMPLEMENTATION OF STUDY FINDINGS IN COLORADO

## STATISTICAL SUMMARY


$\square$


| 2.16 | 0.01 |
| :--- | :--- |
| 3.69 | 1.08 |
| 3.18 | 1.33 |
| 2.39 | 1.21 |
| 2.28 | 1.10 |
| 2.54 | 1.28 |
| 2.65 | 1.10 |
| 2.22 | 0.03 |
| 1.78 | 0.69 |
| 1.81 | 0.80 |
| 3.24 | 1.34 |


2.540 .68 $0.68 \quad 0.30$

Trucker's Survey Results, $\quad 1=$ Bad $\quad 5=$ Good

## TRUCK DRIVER SURVEY

The Western Highway Institute is currently working with the Colorado Department of Transportation to gather information on which ramps and interchanges create problems for the professional truck driver. The information gathered will be used to: 1) identify trouble areas in Colorado; 2) develop strategies to assist truck drivers in these high accident areas; and 3) enable highway engineers to design ramps and interchanges to more safely address the needs of commercial vehicle operators and the traveling public.

Please complete the following information. All information will remain confidential. The rood of this project is to enhance the safety of commercial vehicle operators and their equipment.

1. Check the type of trip you typically run.

| a 30 | Interstate - Long-haul (over 500 miles) |
| :---: | :---: |
| b. $\quad 27$ | Intrastate |
| c. $\quad 41$ | Local Pick Up and Delivery |
| d. $\quad 1$ | Small Package (under 50 pounds) |
| e. $\quad 3$ | Other; please specify__Peddle; Pedal; Shuttle |
| 1 | No Response |
| 103 | Total |

(note: more than 84 responses because some drivers indicated more than I type of trip)
2. Indicate percentage of loads that are:
a

b. $100 \%$ Truckload
$100 \%$ Less-than-truckload

| \% Truckload: \# of Responses | \% Truckload | \# of Responses |  |
| :---: | :---: | :---: | :---: |
| 0 | 9 | 80 | 3 |
| 1 | 1 | 85 | 1 |
| 5 | 2 | 90 | 3 |
| 10 | 1 | 95 | 4 |
| 20 | 4 | 98 | 1 |
| 25 | 1 | 100 | 26 |
| 30 | 1 | No Response | 1 |
| 35 | 1 | Total |  |
| 45 | 1 |  | 84 |
| 50 | 9 | (note: if the driver only checked the blank |  |
| 60 | 2 | it was considered $100 \%$ ) |  |
| 65 | 1 |  |  |
| 70 | 6 |  |  |
| 75 | 6 |  |  |

3. Mark the type of commodities primarily hauled:
a. 34 General Freight
b__Il3_Specialized Freight _15 Agricultural products

2 Heavy machinery $39 \quad$ Refrigerated products 4 Liquid/Tank 7 Building materials I2 Household materials 0 Motor vehicles 20 Hazardous materials (please specify type)

Bleach
_ 9 Other: (please specify)__Food/Candy Not Specified
$-5$

Groceries
General Hazardous
0 _ Not Specifie
$1 \overline{47}$ Tota
Bakery Products Corrosive
Groceries
Flammable
Frozen, Fresh, Dry
US Mail
US Mail
Not Specified
Matches, Antifreeze
Not Specified
US Mail Gas \& Diesel
Restaurant Supplies Not Specified
Not Specified
All except explosive
All types
Bread
Not Specified
Cleaners
Paint/Corrosives
Soap, Cleaners
Not Specified
Corrosive,
Flammable
Dish Chemicals
4. Check the category below which most appropriately describes your professional status:

| a. $\quad 84$ | Company driver |
| :---: | :---: |
| $b$. | Owner - operator |
| c. | Leased employee |
| 84 | Total |

5. a. Check years of driving experience:

6. Indicate sex and age:
Male

| a. | 1 |
| :---: | :---: |
| b. | 25 |
| c or less | 26 to 29 |
| c | 36 |$\quad 30$ to 39


| d. | 25 |
| :--- | :--- |
| e. | 40 to 49 |
| f | 10 |
|  | So to 59 |
|  | 60 or older |

Female

| 1 | $30-39$ |
| :--- | :--- |
| 3 | $40-49$ |

(note: if no response to sex but response to age, assumed male)
7. Indicate the type of vehicle(s) you typically drive and approximate weight hauled (e.g., five-axle tractor trailer at 80,000 pounds, Rocky Mountain doubles at 94,000 pounds, triples at 110,000 pounds, etc.).
$28^{\prime}$ Tractor Trailer ..... 1
5 Axle Reefer Van 80,000 ..... 4
3 Axle tractor-trailer 40,000 ..... 4
5 Axle Tractor Trailer ..... 2
5 Axle Tractor Trailer 80,000 ..... 20
Doubler@80,000/Triples@110,000 ..... 3
Twin Trailers 70,000-80,000 ..... I
5 Axle Tractor Trailer 65,000 ..... 2
80,000 ..... 1
Doubles ..... I
3 Axde 30,000 ..... I
3 Axle 15,000 ..... 2
3 Axle ..... 1
Doubles 80,000 ..... 1
5 Axle 35,000-43,000 ..... 1
5 Axle Van 65,000 ..... 1
Twin Trailers 75,000 ..... 2
Twin Trailers 40,000 ..... 1
3 Axle Tractor Trailer 14,000 ..... I
Tandem axle straight truck 15,000 ..... 1
80,000-94,000 ..... I
4 Axle 65,000 ..... 3
6 to 10 Axle to 200,000 ..... 1
5 Axle 70,000 ..... 2
5 Axle tractor trailer 60-70,000 ..... 2
Doubles 70,000 ..... 2
Triples and Doubles ..... 2
3 Axle 20,000 ..... 1
5 Axle ..... 2
Tandem Bobtail 40,000 ..... I

```
5 axle tt 80,000/R.M. doubles 94,000/triples 110,000 2
5 \text { axle van I}
5 axle var 70,000-75,000
5 axle 80,000/3 axle 54,000/2 axle 30,000,
5 axle 79,000 2
5 axie van 50,000 3
3 axde straight 35,000/3 axle trailer 35,000 I
Doubles and Triples 60,000-110,000 1
4 \text { axle TT 45,000}
3 axje 10-18,000
27'-52' Vans-Straight Trucks 5,000-40,000
No Response
```

8. Rank up to FIVE numbered interchanges shown on the Colorado or Denver area map with I being the most difficult to travel.

Indicate interchanges in order of difficulty to travel safely

| Interchange <br> Number <br> (list up to <br> five inter- <br> changes) | $\underline{1}$ | $\underline{2}$ | $\underline{3}$ | $\underline{4}$ | $\underline{5}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Please circle <br> if difficult <br> to: | ENTER | ENTER | ENTER | ENTER | ENTER |


| I/C \# | No. of Resp. | I/C | \# No. of Resp |
| :--- | :--- | :--- | :--- | :--- |
| 68 | 5 | 99 | 1 |
| 70 | 1 | 100 | 28 |
| 72 | 1 | 101 | 16 |
| 76 | 12 | 112 | 1 |
| 80 | 2 | 180 | 1 |
| 81 | 1 | 182 | 1 |
| 85 | 1 | 190 | 1 |
| 89 | 26 | 192 | 1 |
| 90 | 2 | 196 | 3 |
| 91 | 4 | $196 A$ | 4 |
| 92 | 4 | 197 | 14 |
| 93 | 4 | 198 | 1 |
| 95 | 1 | 199 | 2 |
| 96 | 1 | 202 | 2 |
| 97 | 4 | 203 | 1 |

I/C \# No. of Resp. I/C \# 2055295 2064307 208303
$209 \quad 316$

| 211 | 3 | 323 | 7 |
| :--- | :--- | :--- | :--- |


| $238 A$ | 327 | 1 |
| :--- | :--- | :--- |


| 241 | 3 | 328 | 17 |
| :--- | :--- | :--- | :--- |

245A $1 \quad$ No Resp. 12

245B 2
$246 \quad 4$
2472
2487
252A 4
2537
293 |

# Attendance - Focus Group Meeting 

 October 26, 1994| Name | Organization |
| :--- | :--- |
| Howard Adams | King Soopers |
| James Blair | Westway Express |
| Lia Duda | Westway Express |
| Val Eagal | Colorado Petroleam |
| Chuck Fingn | Westway Express |
| Ray Gassaway | USDOT/FHWA/OMC |
| James L. Harris | Colorado Petroleam |
| Norm Kaus | United Parcel Service |
| Don Pfertsh | United Parcel Service |
| John Pitzer | Colorado State Patrol |
| Al Ream | King Soopers |
| Steve Reeves | Klein Trucking |

## Project team:

| Wael Awad | University of Colorado at Denver |
| :--- | :--- |
| Melissa Coleman | Western Highway Institute |
| Lyme Dearasaugh | University of Colorado at Denver |
| Greg Fulton | Colorado Department of Transportation |
| Bruce Janson | University of Colorado at Denver |
| Debb Johnson | Western Highway Institute |
| Donalee Kolva | Colorado Motor Cariers Association |
| Jake Kononov | Colorado Department of Transportation |

# Comments from Focus Group Meeting <br> October 26, 1994 

## Comments on specific interchanges:

1-25 \& SH 34
Acceleration distance not adequate for trucks in wreave area. Yes ( $60 \mathrm{ft}<$ mean=169 ft)
Short weave area. ..... Yes ( $500 \mathrm{ft}<$ mean=1117 ft)
Avoidance maneuvers
Speeds too fast
Poor sight distance in weave areas.Tight radius loop ramps.Yes ( $R=151 \mathrm{ft}<$ mean=157 ft)Downward grade
Truck posted speeds need to be about 10 mph lower on loop ramps
Carrier base (familiar with interchange)
Fewer trucks headed north than south
Poor signage southbound
Loading conditions may be a problem
High track exposare. ..... No (Truck Vol. $=3214<$ mean $=4005$ )
Superelevation transition
$1-70 \&$ Ouebec
Too much traffic. ..... No $(A A D T=93300<$ Mean $=100540)$
End of NE ramp, accel. \& decel lane too short
End of NE ramp, lane configuration confusing
Insufficient advance waming \& direction
Lergest Denver truck stop \& terminal. Not largest (Truck Vol $=4329>$ mean=4005)
Closeness of NB signal on Quebee \& Sand Creek ..... Yes
Familiarity with interchange
Visibility at end of NE ramp is poor
Major truck stop. ..... Yes (Truck Vol $=4329>$ mean $=4005$ )
1-70 \& 1-225
Now wider merge areas
Confusing signing
Congestion.

$$
\text { No ( AADT }=74000<\text { mean }=100540 \text { ) }
$$

No advance siguing
Difficult roxd surface - on I-70 EB between SWI \& SEI
Construction has improved interchange
Many major streets in short proximity to each other
Visibility is a problem - SEl to EB I-70
I-70 \& Pecos
EB I-70 steep off-ramp - short - downgrade
I-70 too low below I-70 rising crest
Bridge blocking rear view sight distance -approaching SEI
Poor sight distance from SE1
Signs also in way
Mousetrap backup
Accidents in AM Peak
Exit to 48th - drivers don't expect stop light
Poor curvature on ramp to 48th. Yes ( 107 Degree or $\mathrm{R}=54 \mathrm{ft}$ < mean=157 ft )
$1-25 \&$ Santa Fe
Merging too early - NB Santa Fe to NB I-25. Yes
Sudden grade change
Superelevation transition
Poor rear visibility
Possibly redirect trucks to other on-ramp \& not mix with HOV vehicle
Drivers don't realize SE-1 continues as a contimous lane on I-25 SB
I-25 \& Bijou
Strong curves for high speeds. No (8 Degree or $\mathrm{R}=716 \mathrm{ft}>$ mean=157 ft)
Lane drop in NB direction on 1-25. ..... Yes
High traffic volumes. No ( AADT $=69900<$ mean $=100540$ )
Short ramps. ..... Yes ( Ramp Length=450 ft < mean=733 ft)
Need to relocate exit ramps past curve
1-70 \& Ward
Truck ztop. No (Truck Vol $=3190<$ mean $=4005$ )
Sharp transition at merge point at ramp $D$.and $R=286 \mathrm{ft}>\operatorname{mean}=157 \mathrm{ft}$ )
Curvature of $\mathbf{C}$ is deceptively sharp. Yes (Ramp Length $=600 \mathrm{ft}, \mathrm{R}=130 \mathrm{ft}$ )
Steep grade on ramp D
Short decel lane for ramp $\mathbf{C}$. ..... No ( $1680 \mathrm{ft}>\operatorname{mean}=1117 \mathrm{ft})$
Others
I-70 \& Glenwood Springs Index $=7$
I-76 \& SH 85 (reverse superelevation - 76 WB onto 85)
I-76 \& I-270Index $=22$, Frequency $=6$, Exp. $=0.002$Index $=10$
I-25 \& 1st Ave (in Pueblo) Index $=1$

## Summary

Stripe maintenance in high volume areas
Lack of advanced signage
Separate signs for truck speeds on ramps - Truck speed signs
Lengthen acceleration lanes
Clear overhead signs
Brighter/Flashing signs
Picture signs (configuration of interchinge)
Redirecting trucks to easiter ramps
Educate car driver (newspaperiVV spot)
Warnings for high volime tinck aneas (signs)
Examilie good interctianges
Grooving road \& gore areas to alert drivers
Rumbie stripes for slowing
Curve trinstions
Visibility \& Communcation - big factors

| intreng Num | Cross Road | Accidents 199319921991 Tota |  |  |  | Total Total Acc. Acc. Acc. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rounts $1-25$ |  |  |  |  |  |  |  |  |  |
| 1 | Starkville interchange | 1 |  |  | 1 |  | 1 |  | 1 |
| 2 | Country Club Dr., Trinidad | 1 |  |  | 1 | 1 |  | 1 | 5 |
| 3 | SH 160, Trinidad | 1 | 1 |  | 2 |  | 2 |  | 2 |
| 4 | SH 12, Titided |  |  |  | 0 |  |  |  | 0 |
| 5 | Commerclal St, Trinided |  |  |  | 0 |  |  |  | 0 |
| 6 | SH:299, Coddard St. Trinided |  |  |  | 0 |  |  |  | 0 |
| 7 | Hochne Rd. |  |  | 1 | 1 |  | 1 |  | 1 |
| 8 | Ludiow |  |  |  | 0 |  |  |  | 0 |
| - | SH 25 Aquilar Spur |  |  |  | 0 |  |  |  | 0 |
| 10 | Rouse Rd. |  |  |  | 0 |  |  |  | 0 |
| 11 | SH 25 Wakenburg Bus. Rt S. |  | 1 |  | 1 |  | 1 |  | 1 |
| 12 | EH 10 and SH 160, e/o Walsenburg | 1 |  |  | 1 |  | 1 |  | 1 |
| 13 | SH 25 Walsenbung Bus. Rt N. |  |  |  | 0 |  |  |  | 0 |
| 14 | Butte Rid. |  |  | 1 | 1 |  | 1 |  | 1 |
| 18 | Herfino Interchange, Rd E (CO Rd. 104) |  |  |  | 0 |  |  |  | 0 |
| 16 | Apache interchange |  |  |  | 0 |  |  |  | 0 |
| 17 | Grenerso Rd. |  |  |  | 0 |  |  |  | 0 |
| 18 | SH 165 |  |  |  | 0 |  |  |  | 0 |
| 18 | Bumit Mill Rd. |  |  |  | 0 |  |  |  | 0 |
| 20 | Stem Beach |  |  |  | 0 |  |  |  | 0 |
| 21 | SH 45 |  |  |  | 0 |  |  |  | 0 |
| 22 | Access Rd. W. (Hintols Ave.) |  |  |  | 0 |  |  |  | 0 |
| 23 | Indims Ave. |  | 1 |  | 1 |  | 1 |  | 1 |
| 24 | Central Ave. |  |  |  | 0 |  |  |  | 0 |
| 28 | Ediorado SL. |  |  |  | 0 |  |  |  | 0 |
| 28 | liex St. | 1 | 1 | 1 | 3 | 4 | 2 | 1 | 7 |
| 27 | 1st St. | 1 |  |  | 1 |  | 1 |  | 1 |
| 28 | Sth EL | 1 |  |  | 1 |  | 1 |  | 1 |
| 28 | 13th SL | 1 | 1 |  | 2 | 2 | 1 | 1 | 6 |
| 30 | SH 50, 20:H St. | 1 | 1 |  | 2 | 1 | 1 | 1 | 6 |
| 21 | 29th St |  | 1 |  | 1 |  |  |  | 0 |
| 22 | SH 47 and SH 50 | 1 | 5 | 2 | 8 | 3 | 8 | 2 | 16 |
| 33 | Eaxieridge Ehvol. | 1 |  |  | 1 |  | 1 |  | 1 |
| 84 | Eden Ifterchange |  |  |  | 0 |  |  |  | 0 |
| 26 | Erequion |  |  |  | 0 |  |  |  | 0 |
| 38 | EH 85, Fountain |  |  |  | 0 |  |  |  | 0 |
| 37 | SH16 |  |  |  | 0 |  |  |  | 0 |
| 28 | SH 03 |  |  | 1 | 1 |  | 1 |  | 1 |
| 39 | SH28 | 2 | 3 | 1 | 6 | 2 | 5 | 1 | 10 |
| 10 | SH 24 Bypass |  |  |  | 0 |  |  |  | 0 |
| 41 | SH 25 and SH 85, Nevada Ave. | 2 | 1 |  | 3 | 1 | 2 | 1 | 7 |
| 42 | Tejon St. |  |  |  | 0 |  |  |  | 0 |
| 48 | SH 24, Cimarron SL | 3 |  |  | 3 | 1 | 2 | 1 | 7 |
| 4 | Bfou St. | 3 | 5 | 1 | 9 | 3 | 7 | 2 | 17 |
| 46 | Uintah St. | 1 | 1 |  | 2 |  | 2 |  | 2 |
| 48 F | Fontanero St. | 2 | 1 |  | 3 | 2 | 1 | 2 | 11 |
| 47 S | SH 38, Fulmore St. | 5 | 4 | 1 | 10 | 4 | 7 | 3 | 22 |


| Intrchg |  |  | $\begin{aligned} & \text { Accid } \\ & 1992 \end{aligned}$ |  |  |  | Total Fatal |  | \# Acc. wflnj. | \# Acc. wiFata | al Index |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Num | Crass Road |  |  | 2 | 5 | 1 |  | 4 | 1 |  | 9 |
| 48 | S. Ramps, Garden of Gods Rd. |  | 3 | 2 | 0 |  |  |  |  |  | 0 |
| 49 | N. Ramps, Garden of Gods Rd. |  | 1 | 2 | 3 | 2 |  | 1 | 2 |  | 11 |
| 50 | Rocknimmom Interchange | 2 |  |  | 2 | 1 |  | 1 | 1 |  | 6 |
| 51 | SH 25 Colo Spgs Bus. Rt., Nevada Ave. | 2 |  | 3 | 5 | 1 |  | 4 | 1 |  | 9 |
| 52 | Woodmen Rd. | 2 | 1 | 4 | 7 | 5 |  | 3 | 4 |  | 23 |
| 63 | SH 83 Spur and South Gate Rd. | 2 | 1 | 4 | 0 |  |  |  |  |  | 0 |
| 54 | Briargate | 1 |  |  | 1 |  |  | 1 |  |  | 1 |
| 55 | North Gate Rd. | 1 | 1 | 1 | 2 | 3 |  |  | 2 |  | 10 |
| 56 | Baptist Rd. |  | 1 | 1 | 0 | 3 |  |  |  |  | 0 |
| 57 | SH 105, Monument |  | 1 |  | 0 |  |  | 1 |  |  | 1 |
| 58 | Palmer Divide Rd. |  | 1 |  | 0 |  |  |  |  |  | 0 |
| 59 | SH 18 |  |  |  | 0 |  |  |  |  |  | 0 |
| 60 | Lark Spur |  | 1 | 1 | 3 | 2 |  | 2 | 1 |  | 7 |
| 61 | South Castle Rock | 1 | 1 | 1 | 4 | 2 |  | 4 |  |  | 4 |
| 62 | North Castle Rock | 2 | 1 | 1 | 4 0 |  |  |  |  |  | 0 |
| 63 | SH 85, no Castle Rock |  |  |  | 0 |  |  |  |  |  | 0 |
| 64 | Meadows Pwky |  | 2 | 1 | 3 | 2 |  | 2 | 1 |  | 7 |
| 65 | Happy Canyon Rd (CO Rd. HC1) |  | 2 | 1 | 2 | 2 |  | 1 | 1 |  | 6 |
| 66 | Castle Pines (CO Rd. BH1) | 1 | 1 | 1 | 2 | 2 |  | 2 |  |  | 2 |
| 67 | Lincoln Ave. (CO Rd, 8) | 1 | 1 |  | 1 |  |  | 1 |  |  | 1 |
| 68 | SH 470 |  |  | 1 | 1 | 1 |  |  | 1 |  | 5 |
| 69 | County 1 ine Rd. |  |  |  | 0 | 1 |  |  |  |  | 0 |
| 70 | S. Ramp Dry Creek Rd. (ramp off) |  |  | 1 | 1 |  |  | 1 |  |  | 1 |
| 71 | N Famp Dry Creek Rd. (ramp on) | 4 | 1 | 1 | 6 | 1 |  | 5 | 1 |  | 10 |
| 72 | SH 88, Arapahoe Rd. | 4 | 1 | 1 | 0 |  |  |  |  |  | 0 |
| 73 | S. Ramps Orchard Rd. (ramp off) |  | 1 | 1 | 2 | 1 |  | 1 | 1 |  | 6 |
| 74 | N. Rames, Orchard Rd. (ramp Off) |  | 3 | 2 | 6 | 1 |  | 5 | 1 |  | 10 |
| 75 | SH 88, Belleview Ave. | 1 | 3 | 4 | 8 | 4 |  | 6 | 3 |  | 21 |
| 76 | 1-225 Interchange | 3 | 3 | 2 | 7 | 4 |  | 5 | 2 |  | 15 |
| 77 | S. Ramp SH 30'SH 285, Hampden Ave. (ramp off | 2 | 3 | 2 | 7 | 4 |  | 5 | 2 |  | 0 |
| 78 | N. Ramp SH 301SH 285, Hampden Ave. (ramp on) |  |  |  | 9 | 2 |  | 7 | 2 |  | 17 |
| 79 | Yale Ave. | 8 | 1 | 2 | 9 6 | 2 |  | 4 | 2 |  | 14 |
| 80 | Evans Ave. | 4 |  | 2 | 8 | 1 |  | 8 | 1 |  | 13 |
| 81 | SH 2, Colorado Blva. | 3 | 1 | 5 | 9 5 | 1 |  | 5 | 1 |  | 5 |
| 82 | Undversty Btivd. |  | 2 | 3 | 5 |  |  | 5 |  |  | 0 |
| 83 | Downing St. |  |  |  | 0 |  |  |  |  |  | 0 |
| 84 | Emerson St. |  |  | 3 | 6 |  |  | 6 |  |  | 6 |
| 85 | Washington St. | 2 | 3 | 3 | 6 | 1 |  | 5 | 1 |  | 10 |
| 86 | Broadway | 3 | 3 |  | 10 | 2 | 1 | 8 | 1 | 1 | 125 |
| 87 | SH 86, Santa Fe Dr. | 1 | 5 | 4 | 10 | 3 | 1 | 6 | 3 |  | 21 |
| 88 | SH 26, Alemeda Ave. | 1 | 5 | 3 | 9 | 3 |  | 5 | 1 |  | 10 |
| 89 | SH 6, 6th Ave. | 5 | 1 |  | 8 | 4 |  | 5 | 3 |  | 20 |
| 90 | 8 8th Ave. |  | 3 | 5 | 8 | 4 |  | 7 | 1 |  | 12 |
| 91 | SH 40, Colfax Ave. | 1 | 2 | 5 | 8 | 1 |  |  |  |  | 0 |
| 92 | Auraria Pkwy. |  |  |  | 0 |  |  |  |  |  | 0 |
| 93 | 17th Ave and 19th Ave. Ramps |  |  |  | 14 |  |  | 11 | 3 |  | 26 |
| 94 | 23rd St. | 8 | 4 | 2 | 14 | 4 |  | 10 | 2 |  | 132 |
| 95 | Speer Blvd. | 4 | 6 | 3 | 13 | 4 | 1 | 8 | 3 |  | 123 |
| 96 | 20th St. | 4 | 2 | 5 | 29 | 8 |  | 25 | 4 |  | 45 |
| 97 | Fox/38th Ave. | 11 | 9 | 8 | 29 | - 10 |  | 18 | 7 |  | 53 |
| 98 | 1-70 interctange | 9 | 5 | 11 | 25 | 10 |  | 9 | 6 |  | 39 |
| 99 | SH 53, 58th Ave. | 7 | 7 | 1 | 15 | 7 |  | 9 | 6 |  | 39 |


| Intrchg |  | 1993 | Accid |  |  |  | Total \# Acc. Fatal w/PDO | \# Acc. w/inj. | \# Acc. w/Fatal index |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Num | Cross Road | 1993 | 1 |  | 6 | 2 | 5 | 1 | 10 |
| 100 | -76 interchange | 2 | 5 | 3 | 10 | 6 | 5 | 5 | 30 |
| 101 | SH 36 | 2 |  | 1 | 1 |  | 1 |  | 1 |
| 102 | 84th Ave. |  | 1 | 3 | 4 | 5 | 2 | 2 | 12 |
| 103 | Thomton Pkwy. | 5 | 3 | 1 | 9 | 2 | 7 | 2 | 17 |
| 104 | 104th Ave. | 1 | 3 | 2 | 6 | 3 | 5 | 1 | 10 |
| 105 | SH 128, 120th Ave | 1 | 3 | 2 | 6 | 1 | 3 | 1 | 8 |
| 106 | SH 7 ( 7 (CORd 8) (Erie) | 1 | 1 | 1 | 2 | 6 | 1 | 1 | 6 |
| 107 | Rd. E. and W. (CO Rd. 8) (Erie) | 1 | 2 | 1 | 3 | 3 | 1 | 2 | 11 |
| 108 | SH 52 | 1 | 2 | 1 | 3 | 3 | 1 | 2 | 11 |
| 109 | SH 119 | 1 | 2 |  | 2 |  | 2 |  | 2 |
| 110 | SH 68 |  | 2 |  | 0 |  |  |  | 0 |
| 111 | Mead interchange | 1 |  |  | 1 |  | 1 |  | 1 |
| 112 | SH 56 | 1 |  |  | 0 |  |  |  | 0 |
| 143 | SH 60 |  |  |  | 1 |  | 1 |  | 1 |
| 114 | SH 402 | 4 | 3 | 4 | 11 | 8 | 6 | 6 | 31 |
| 115 | SH 34 |  | 3 | 4 | 0 |  |  |  | 0 |
| 116 | Rd. E and W (CO Rd. 26) (Aipport Dr.) | 1 |  |  | 1 |  | 1 |  | 1 |
| 117 | SH 382 | 1 | 1 | 1 | 3 |  | 3 |  | 3 |
| 118 | SH 88 | 1 | 1 | 1 | 1 |  | 1 |  | 1 |
| 119 | Prospect Interchange | 3 | 3 | 2 | 8 | 1 | 7 | 1 | 12 |
| 120 | SH 14 | 3 | 3 | 2 | 0 | 1 |  |  | 0 |
| 121 | CORd. 50 |  | 1 |  | 1 |  | 1 |  | 1 |
| 122 | SH 1 |  | 1 |  | 0 |  |  |  | 0 |
| 123 | Owl Canyon |  |  | 1 | 1 | 2 |  | 1 | 5 |
| 124 | Carm Interchange |  |  | 1 | 1 | 2 |  |  |  |
| Route $\rightarrow$ | $1-70$ |  |  |  | 1 | 1 |  | 1 | 5 |
| 125 | SH 6, to Mack | 1 |  | 1 | 1 | 1 | 1 |  | 1 |
| 126 | SH 139, to Loma |  |  | 1 | 0 |  |  |  | 0 |
| 127 | SH 340, Fruita |  |  |  | 0 |  |  |  | 0 |
| 128 | SH 6 and W SH 70 Grand Jet Bus. RL |  |  |  | 0 |  |  |  | 0 |
| 129 | Rd. N. and S. (CO Rd. 24) |  | 1 |  | 1 |  | 1 |  | 1 |
| 130 | Horizon Dr. | 3 |  |  | 3 | 3 |  | 3 | 15 |
| 131 | E EH 70 Grand Jat Bus. RL. | 3 |  |  | 0 |  |  |  | 0 |
| 132 | Palisade interchange |  |  |  | 0 |  |  |  | 0 |
| 133 | SH 6, e\% Palisade |  |  |  | 0 |  |  |  | 0 |
| 134 | Cameo Interchange |  |  |  | 0 |  |  |  | 0 |
| 135 | SH 65 Interchange |  |  |  | 0 |  |  |  | 0 |
| 136 | Debeque Interchange |  |  |  | 0 |  |  |  | 0 |
| 137 | Parachute interchange |  |  |  | 0 |  |  |  | 0 |
| 138 | Rurison Interchange |  |  |  | 0 |  |  |  | 0 |
| 139 | SH 6, who Rifle | 1 | 1 |  | 2 |  | 2 |  | 2 |
| 140 | SH 18 | 1 | 1 |  | 0 |  |  |  | 0 |
| 141 | SH 70 Sith Spur |  |  |  | 0 |  |  |  | 0 |
| 142 | Rd. N.S. (CO Rd. 240), to New Castle |  |  |  | 0 |  |  |  | 0 |
| 143 | SH 6, Canyon Creek |  |  |  | 0 |  |  | 1 | 5 |
| 144 | West Glenwood | 1 |  | 1 | 3 | 1 | 2 | 1 | 7 |
| 145 | SH 82 | 1 |  | 2 | 3 |  |  |  | 0 |
| 146 | No Name |  |  |  | 0 |  |  |  | 0 |
| 147 | Deadhorse Creek, Hanging Lake Park |  |  |  | 0 |  |  |  | 0 |
| 148 | W. Dotsero |  |  |  | 0 |  |  |  | 0 |
| 149 | E. Dotsero |  |  |  | 0 |  |  |  | 0 |
| 150 | SH 6, Gypsum |  |  |  | 0 |  |  |  |  |



| IntrchgNum | Cross Road | Accidents 199319924991 |  |  |  |  | Total Fatal |  | \# Acc. w/lnj. | \# Acc. w/Fatal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1993 | 1992 | 18 | 13 | 3 | 1 | 9 | 3 | 1 | 36 |
| 202 | SH 2, Colorado Blvd. | 5 | 1 | 1 | 4 | 1 |  | 3 | 1 |  | 8 |
| 203 | Dathlia St. | 2 | 1 | 1 | 2 |  |  | 2 |  |  | 2 |
| 204 | Monaco St. | 12 | 9 | 3 | 24 | 5 |  | 21 | 3 |  | 36 |
| 205 | SH 35, Quetec St. | 12 3 | 5 | 3 | 8 | 1 |  | 7 | 1 |  | 12 |
| 206 | SH 270 | 9 | 4 | 3 | 16 | 14 |  | 11 | 5 |  | 36 |
| 207 | Havana St. | 9 | 7 | 7 | 21 | 5 |  | 18 | 3 |  | 33 |
| 208 | Peoria St. | 3 | 8 | 2 | 13 | 7 |  | 9 | 4 |  | 29 |
| 209 | 1-225 Interchange | 4 | 3 | 2 | 9 | 4 |  | 6 | 3 |  | 21 |
| 210 | Chambers Rd. | 4 | 3 | 2 | 0 |  |  |  |  |  | 0 |
| 211 | Pena Dr/N. Buckley Rd. | 2 | 3 | 3 | 8 | 4 |  | 4 | 4 |  | 24 |
| 212 | SH 32, Tower Rd. | 2 | 1 | 3 | 1 |  |  | 1 |  |  | 1 |
| 213 | SH 40, Colfax Ave. | 1 |  |  | 1 | 1 |  |  | 1 |  | 5 |
| 214 | Gun Clut Rd., Rd. N. (CO Rd. 18N) | 1 | 1 | 1 | 2 |  |  | 1 | 1 |  | 6 |
| 216 | SH 36, wlo Watkins |  | 1 |  | 0 |  |  |  |  |  | 0 |
| 216 | SH 70 Watkns Spur |  |  |  | 0 |  |  |  |  |  | 0 |
| 217 | Manila Rd. | 1 |  |  | 1 | 1 |  |  | 1 |  | 5 |
| 218 | SH 79, Bennett | 1 |  |  | 0 |  |  |  |  |  | 0 |
| 218 | Ramp to US 36 and Bennett Rest Area |  |  |  | 0 |  |  |  |  |  | 0 |
| 220 | SH 70 Strasturg Spur |  |  |  | 0 |  |  |  |  |  | 0 |
| 221 | SH 36, Byers |  |  |  | 0 |  |  |  |  |  | 0 |
| 222 | Peoria, Frontage Rd. conth. to SH 40 |  |  |  | 0 |  |  |  |  |  | 0 |
| 223 | SH 70 Deer Trail Spur |  |  |  | 0 |  |  |  |  |  | 0 |
| 224 | SH 70 Apate Spur |  |  | 1 | 1 | 1 |  |  | 1 |  | 5 |
| 225 | SH 86 | 2 | 1 |  | 3 | 2 |  | 1 | 2 |  | 11 |
| 226 | SH 24 Limon Spur | 2 | 1 |  | 0 |  |  |  |  |  | 0 |
| 227 | SH 24, e/o Limon | 4 |  | 2 | 3 | 1 |  | 2 | 1 |  | 7 |
| 228 | SH 24 and SH 40 | 1 |  | 2 | 0 | 1 |  |  |  |  | 0 |
| 229 | Genas Interchange |  |  |  | 1 |  |  | 1 |  |  | 1 |
| 230 | Bovina interchange |  |  | 1 | 1 | 3 |  |  | 1 |  | 5 |
| 231 | Arriba interchange |  |  |  | 0 |  |  |  |  |  | 0 |
| 232 | Flagter Interctrange |  |  |  | 1 | 1 |  |  | 1 |  | 5 |
| 233 | SH 59, swlo Seibert | 1 |  | 1 | 1 | 1 |  | 1 |  |  | 1 |
| 234 | SH 70, Vons Spur |  |  | 1 | 1 |  |  | 1 |  |  | 1 |
| 235 | SH 57. Stration |  |  |  | 0 |  |  |  |  |  | 0 |
| 236 | Bethune Interckange |  |  |  | 0 |  |  |  |  |  | 0 |
| 287 | SH 385, Burtington |  |  |  | 1 |  |  | 1 |  |  | 1 |
| 238 | Burlington Spur | 1 |  |  | 1 |  |  |  |  |  |  |
| Routes | I-225 |  |  |  | 7 |  |  | 7 |  |  | 7 |
| 2884 | -25 Interchange | 2 | 2 | 3 | 7 |  |  | 7 |  |  | 4 |
| 259 | Tamarac | 3 |  | 1 | 4 |  |  | 2 | 1 |  | 7 |
| 240 | Yosemite St. |  |  | 3 | 3 | 1 |  | 1 | 2 |  | 11 |
| 241 | SH 83, Parker Rd. | 2 |  | 1 | 3 | 3 |  | 2 | 1 |  | 7 |
| 242 | Ififf Ave. | 2 | $q$ |  | 8 | 1 |  | 7 | 1 |  | 12 |
| 243 | Mississippl Ave. | 5 |  | 3 | 8 | 1 |  | 7 |  |  | 1 |
| 244 | SH 30, 6th Ave. | 1 |  |  | 12 |  | 1 | 7 | 4 | 1 | 38 |
| 245 | SH 40, Colfax Ave. | 6 | 2 | 4 | 12 | 8 | 1 | 5 | 3 |  | 20 |
| 245A | -70 Interchange | 4 | 4 |  | 8 |  |  |  |  |  |  |
| Route - | 1-270 |  |  |  | 3 | 2 |  | 1 | 2 |  | 11 |
| 2458 | 1-78 Interchange | 1 | 1 | 1 | 4 | 2 |  | 4 |  |  | 4 |
| 246 | York St. | 2 |  | 2 | 4 |  |  | 4 | 1 |  | 11 |
| 247 | SH 6, Vasquez Blvd. | 4 | 1 | 2 | 7 | 1 |  | 6 | 1 |  | 6 |
| 248 | NB on ramp from SH 35 (Quebec St.) | 1 |  | 1 | 2 | 1 |  | 1 | 1 |  | 6 |


| Intrchg |  | $1993$ | $\begin{aligned} & \text { Accid } \\ & 1992 \end{aligned}$ |  |  |  | Total \# Acc. Fatal w/PDO | \# Acc. w/inj. | \# Acc. w/Fatal Index |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Num | SH 35, Quebec St. Cross Road | $\begin{array}{r} 1993 \\ .1 \end{array}$ | $2$ | 1 | 4 | 1 | $3$ | $1$ | 8 |
| Routes | 1-76 |  |  |  |  |  |  | 2 | 10 |
| 249A | t-70 and SH 121 Interchange |  |  | 2 | 2 | 2 | 1 | 2 | 10 |
| 250 | SH 95 (Sheridan Blvd.) |  | 1 | 1 | 1 |  | 1 |  | 1 |
| 251 | SH 287 (Federal Bivd.) | 1 | 1 |  | 1 |  | 1 |  | 1 |
| 252 | Assumed Pecos St. | 1 3 | 2 | 3 | 8 |  | 8 |  | 8 |
| 2524 | 1-25 | 3 | 2 | 3 | 2 | 3 |  | 2 | 10 |
| 253 | l-270 interchange | 2 | 1 |  | 1 | 3 | 1 |  | 1 |
| 254 | SH 224 |  | 1 |  | 0 |  |  |  | 0 |
| 255 | SH 6 | 2 |  | 1 | 3 | 3 | 1 | 2 | 11 |
| 256 | 88th Ave. | 2 |  | 1 | 3 | 3 | 3 |  | 3 |
| 257 | 96th Ave. | 1 |  | 3 | 4 | 2 | 2 | 2 | 12 |
| 258 | SH 85 | 1 |  | 3 | 0 |  |  |  | 0 |
| 259 | SH 2 | 1 |  | 1 | 2 | 3 |  | 2 | 10 |
| 260 | SH 51 | 1 |  |  | 0 |  |  |  | 0 |
| 261 | Rd. E. and W. (136th Ave.) |  |  |  | 0 |  |  |  | 0 |
| 262 | Rd. N. and S. (Burlington Blvd) (Barr Lake) |  |  |  | 0 |  |  |  | 0 |
| 263 | Rd. E. and W. (Bromley Ln.) | 1 |  | 1 | 2 | 2 | 1 | 1 | 6 |
| 264 | Rd. E. and W. (CO Rd. 2), Lockbuie | 1 |  | 1 | 1 | 2 | 1 |  | 1 |
| 265 | SH 52 | 1 |  | 1 | 2 | 1 | 1 | 1 | 6 |
| 266 | Kersey Interchange | 1 |  | 1 | 0 |  |  |  | 0 |
| 267 | SH 76 Keenesburg Spur |  |  |  | 0 |  |  |  | 0 |
| 268 | Roggen Interchange, CO Rd. 73 |  |  |  | 0 |  |  |  | 0 |
| 269 | Rainter Rd., (EB off only) |  |  |  | 0 |  |  |  | 0 |
| 270 | W. SH 6, w/o Wiggins |  |  |  | 0 |  |  |  | 0 |
| 271 | SH 39 |  | 1 |  | 1 |  | 1 |  | 1 |
| 272 | E. SH 6 and SH 34, e/o Wiggins |  | 1 |  | 0 |  |  |  | 0 |
| 273 | Long Bridge | 3 |  |  | 3 | 2 | 1 | 2 | 11 |
| 274 | SH 34 wfo Fort Morgan | 3 |  |  | 0 | 2 | 1 |  | 0 |
| 276 | SH 144 |  | 1 |  | 1 |  | 1 |  | 1 |
| 276 | SH 52 | 2 | 1 | 1 | 3 |  | 3 |  | 3 |
| 277 | Barlow Rd | 2 |  | 1 | 0 |  |  |  | 0 |
| 278 | Dodd Bridge |  |  |  | 0 |  |  |  | 0 |
| 278 | Hospital Rd. | 1 |  | 4 | 2 |  | 2 |  | 2 |
| 280 | SH7t | 1 |  | 1 | 0 |  |  |  | 0 |
| 281 | SH 6 and SH 34 Spur, ne/o Brush |  |  |  | 0 |  |  |  | 0 |
| 232 | Hilirose interchange |  | - |  | 0 |  |  |  | 0 |
| 283 | Merino Interchange |  |  | 1 | 1 |  | 1 |  | 1 |
| 284 | SH 63, Ahwood |  |  | 1 | 1 |  | 1 |  | 1 |
| 285 | SH 6, Sterling |  |  |  | 0 |  |  |  | 0 |
| 286 | Ifff Interchange |  |  |  | 0 |  |  |  | 0 |
| 287 | Proctor Interchange |  |  |  | 0 |  |  |  | 0 |
| 288 | SH 55, Crook |  |  |  | 0 |  |  |  | 0 |
| 289 | Red Lion Rd. |  |  |  | 0 |  |  |  | 0 |
| 290 | SH 59, Sedgwick |  |  |  | 0 |  |  |  | 0 |
| 291 | Ovid Interchange |  |  |  | 0 |  |  |  | 0 |
| 292 | SH 385, Julesburg |  |  |  | 0 |  |  |  |  |
| Route $\rightarrow$ | US 36 (Denver-Boulder Tpk) |  |  |  |  |  |  |  | 0 |
| 293 | SH 121 |  |  |  | 0 |  |  |  | 0 |
| 294 | 104th Ave |  |  |  | 0 |  |  |  | 0 |
| 295 | SH 95, Sheridan Blvd. |  |  |  | 0 |  |  |  | 0 |
| 296 | SH 287, Federal Blvd. |  |  |  | 0 |  |  |  |  |


| intrchg <br> Num | Cross Road | $\begin{gathered} \text { Accidents } \\ 199319921991 \text { Tot } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: |
| 297 | Zuni St. |  |  |
| 298 | Pecos St. |  |  |
| 299 | Broadwray |  |  |
| Route $\rightarrow$ | US 285 |  |  |
| 300 | SH 8 |  |  |
| 301 | SH 470 |  |  |
| 302 | SH 391 (Kipling Pwky.) |  |  |
| 303 | SH 121 (Wadsworth Bivd.) |  |  |
| 304 | SH 85 (Sheridan Blvd.) |  |  |
| 305 | Rd. N. (S. Knox Ct.) Rd. SW (S. Lowell Blvd.) |  |  |
| 306 | SH 88 (Federal Blvd.) |  |  |
| 307 | SH 85 (Santa Fe Dr.) |  |  |
| 308 | SH 75 (Broadway) |  |  |
| Route- ${ }^{\text {a }}$ | SH 470 |  |  |
| 309 | SH 8 |  |  |
| 310 | Quincy Ave. |  |  |
| 314 | Bowles Ave. |  |  |
| 312 | Ken Caryi |  |  |
| 313 | Kipting |  |  |
| 314 | SH 121 |  |  |
| 315 | SH 75 (Platte Canyon Rd.) |  |  |
| 316 | SH 85 (Santa Fe Dr.) |  |  |
| 317 | Broadway |  |  |
| 318 | SH 177 (University Blvd.) |  |  |
| 319 | Quebec |  |  |
| Routes | US 6 |  |  |
| 320 | Indiana St. |  |  |
| 321 | Simms St. |  |  |
| 322 | SH 391, Kipling St. |  |  |
| 323 | Gamison St |  |  |
| 324 | Carr St. |  |  |
| 325 | SH 121, Wadsworth Bivd. |  |  |
| 326 | Knax Ct. |  |  |
| 327 | SH 88, Federal Bivd. |  |  |
| 328 | Bryant St. |  |  |
| UC: | Interchange | Route | Index |
| 97 | Four38th Ave. | 1-25 | 45 |
| 98 | 1-70 Interchange | 1-25 | 53 |
| 98 | SH 53, 58th Ave. | 1-25 | 39 |
| 188 | SH 72, Ward Rd. | $1-70$ | 55 |
| 196 | Pecos 81. | 1-70 | 47 |
| 196A | 1-25 | -70 | 73 |
| 197 | Washington St. | 1.70 | 45 |
| 202 | SH 2, Colorado Blvd. | $1-70$ 1.70 | 36 |
| 205 | SH 35, Quebec St. | 1.70 | 36 |
| 207 | Havana St. | 1-70 | 36 |
| 245 | SH 40, Colfax Ave. | 1-225 | 39 |

## IMPLEMENTATION OF STUDY FINDINGS IN COLORADO

Following statistical analysis of truck accidents at interchanges a cloverleaf interchange in northem Colorado was identified as having higher than expected frequency of truck rollovers. The interchange of l-25 and SH 34 is depicted in Figure A. 1 below. To address the issue, larger warning signs were installed at the entrances to the ramps. Following installation of the warning signs an observational before and after study was conducted to evaluate the effectiveness of the counter measures. The results of the study are presented in Table A.2.


Figure A. 1 I-25 and SH 34 interchange

Observatlonal Before and After Study at the l-25 \& SH 34 Interchange


The observational before and after study did not indicate a significant impact on safety as a result of warning sign installation. A recommendation was made to the Regional Office to consider this site for potential improvement under the Hazard Elimination Program.

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[^0]:    - Desiga whicle with $48^{\circ}$ uriler as adopeed in 1982

    STAA (Surfice Trampormion Assisumer Act)

    * Deriga vecicle widh $53^{\prime}$ raiker as grand fodtered in

    1982 STAd (Surface Tracportaion Alsistame Act)

