

Memorandum

MATERIALS AND GEOTECHNICAL BRANCH
GEOTECHNICAL PROGRAM
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IM 088A-024

Federal Blvd over US-6

SA 16228

TO: Mahmood Hasan, Staff Bridge

FROM: David Thomas, Geotechnical Program

DATE: December 3, 2009

SUBJECT: GEOTECHNICAL RECOMMENDATIONS FOR REPLACEMENT OF STRUCTURE F-16-EK

1.0 INTRODUCTION

This report presents geotechnical investigation observations and recommendations for the replacement of existing bridge structure F-16-EK, which carries Colorado Highway 88 (Federal Blvd) over US-6 at mile marker 1. The purpose of the geotechnical investigation is to characterize physical properties of foundation materials at the proposed bridge and ramp retaining wall locations. Foundation recommendations are also provided for design and construction. The scope of work was based on conversations with Hsu-Kun (Nick) Cheng of Region 6 South Engineering and Mansour (Mike) Mohseni with Staff Bridge.

1.1 PROJECT DESCRIPTION

The current four span bridge was built in 1958 on timber piles. The proposed bridge will be a two span bridge, but widened to accommodate additional traffic and turn lanes. Retaining walls will be required to the south along US-6 to support a proposed on-ramp reconfiguration from Federal Blvd to east bound US-6 with heights estimated from 3 to 27 feet.

2.0 GEOTECHNICAL INVESTIGATION

Geotechnical field activities were completed from May 4th through 20th, 2009. Five borings, TH1 through TH5, were advanced at the proposed pier and abutment locations. Ten borings, TH6 through TH15, were advanced at the proposed wall locations along US-6. The borings were advanced using a CME 75 truck mounted and a CME 550 all-terrain drill rigs with hollow stem auger and wire line core techniques. Standard penetration tests using split spoon samplers and California samplers were performed in the borings at select intervals per ASTM D-1586 and D-3550, respectively.

Traffic control was required for the abutment borings (TH1 through TH3) to allow for drilling on the exit and on ramps to US-6. Traffic control for the ramps was coordinated and provided by Jeff Martinez with CDOT. Night traffic control was also required to drill three borings. The

first was the pier location (TH5) in the No. 1 east bound lane on US-6. The remaining two borings (TH14 and TH15) were drilled on the Bryant St. exit ramp from US-6 for wall foundations. The borings were advanced in the exit lane because the rig could not safely access the proposed wall location approximately 20 feet to the south due to steep embankment topography and adjacent private property. The night traffic control was coordinated with Anthony Bertram from CDOT Patrol 7.

2.1 GEOLOGY

The general geology consists of medium stiff to very stiff clay overlaying medium dense to very dense well graded sand overlaying very hard claystone bedrock. Bedrock was encountered between 5,171 feet above mean sea level (amsl) (83 feet below ground surface [bgs]) to the north and 5,173 feet amsl (84 feet bgs) to the south. Soil and bedrock characteristics were consistent among borings. Groundwater was encountered in the borings during drilling between 5,194 feet amsl (28 feet bgs) to the east in TH14 and 5,224 feet amsl (32 feet bgs) to the west in TH3. Flowing sand conditions existed in areas where sand was present below the groundwater table. The boring logs and geology sheets are presented in Attachments 1 and 2, respectively.

2.2 PHYSICAL PROPERTIES

Clay samples resulted in AASHTO classifications of A-6 to A-7-6 with group indexes ranging from 1 to 31. Claystone samples resulted in an AASHTO classification of A-7-6 with group indexes of 29 to 40. The uniaxial compressive strengths for four bedrock samples ranged from 12.2 to 15.6 kips per square foot (ksf) and averaged 14.5 ksf. The unconfined compression test samples were obtained with a California sampler and may be lower than insitu values. Swell-consolidation results ranged from 0.1% to 2.0% under a 1 ksf load for clay samples collected beneath the proposed wall footings. Detailed material properties are presented in the laboratory test summary in Table 1.

2.3 GEOCHEMISTRY

The bedrock was analyzed for percent sulfate, pH and resistivity. Based on the results of water soluble sulfate testing obtained from CP 2103, the potential for sulfate attack on Portland cement concrete in direct contact with the bedrock would be classified as a Class 0 exposure per Table 601.4 of the CDOT Standard Special Revision Section 601. Results for bedrock pH suggests no corrosion potential or non-aggressive behavior, however, bedrock resistivity values suggest a strong corrosion potential or aggressive behavior. Foundation design should consider a strong corrosion potential based on the resistance values per Table C.1 of FHWA report FHWAO-IF-3-017, Geotechnical Engineering Circular No. 7 - Soil Nail Walls.

3.0 RECOMMENDATIONS

The subsurface conditions are favorable for a bridge on drilled shaft or driven pile foundations. The ultimate capacity for design typically assumes a weighted load factor of 1.5 and a resistance factor of 0.5 when using the Load and Resistance Factor Design (LRFD) method.

TABLE 1
SA 16628: FEDERAL BLVD (SH-88) OVER US-6
LABORATORY TEST SUMMARY

Boring No.	Depth (ft bgs)	Elevation (ft amsl)	Sample No.	Visual Description	USCS	AASHTO	AASHTO Gradation				Liquid Limit	Plastic Limit	Plastic Index	Water Content (%)	Dry Density (lb/ft³)	Uniaxial Compressive Strength (psf)	Water Soluble Sulfates (%)	Swell Consolidation (%)	Soil pH H ₂ O/C _a Cl ₂	Resistivity ohm/cm Saturated
							Gravel (%)	Coarse Sand (%)	Fine Sand (%)	Silt & Clay (%)										
TH1	4.0		1B	Clay	CL	A-6 (9)	4.8	8.6	30.0	56.5	38	16	22	15.6	—	—	—	—	—	—
TH1	19.0		1C	Clayey Sand	SC	A-6 (1)	9.0	17.5	37.5	35.9	35	19	16	19.8	—	—	—	—	—	—
TH1	74.0		1G	Gravel	GW-GC	—	48.3	24.0	18.1	9.6	—	—	—	8.6	—	—	—	—	—	—
TH2	23.0		2C	Clay	CL	—	0.0	0.5	10.3	89.1	—	—	—	28.8	—	—	—	—	—	—
TH2	68.5		2G	Sand	SW	—	31.4	33.0	31.5	4.1	—	—	—	13.2	—	—	—	—	—	—
TH2	98.0		2J	Claystone	CH	A-7-6 (30)	0.2	0.0	0.3	99.5	50	24	26	15.2	117.7	15,623	0.02	—	—	—
TH3	33.0		3C	Clay	CL	—	0.1	0.9	15.6	83.5	—	—	—	27.2	—	—	0.01	—	—	—
TH3	93.0		3F	Claystone	CL	—	0.0	0.0	0.0	100.0	—	—	—	15.1	116.4	15,047	0.01	—	—	—
TH4	18.5		4C	Clayey Sand	SC	—	0.6	12.2	39.3	47.9	—	—	—	19.4	—	—	—	—	—	—
TH4	28.5		4D	Clay	CH	A-7-6 (31)	0.1	0.6	11.9	87.5	53	19	34	30.1	93.2	—	—	—	—	—
TH4	53.5		4F	Clay	CL	A-6 (11)	0.3	4.7	30.5	64.5	40	19	21	28.1	94.8	—	0.01	—	—	—
TH4	93.5		4I	Claystone	CH	A-7-6 (29)	0.0	0.0	0.1	99.9	50	25	25	17.1	114.3	12,236	0.01	—	—	—
TH4	90.0		4-BR	Claystone	—	—	—	—	—	—	—	—	—	15.3	118.3	—	0.01	—	8.27	—
TH5	69.0		5G	Claystone	CH	A-7-6 (40)	0.0	0.0	0.1	99.9	55	19	36	15.3	118.3	15,029	0.00	—	—	—
TH6	15.0		6B	Sandy Clay	CL	A-7-6 (11)	3.4	11.2	29.7	55.7	42	16	26	17.9	—	—	—	—	—	—
TH6	24.0		6C	Clay	CL	A-6 (10)	4.0	5.9	30.8	59.3	40	19	21	28.4	94.1	—	0.00	—	—	—
TH6	35.0		6D	Clay	CL	—	—	—	—	76.5	—	—	—	26.9	—	—	—	—	—	—
TH7	13.5		7B	Clay	CL	A-7-6 (17)	0.9	7.5	27.5	64.1	48	18	30	22.7	102.1	—	—	1.5	—	—
TH8	18.0		8C	Clay	CL	A-7-6 (20)	0.0	0.2	18.7	81.1	42	17	25	25.5	—	—	0.00	—	—	—
TH8	48.0		8F	Clay	—	—	—	—	—	73.7	—	—	—	32.1	—	—	—	—	—	—
TH9	23.5		9C	Clay	CL	A-7-6 (21)	0.0	1.7	13.9	84.4	44	19	25	31.7	92.2	—	—	1.1	—	—
TH9	33.5		9D	Clay	CL	A-7-6 (17)	1.1	8.1	26.9	63.9	47	17	30	22.5	103.9	—	—	—	—	—
TH9	58.5		9F	Clay	CL	—	—	—	—	90.0	—	—	—	36.6	—	—	—	—	—	—
TH10	4.5		10B	Clay	—	—	—	—	—	89.3	—	—	—	17.6	105.3	—	—	—	—	—
TH10	14.5		10E	Clay	CL	A-7-6 (11)	1.9	11.0	31.9	55.1	45	18	27	21.7	102.4	—	—	2.0	—	—
TH11	19.5		11C	Clay	CL	A-7-6 (30)	0.0	1.3	14.2	84.5	54	20	34	26.3	—	—	0.08	—	—	—
TH11	39.5		11E	Gravel	GW	—	51.2	33.4	13.6	1.8	—	—	—	10.2	—	—	—	—	—	—
TH12	9.5		12B	Sandy Clay	CL	A-6 (10)	3.2	6.2	25.8	64.7	37	18	19	12.7	—	—	0.03	—	—	—
TH13	14.5		13C	Sand	SW-SC	—	46.5	40.9	8.4	5.1	—	—	—	2.1	—	—	—	—	—	—
TH13	39.5		13F	Sand	SW	—	37.8	48.7	11.1	2.5	—	—	—	12.7	—	—	—	—	—	—
TH14	9.5		14B	Clay	CL	—	—	—	—	63.8	—	—	—	23.2	—	—	0.07	—	—	—
TH15	24.0		15C	Clay	CL	A-7-6 (10)	13.8	7.5	23.5	55.2	43	18	25	11.6	111.1	—	—	0.1	—	—
COM	88.0		BR	Claystone	—	—	—	—	—	—	—	—	—	—	—	—	0.01	—	8.40	700

3.1 DRILLED SHAFTS

For drilled shafts embedded into the bedrock the ultimate end bearing capacity, q_p , and the ultimate side shear capacity, q_s , required for the LRFD method are presented in Table 2. Allowable end bearing capacity, q_a , and the allowable side shear capacity, f_a , for the Allowable Stress Design (ASD) method also are reproduced in Table 2. The side shear values are applicable in both vertical directions without reduction. Should a different load factor be applied for shafts, the resistance factor should be adjusted by dividing the new load factor by 3, to obtain the corresponding resistance factor.

The recommended minimum bedrock penetration is 10 feet. Side shear in the overburden soil should be ignored due to the difference in strain limit between the soil and bedrock. Also, the top 5 feet of bedrock penetration should be ignored for side shear resistance due to material weathering and potential disturbance from temporary casing.

TABLE 2. RECOMMENDED DRILLED SHAFT RESISTANCE VALUES FOR BEDROCK

Location	Estimated Bedrock Elevation (feet)	ASD		LRFD	
		q_a (ksf)	f_a (ksf)	q_p (ksf)	q_s (ksf)
North Abutment, West Edge	5,172	45	4.5	135	13.5
North Abutment, East Edge	5,172				
South Abutment, West Edge	5,172				
South Abutment, East Edge	5,172				
Center Pier	5,173				

The recommended axial capacities assume a minimum spacing of 2.5 shaft diameters, center-to center, between adjacent drilled shafts. Drilled shafts spaced at 2 diameters will require a reduction factor of 0.9. Closer spacing would require additional analysis and iteration with the structural engineer. The native soil overlying the bedrock or new embankment fill should be neglected when calculating the axial resistance, however, these materials can be considered for the lateral resistance. Material properties presented in Table 3 should be utilized when performing the lateral load analysis of the drilled shafts using LPILE or similar software.

Caving soil may occur above the bedrock elevation. Slurry and/or casing will be needed to support the soils overlying the bedrock during drilled shaft excavation if caving occurs. Dewatering of the drilled holes also may be required prior to placement of the concrete. The potential for dewatering may increase with the amount of time the drill holes remain open. Alternatively, the concrete may be placed by tremie or other methods to avoid placement of concrete into water.

3.2 DRIVEN PILES

For driven piles with Grade 36 steel, a combined skin friction and end bearing ultimate capacity of 27 kips per square inch (ksi) times the cross sectional area of the pile is recommended. For Grade 50 steel, the ultimate capacity would be increased to 36 ksi. Per CDOT Construction Manual Standard Special Provision 502, a pile driving analyzer will be recommended to establish driving criteria. A resistance factor of 0.65 may be used in accordance with AASHTO LRFD specifications. Driven piles would function as end bearing piles at this site with generally less than 5 feet of penetration into bedrock estimated without pre-drilling. Battered piles no steeper than 1:4 (H:V) may be used to provide lateral capacity.

**TABLE 3. RECOMMENDED MATERIAL PROPERTIES FOR
 LATERAL LOAD ANALYSIS USING LPILE**

Material	Internal Friction Angle ϕ (degrees)	Cohesion C (lb/ft ²)	Horizontal Subgrade Reaction k_h (lb/in ³)	Strain at $\frac{1}{2}$ the max principle stress difference ϵ_{50} (in/in)	Total Unit Weight γ_T (lb/ft ³)	Saturated Unit Weight γ_T (lb/ft ³)
New Class 1 Structure Backfill	34	0	64	–	125	135
Native Clay	0	1,000	250	0.010	110	120
Native Sand	32	0	20	–	125	135
Bedrock	0	10,000	1,000	0.005	135	145

3.3 RETAINING WALLS

The subsurface conditions appear favorable for a shallow foundation for retaining walls. Retaining walls vary in height and length from approximately 15 to 33 feet and 40 to 775 feet, respectively. Wall construction will also vary including MSE, cast in place, caisson, cut and fill walls. For retaining wall requiring fill, it is assumed new fill will consist of Class 1 Structure Backfill or borrow material from the onsite sources. Approved backfill from onsite borrow sources or Class 1 Structural Backfill should be compacted to at least 95 percent of the maximum dry density and within 2 percent of optimum moisture content as determined by AASHTO T180 (ASTM D 1557) and as described in Section 203 of the 2005 CDOT Standard Specification for Road and Bridge Construction. Table 4 summarizes the proposed walls and characteristics. The locations of the walls are presented on the attached geology sheets.

TABLE 4. SUMMARY OF RETAINING WALL CHARACTERISTICS

Wall No.	Approx. Maximum Height (ft)	Approx. Length (ft)	Approx. Footing Elevation (ft amsl)	Wall Type (Cut/Fill)	Foundation Soil Type
1	27	40	5,224	Cut	Clay
2	27	775	5,224	Cut & Fill	Clay
3	18	610	5,202	Cut & Fill	Clay
4	18	275	5,208	Fill	Clay & Sand
5	15	120	5,232	Fill	Clay

Retaining wall material parameters for design are presented in Table 5. The coefficients of earth pressure correspond to an active pressure equivalent fluid unit weight of 35 pounds per cubic foot (lb/ft^3) for Class 1 Structural Backfill. Lateral pressures must be reevaluated when sloping backfill or surcharge loads exist. A coefficient of sliding resistance (μ) of 0.45 may be used between concrete or MSE and undisturbed foundation soil. Temporary excavation support will be required where slopes are steeper than 1:1 (H:V). Parameters presented in Table 5 also are suitable for temporary excavation support design. Parameters presented in Table 3 should be utilized when performing the lateral load analysis of drilled shafts using LPILE or similar software.

TABLE 5. MATERIAL PARAMETERS FOR RETAINING WALLS AND TEMPORARY EXCAVATIONS

Material	Typical Total Unit Weight γ_T (pcf)	Internal Friction Angle ϕ (degrees)	Cohesion C (psf)	Earth Pressure Coefficients		
				Active (Ka)	At Rest (Ko)	Passive (Kp)
New Class 1 Structure Backfill	125	34	0	0.28	0.44	3.5
Native Clay	110	20	1,000	0.49	0.66	2.0
Native Sand	125	32	0	0.33	0.47	3.3

The recommendations for drilled shafts presented in Section 3.1 may be used for caisson wall design. It is recommended that the edge to edge spacing between the caissons be limited to 0.25 times the caisson diameter or 18 inches, whichever is less.

The subsurface conditions appear favorable for a soil nail wall along cut wall sections. Using Table 3.10 from Geotechnical Engineering Circular No. 7: Soil Nail Walls (FHWA Report No. A0-IF-03-017), estimated ultimate bond strength for soil nails are 0.6 to 1.2 kip/ft² in the silty clay soils and 2.0 to 2.7 kip/ft² in the sand soils. It is recommended that Class I corrosion protection involving grout and PVC sheathing encapsulation be used for soil nail walls.

Ultimate bearing capacity values for walls 1, 2 and 5 were calculated to be 5.5 kip/ft² in the native clay. Ultimate bearing capacity values for walls 3 and 4 were calculated to be 8 kip/ft² where the native clay was underlain by sand. Bearing capacity values assume a foundation width of 40% of height, 3 foot minimum embedment for frost protection, a resistance factor of 0.5 and a load factor of 1.5. The global stability of the walls should be verified after final design is completed. Maximum wall settlement should be less than 3 inches and take up to two years. A majority of the settlement will occur during construction of the walls.

4.0 SEISMIC DESIGN PARAMETERS

The AASHTO Specifications for LRFD Seismic Bridge Design classify the site as "E" and the seismic zone as "1" using Tables 3.10.3.1-1 and 3.10.6-1, respectively. Using the USGS AASHTO Earthquake Motion Parameters program, the seismic design spectrum plots were created for Spectral Acceleration vs. Time and Spectral Acceleration vs. Spectral Displacement and are presented in Figures 1 and 2, respectively. Additional data from the program is included in Attachment 3. Please contact the Geotechnical Program at 303-398-6604 with questions.

REVIEW: Liu

COPY: Akhavan – Reg.6 RTD
Gross – Reg. 6 South Resident Engineer
Cheng – Reg. 6 South Engineering
Ghaeli/Mero – Reg. 6 Materials
Mohseni – Staff Bridge
Werdel – Reg. 6 Hydraulics
Zufall/Kotzer – Branch Materials & Geotech

FIGURE 1. DESIGN SPECTRAL ACCELERATION VS. TIME

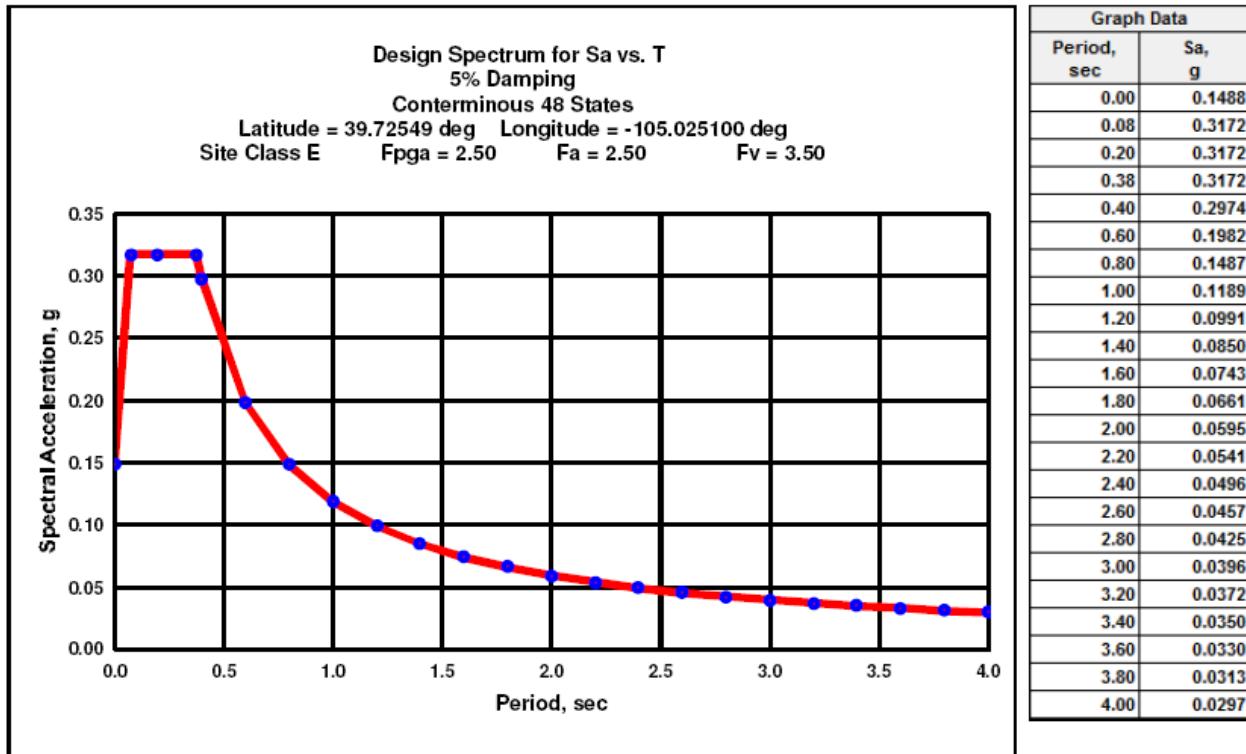
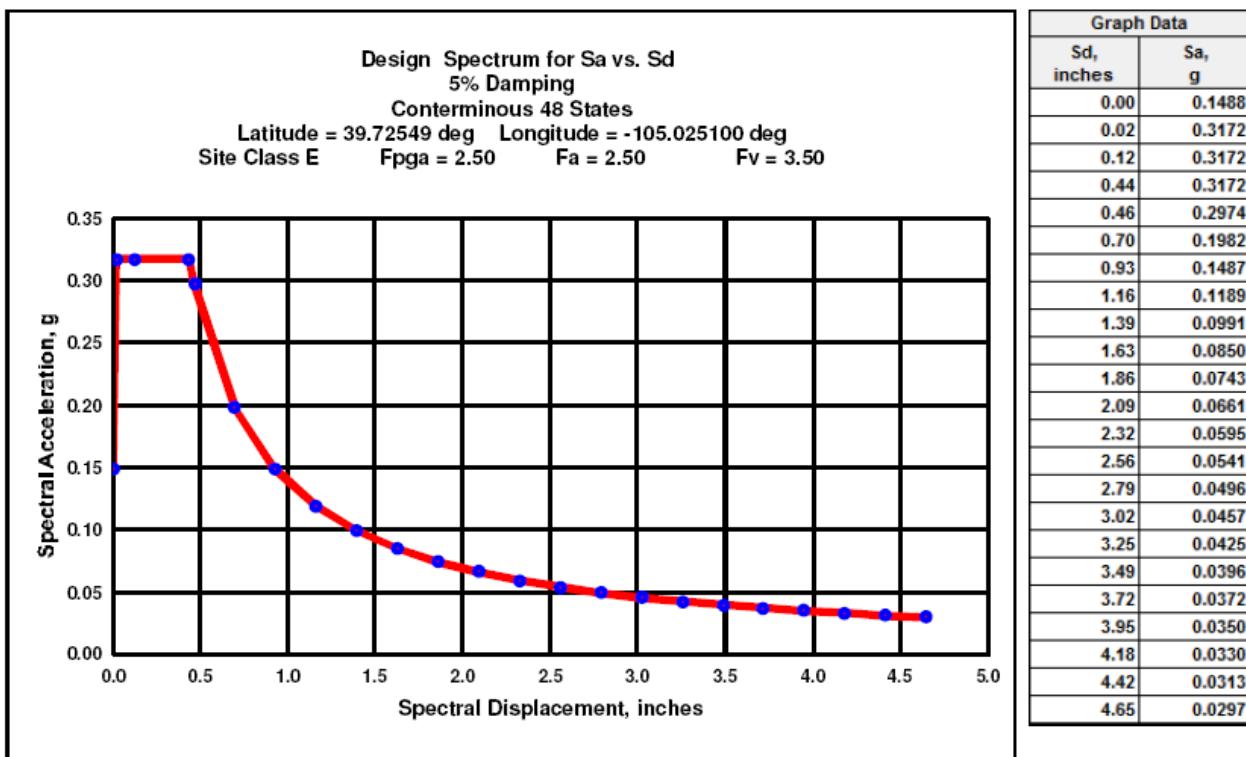


FIGURE 2. DESIGN SPECTRAL ACCELERATION VS. SPECTRAL DISPLACEMENT



ATTACHMENT 1
IM 088A-024, SA 16628, FEDERAL BLVD OVER US-6
BORING LOGS



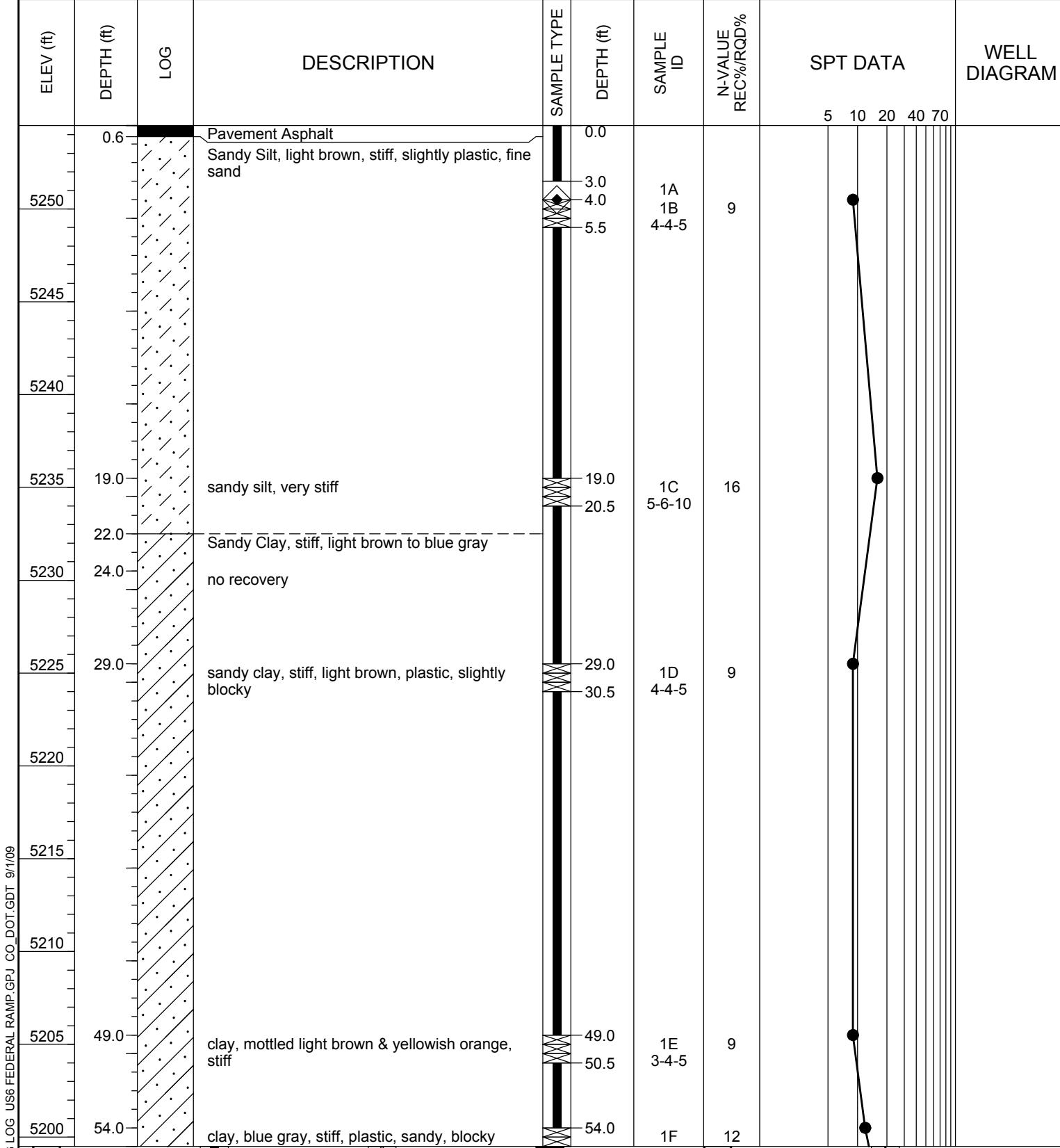
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

1

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/4/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,254.5ft		TOTAL DEPTH 90.0ft		SURVEY INFO N: 687,604 E: 952,764		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH

DATE

TIME

NOTES: CME 75, Wireline backfilled with cuttings



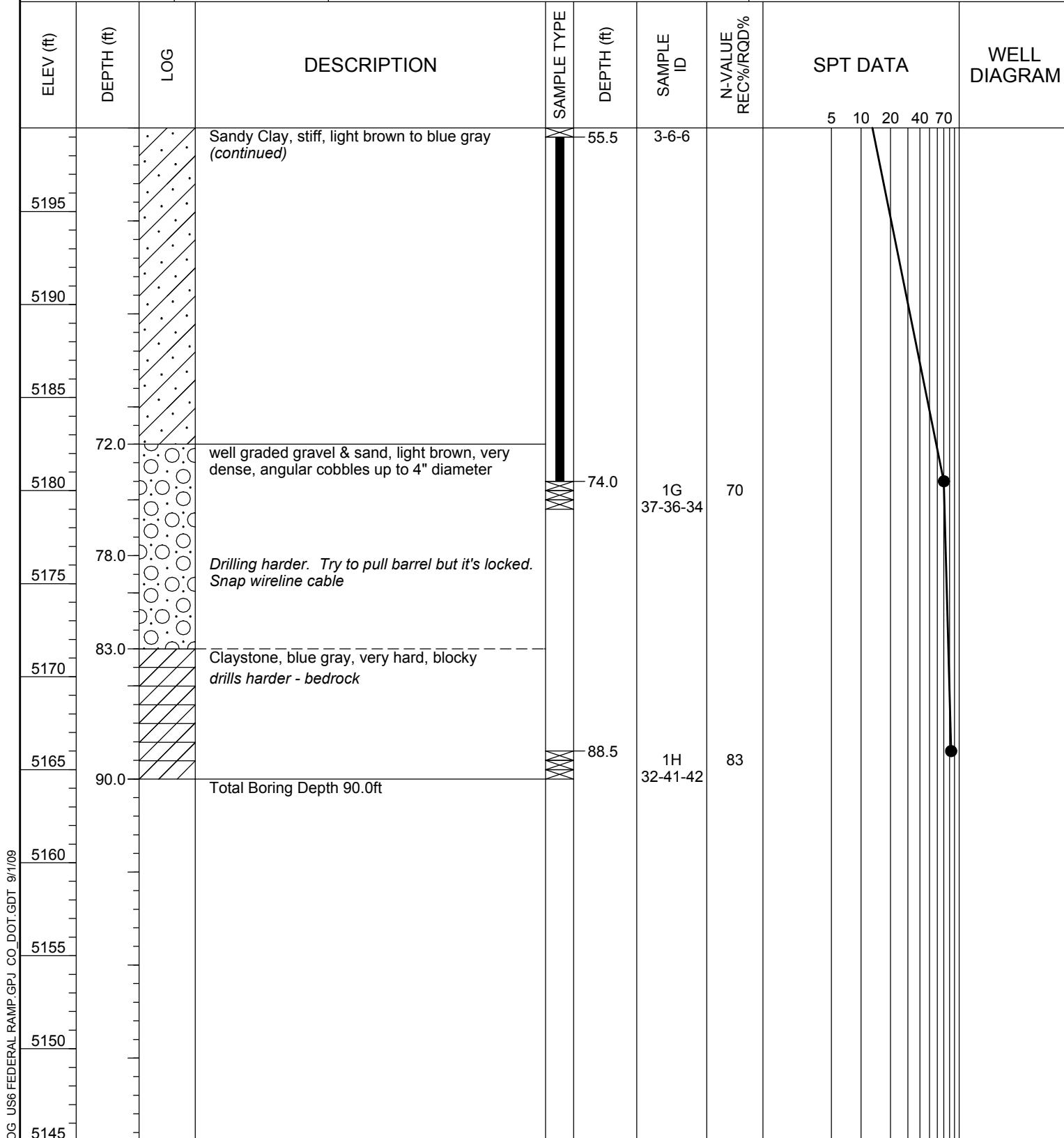
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

1

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/4/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,254.5ft		TOTAL DEPTH 90.0ft		SURVEY INFO N: 687,604 E: 952,764		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



SPT	CON'T	GRAB	SHELBY	CORE	CALIFORNIA
H ₂ O DEPTH					NOTES: CME 75, Wireline backfilled with cuttings
DATE					
TIME					



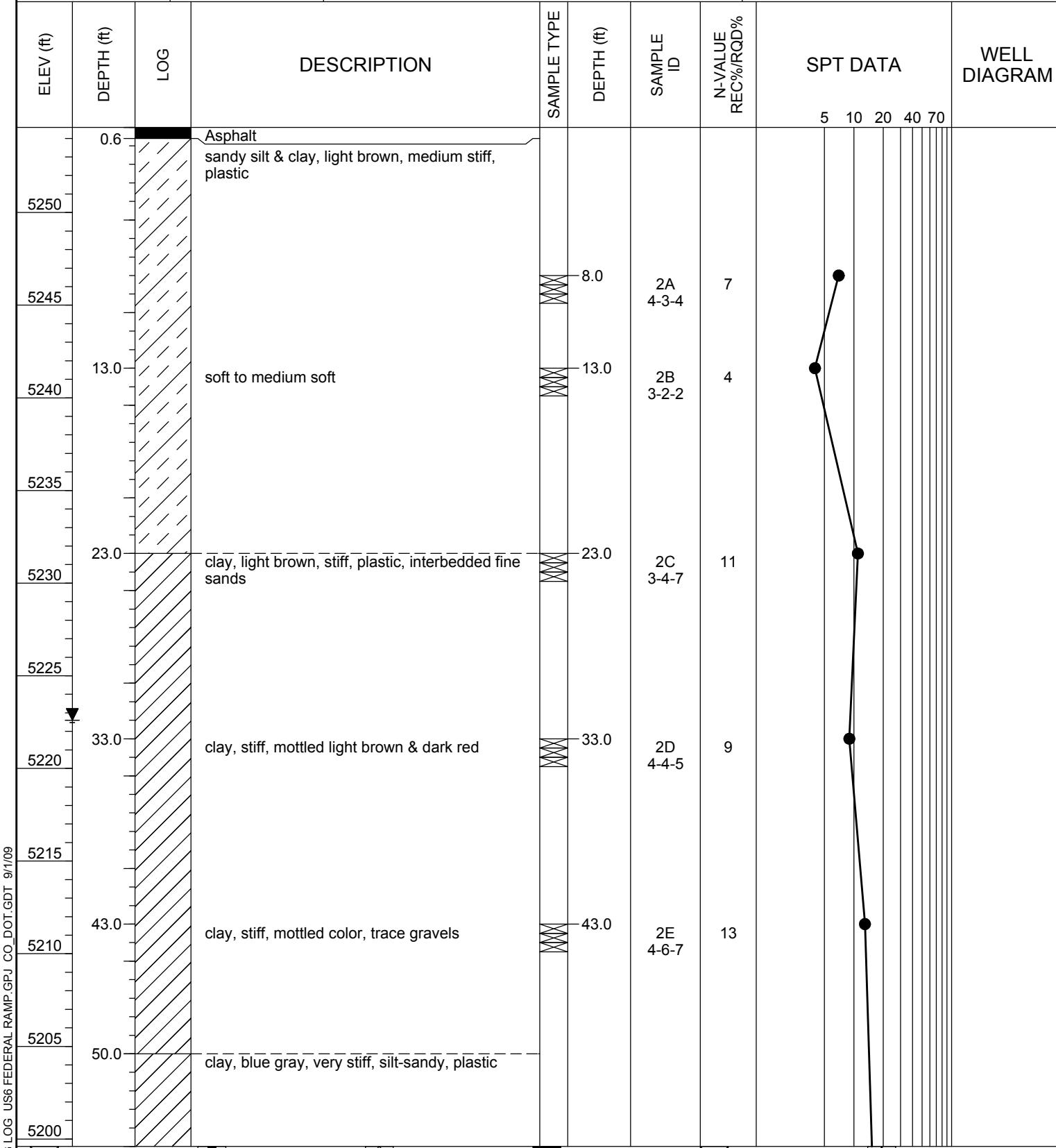
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

2

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/5/09	
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88			
TOP HOLE ELEV 5,254.6ft		TOTAL DEPTH 99.0ft	SURVEY INFO N: 687,606 E: 952,625			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno	



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 32.0 NOTES: CME 75, Auger backfilled with cuttings

DATE 5/5/09

TIME



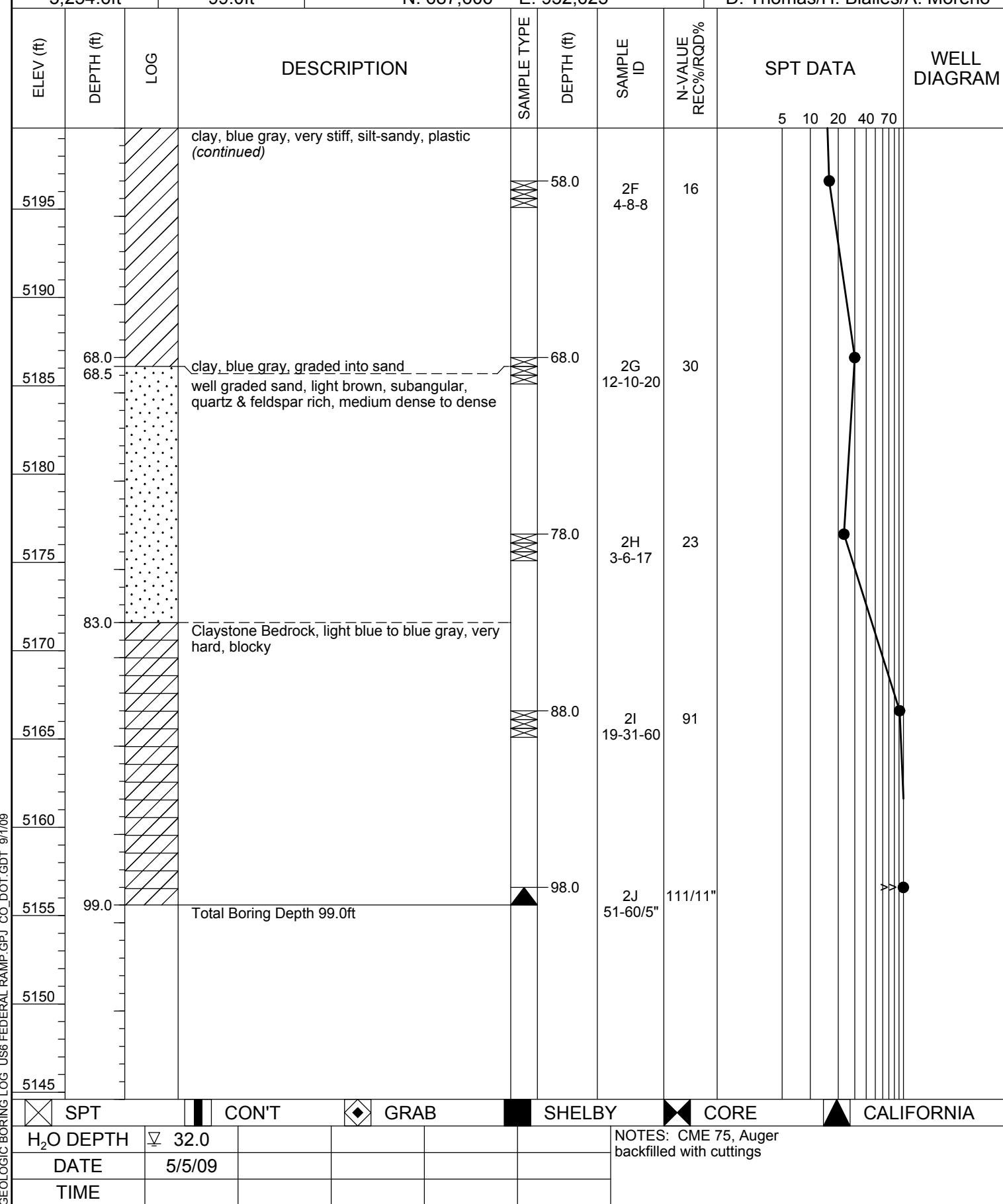
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

2

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/5/09			
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88				
TOP HOLE ELEV 5,254.6ft	TOTAL DEPTH 99.0ft	SURVEY INFO N: 687,606 E: 952,625			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno				





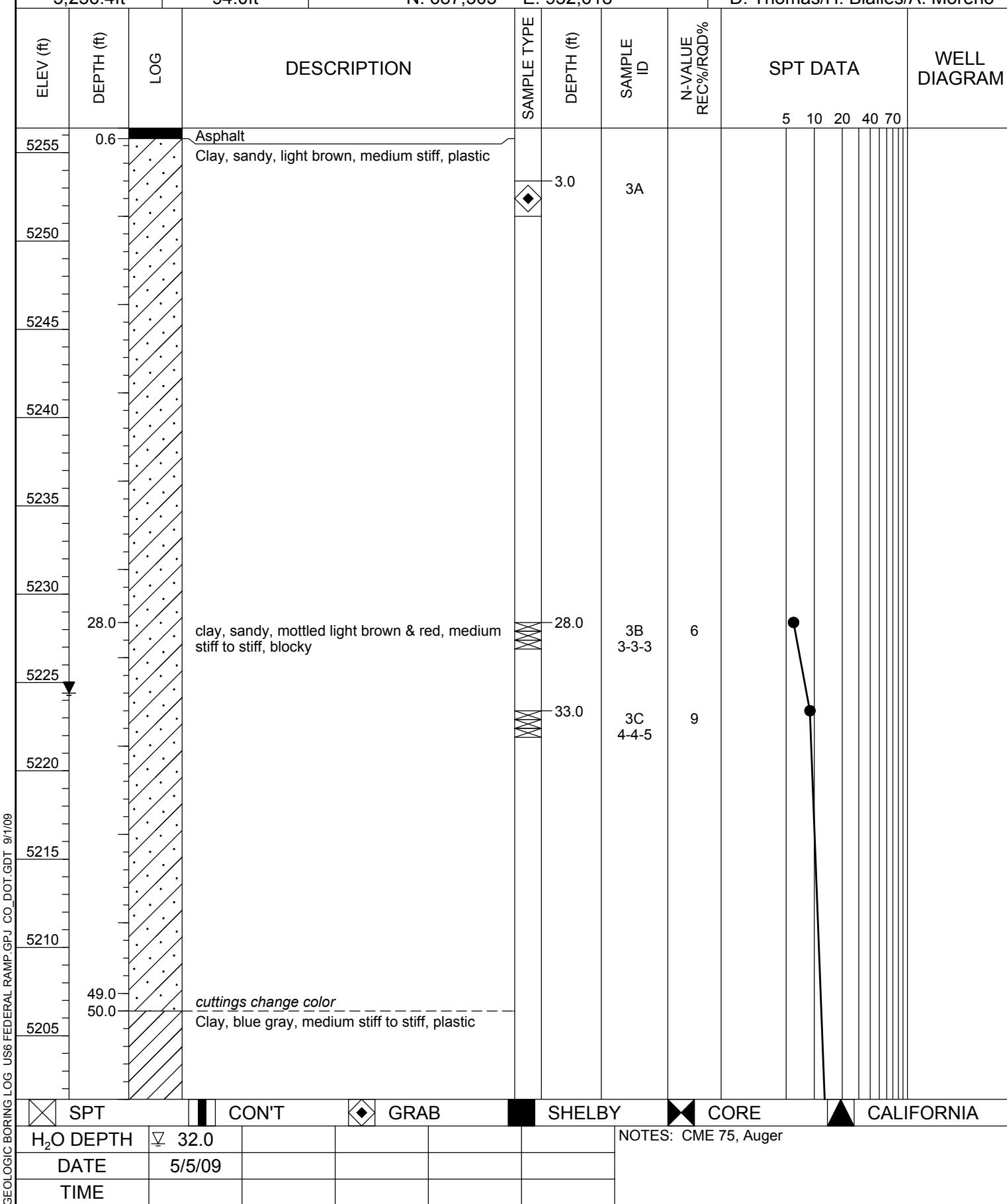
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

3

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/6/09
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88	
TOP HOLE ELEV 5,256.4ft	TOTAL DEPTH 94.0ft	SURVEY INFO N: 687,305 E: 952,618			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno	





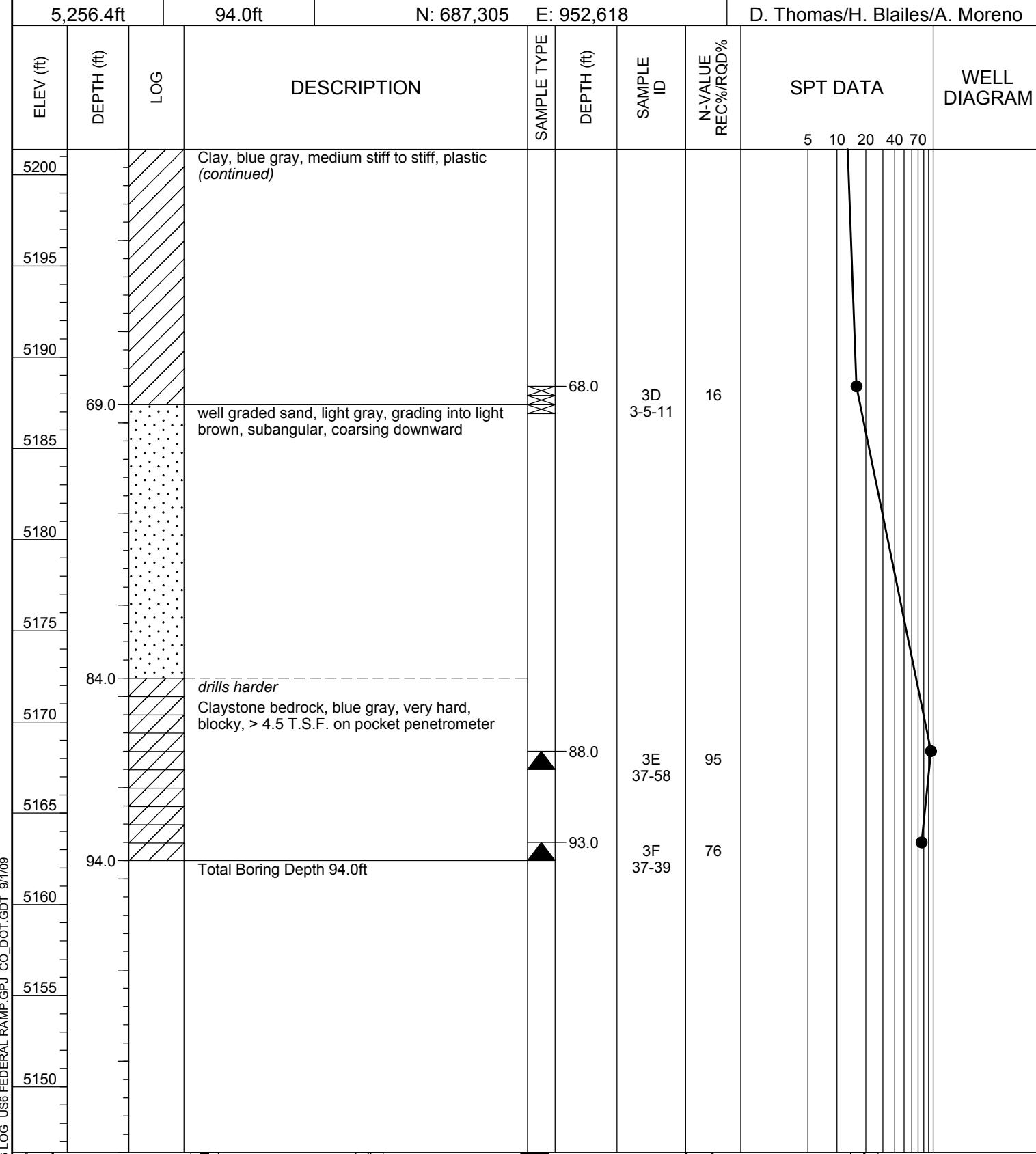
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

3

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/6/09
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88	
TOP HOLE ELEV 5,256.4ft	TOTAL DEPTH 94.0ft	SURVEY INFO N: 687,305 E: 952,618			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno	



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 32.0 NOTES: CME 75, Auger

DATE 5/5/09

TIME



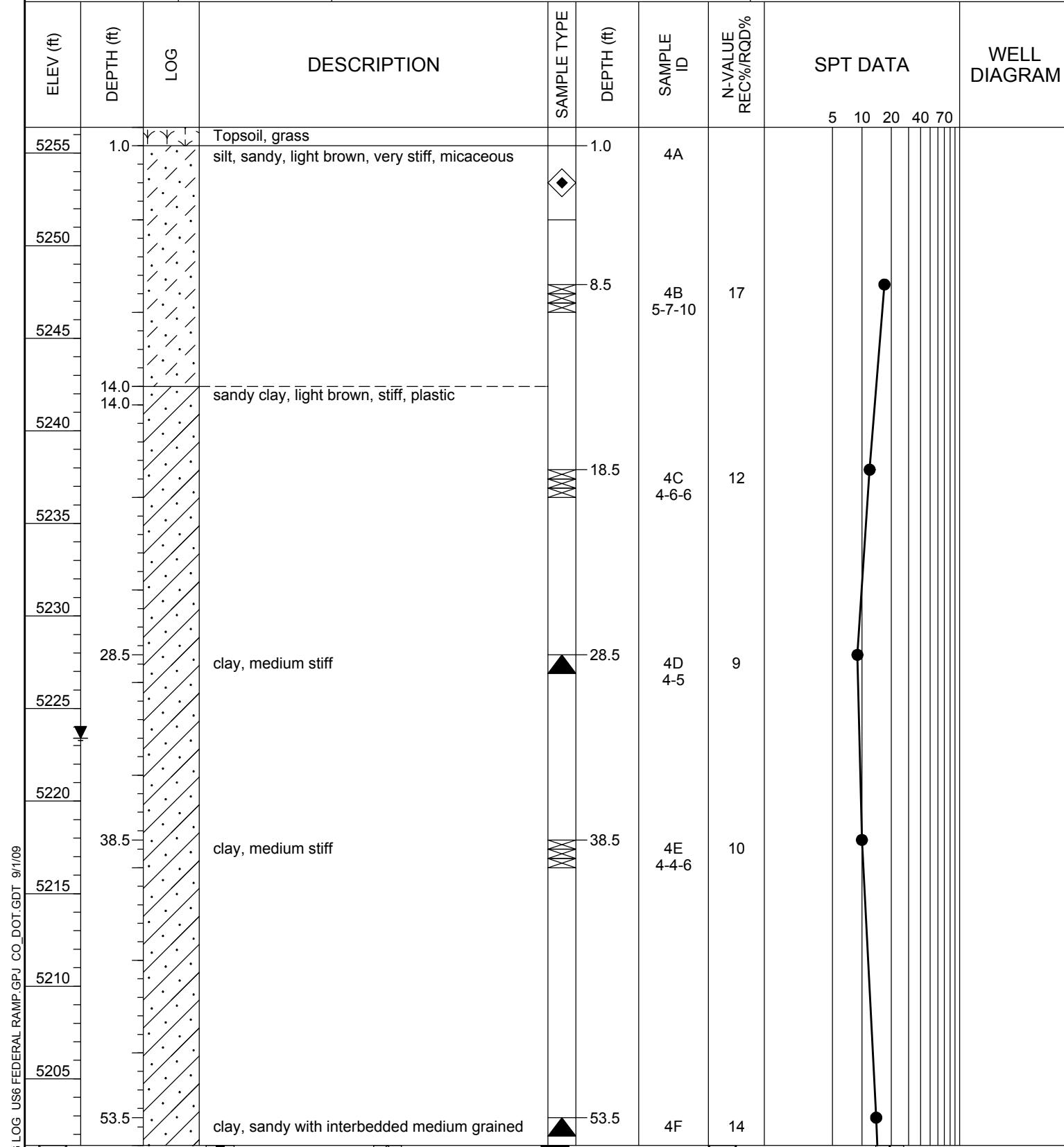
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

4

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/6/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88							
TOP HOLE ELEV 5,256.4ft		TOTAL DEPTH 95.0ft	SURVEY INFO N: 687,315 E: 952,759			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM





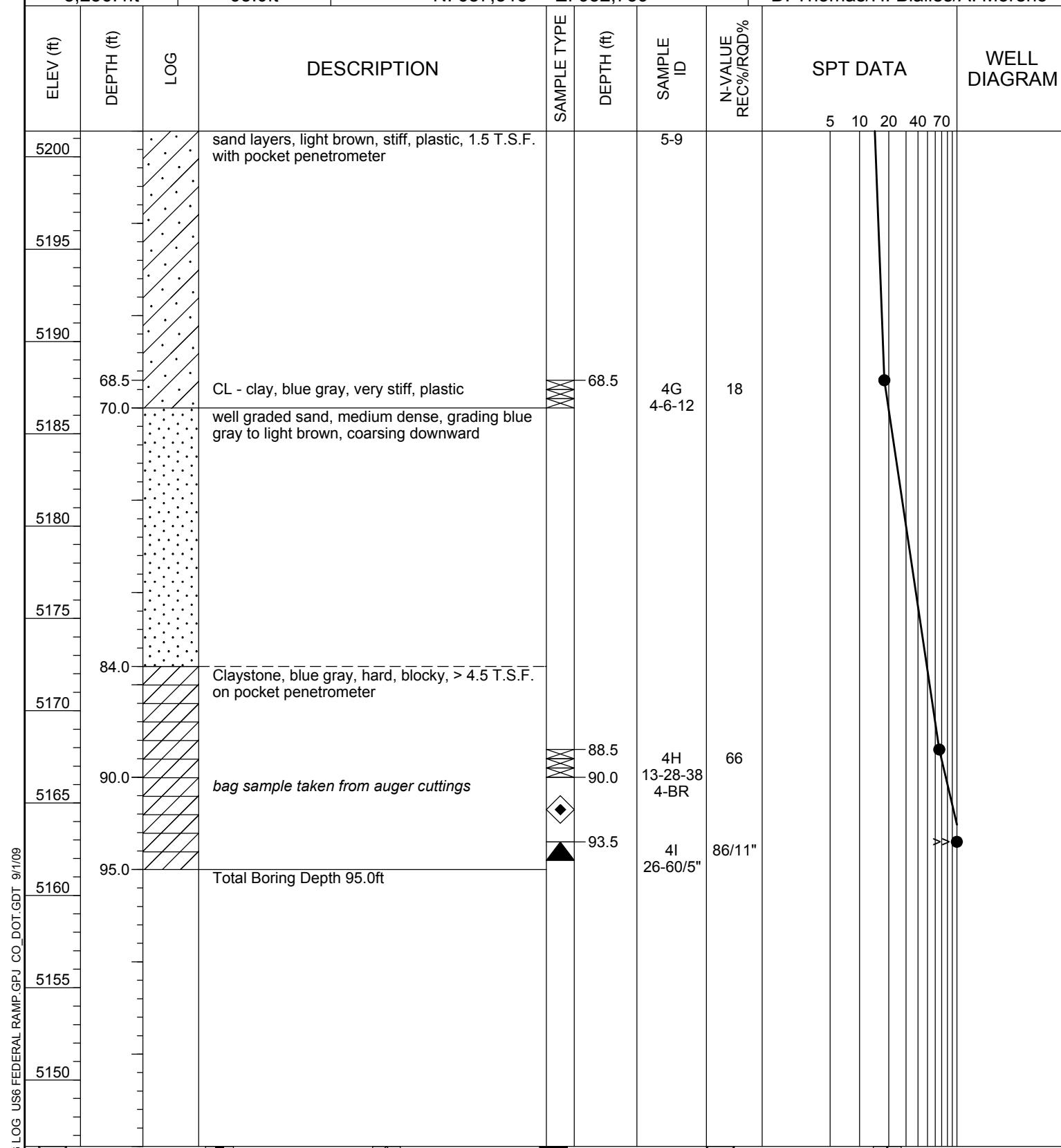
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

4

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/6/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88							
TOP HOLE ELEV 5,256.4ft		TOTAL DEPTH 95.0ft	SURVEY INFO N: 687,315 E: 952,759			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 33.0 NOTES: CME 75, Auger

DATE 5/6/09

TIME



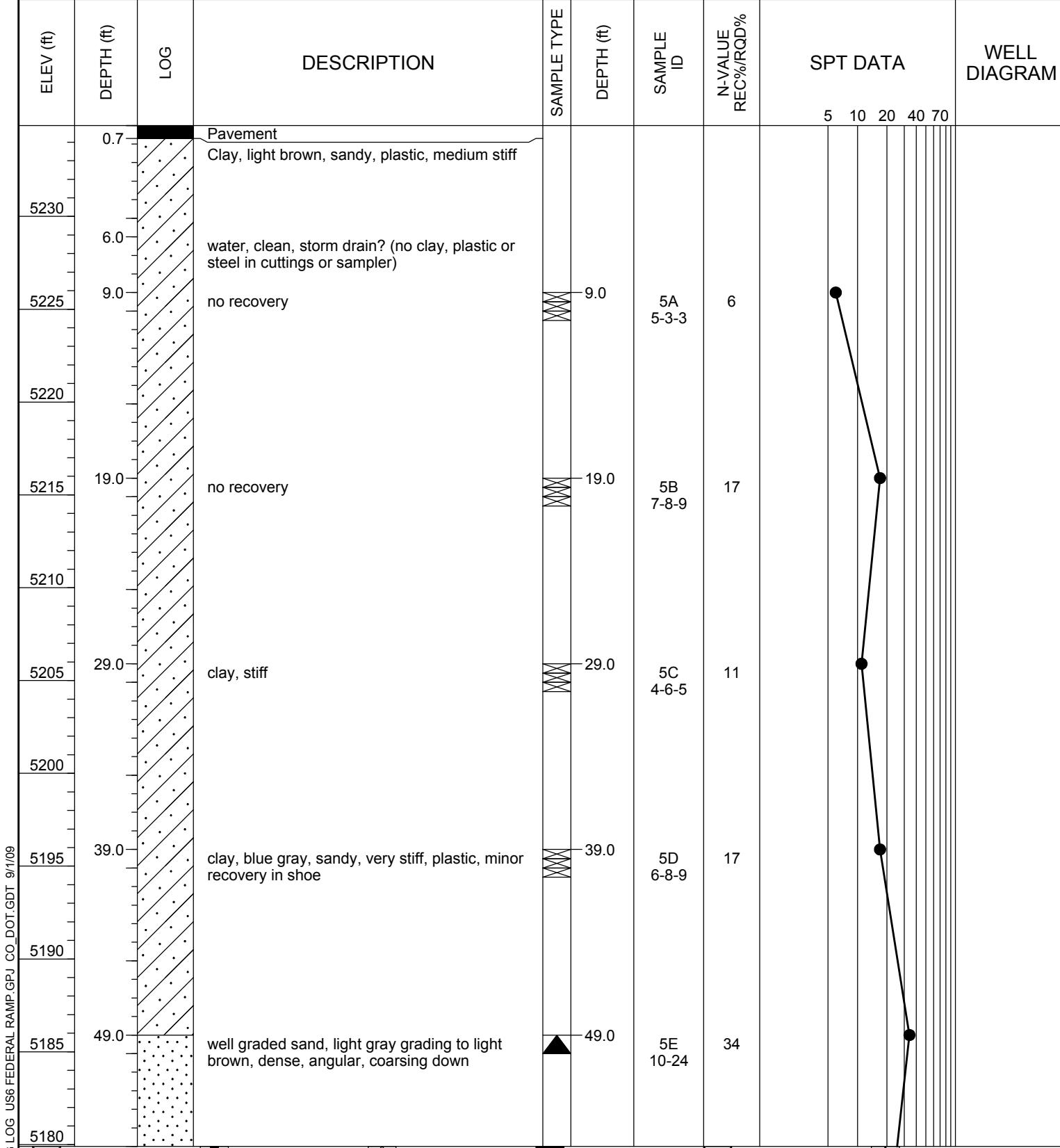
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

5

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/7/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,234.9ft		TOTAL DEPTH 70.0ft		SURVEY INFO N: 687,450 E: 952,723		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



H₂O DEPTH

DATE

TIME

NOTES: CME 75, Auger backfilled with cuttings



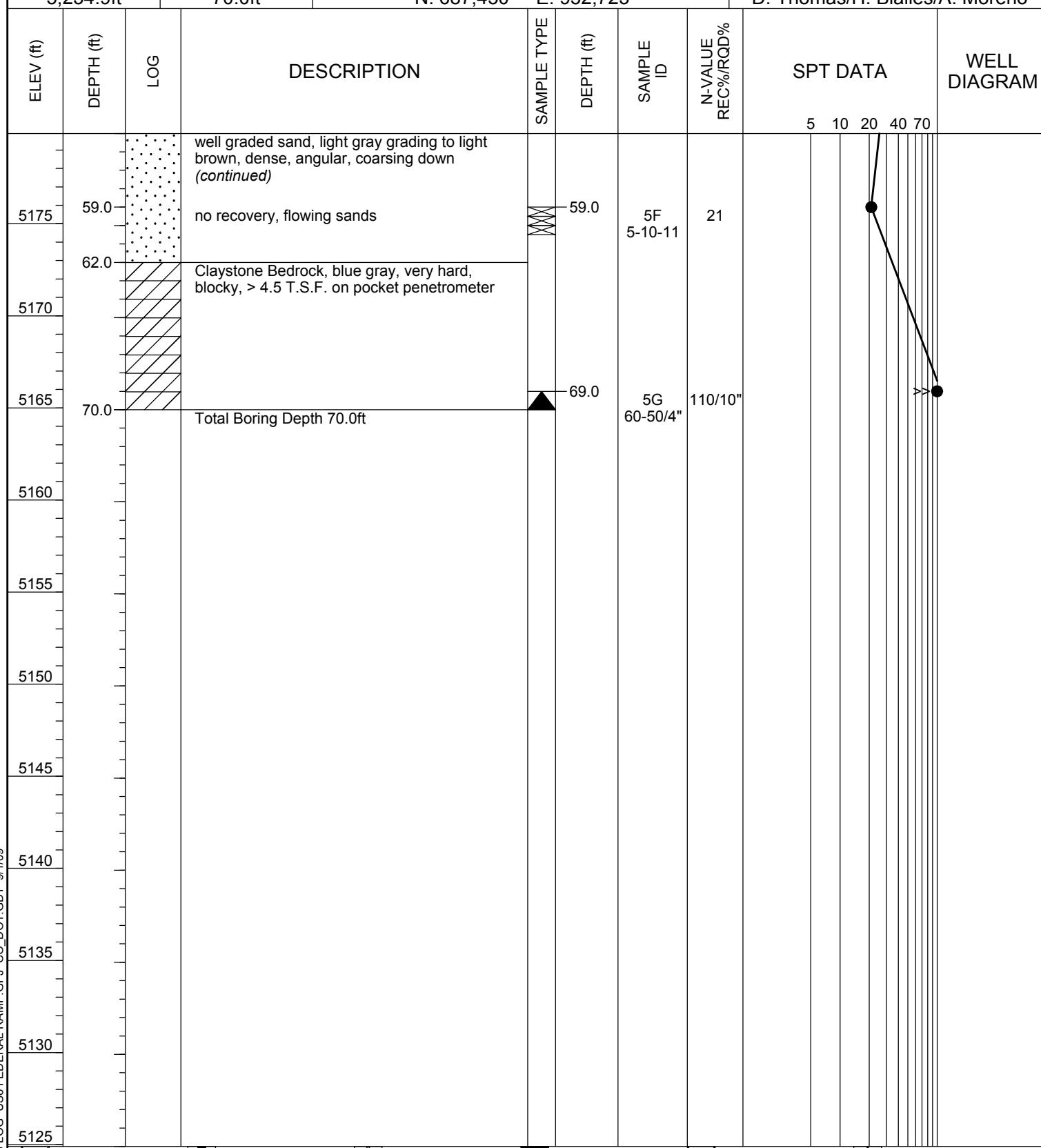
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

5

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/7/09			
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88				
TOP HOLE ELEV 5,234.9ft	TOTAL DEPTH 70.0ft	SURVEY INFO N: 687,450 E: 952,723			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno				



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH

DATE

TIME

NOTES: CME 75, Auger backfilled with cuttings



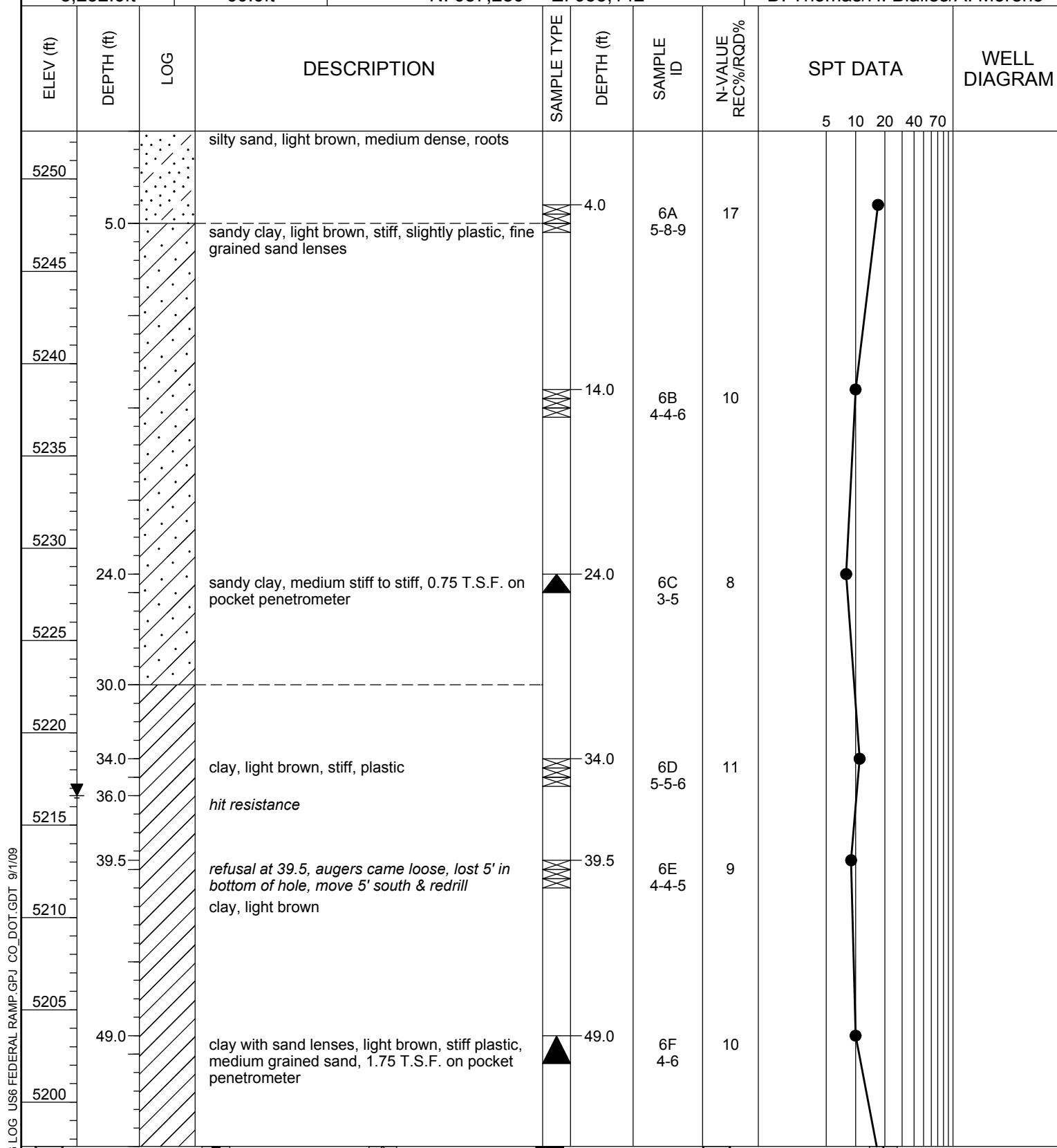
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

6

PROJECT ID			SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/11/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88								
TOP HOLE ELEV 5,252.6ft		TOTAL DEPTH 60.0ft		SURVEY INFO N: 687,280 E: 953,142		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno							
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA			WELL DIAGRAM



	SPT		CON'T		GRAB		SHELBY		CORE		CALIFORNIA
H ₂ O DEPTH	36.0										NOTES: CME 75, Auger
DATE	5/11/09										
TIME											



DEPARTMENT OF TRANSPORTATION

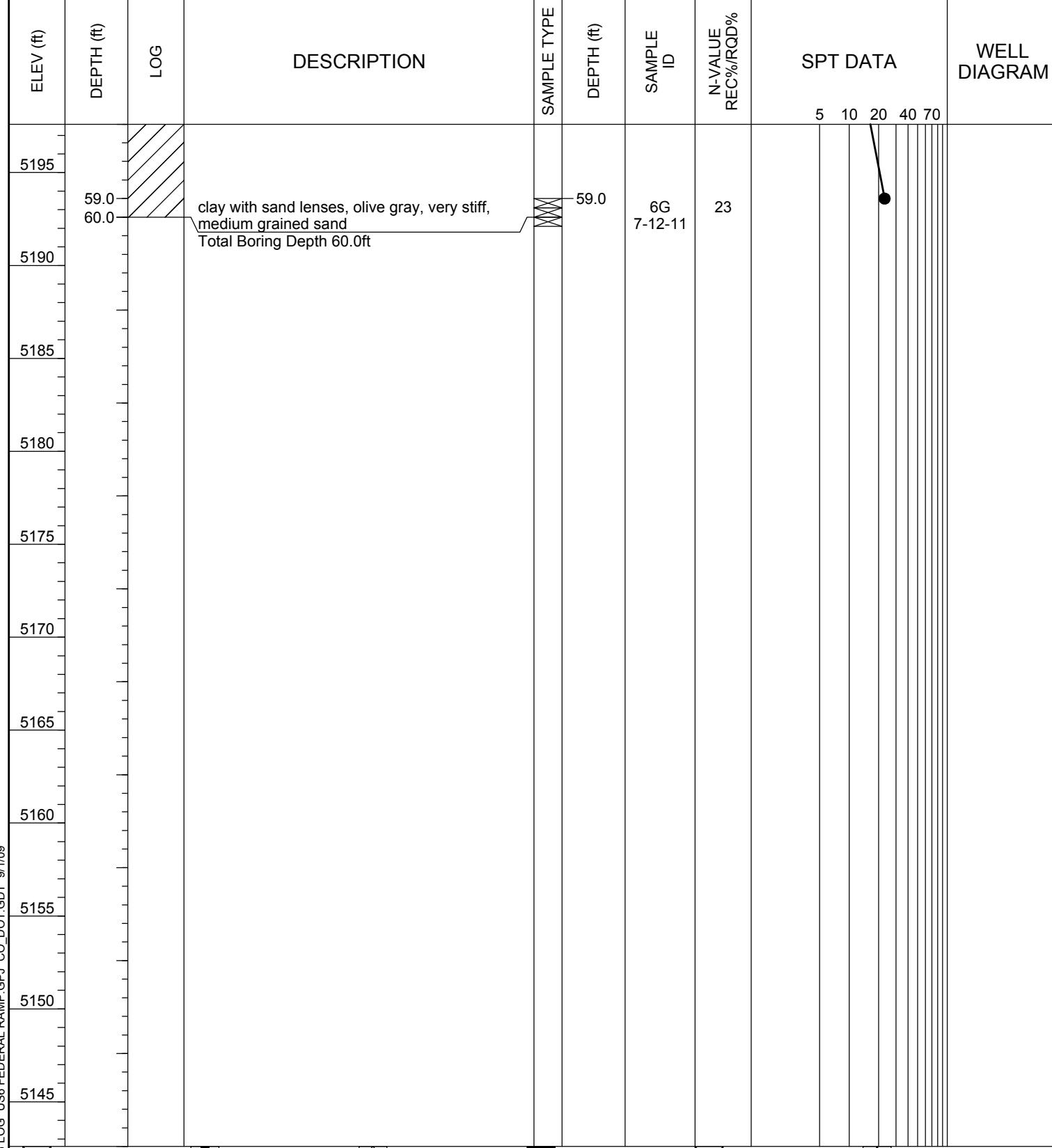
GEOLOGICAL BORING LOG

BORING #

6

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/11/09	
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88		

TOP HOLE ELEV 5,252.6ft	TOTAL DEPTH 60.0ft	SURVEY INFO N: 687,280 E: 953,142	GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno			
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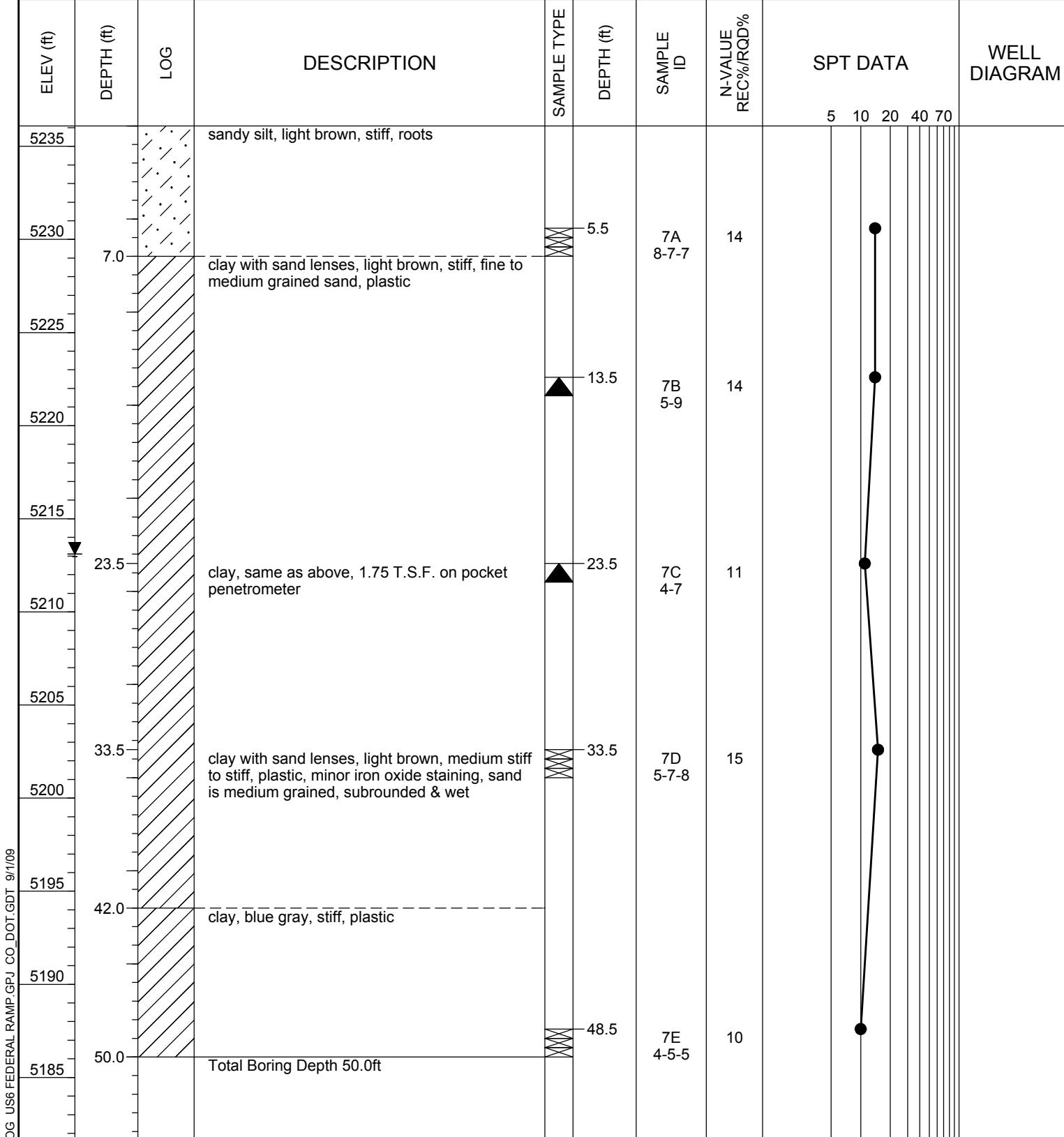
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

7

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/12/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,236.1ft		TOTAL DEPTH 50.0ft		SURVEY INFO N: 687,284 E: 953,263		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM





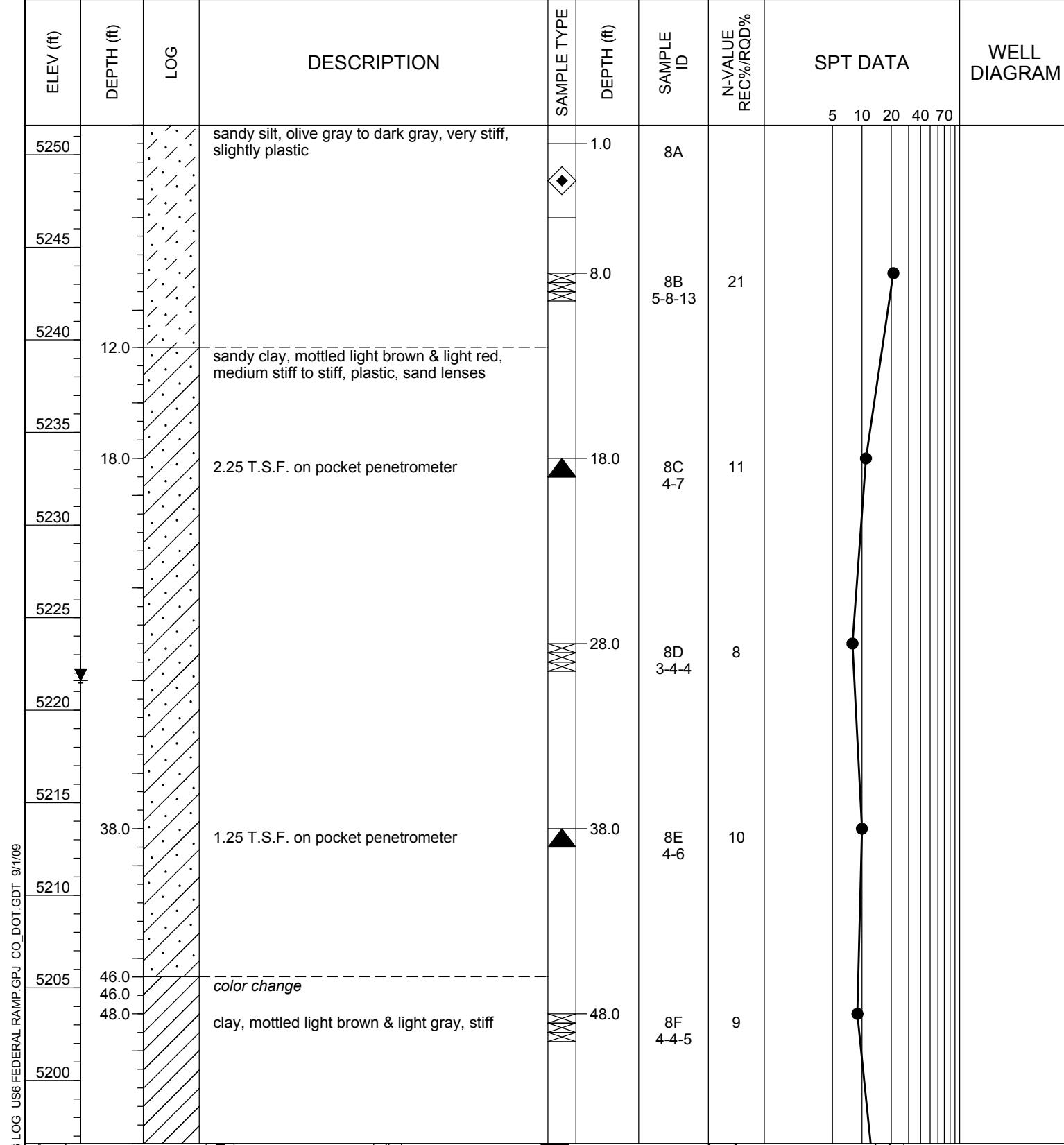
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

8

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/12/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88							
TOP HOLE ELEV 5,251.6ft		TOTAL DEPTH 59.5ft	SURVEY INFO N: 687,330 E: 953,160			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



GEOLOGIC BORING LOG US6 FEDERAL RAMP GPJ CO DOT.GDT 9/1/09

SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 30.0

DATE 5/12/09

TIME

NOTES: CME 75, Auger backfilled with cuttings



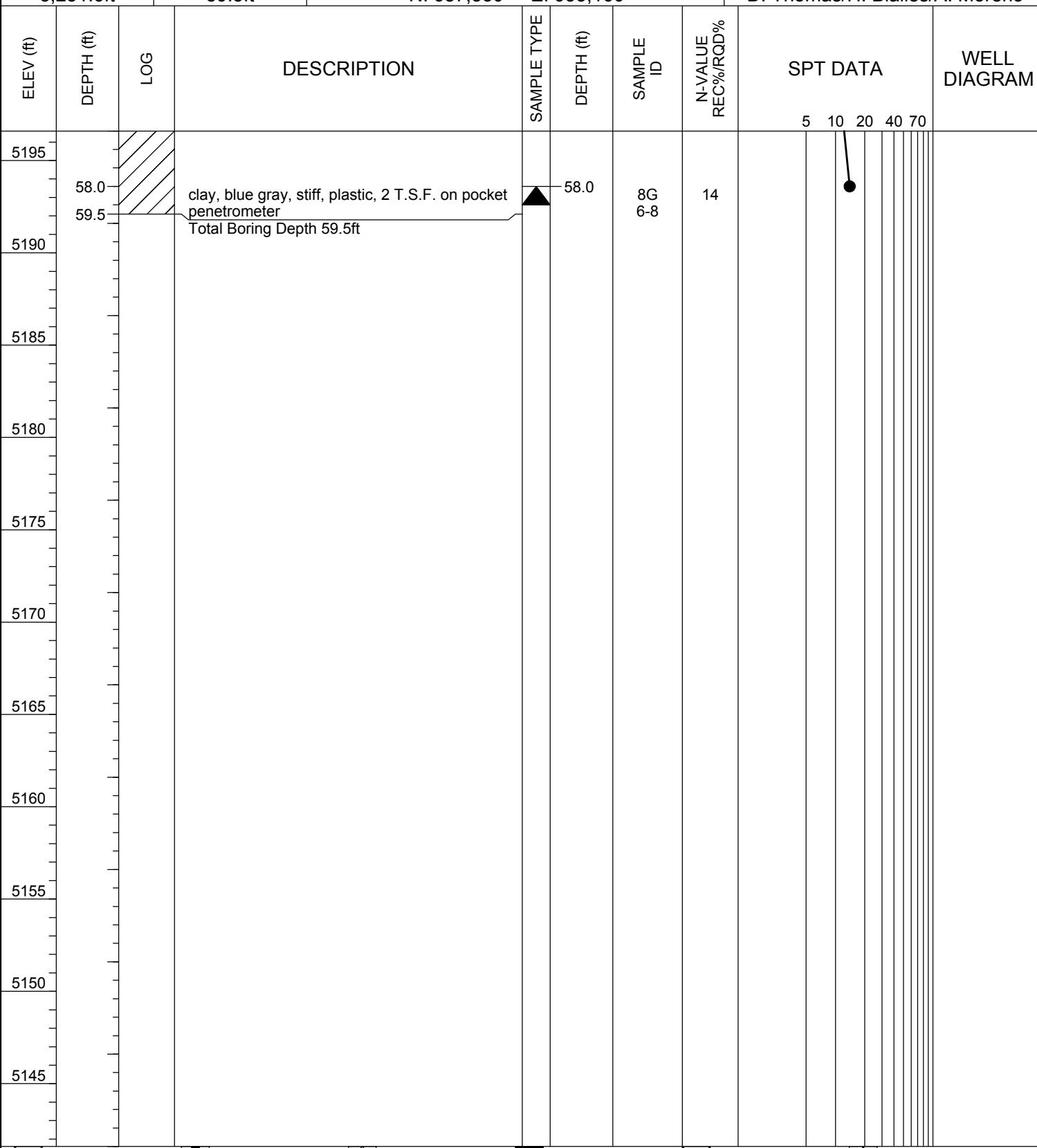
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

8

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/12/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88							
TOP HOLE ELEV 5,251.6ft		TOTAL DEPTH 59.5ft	SURVEY INFO N: 687,330 E: 953,160			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 30.0 NOTES: CME 75, Auger backfilled with cuttings

DATE 5/12/09

TIME



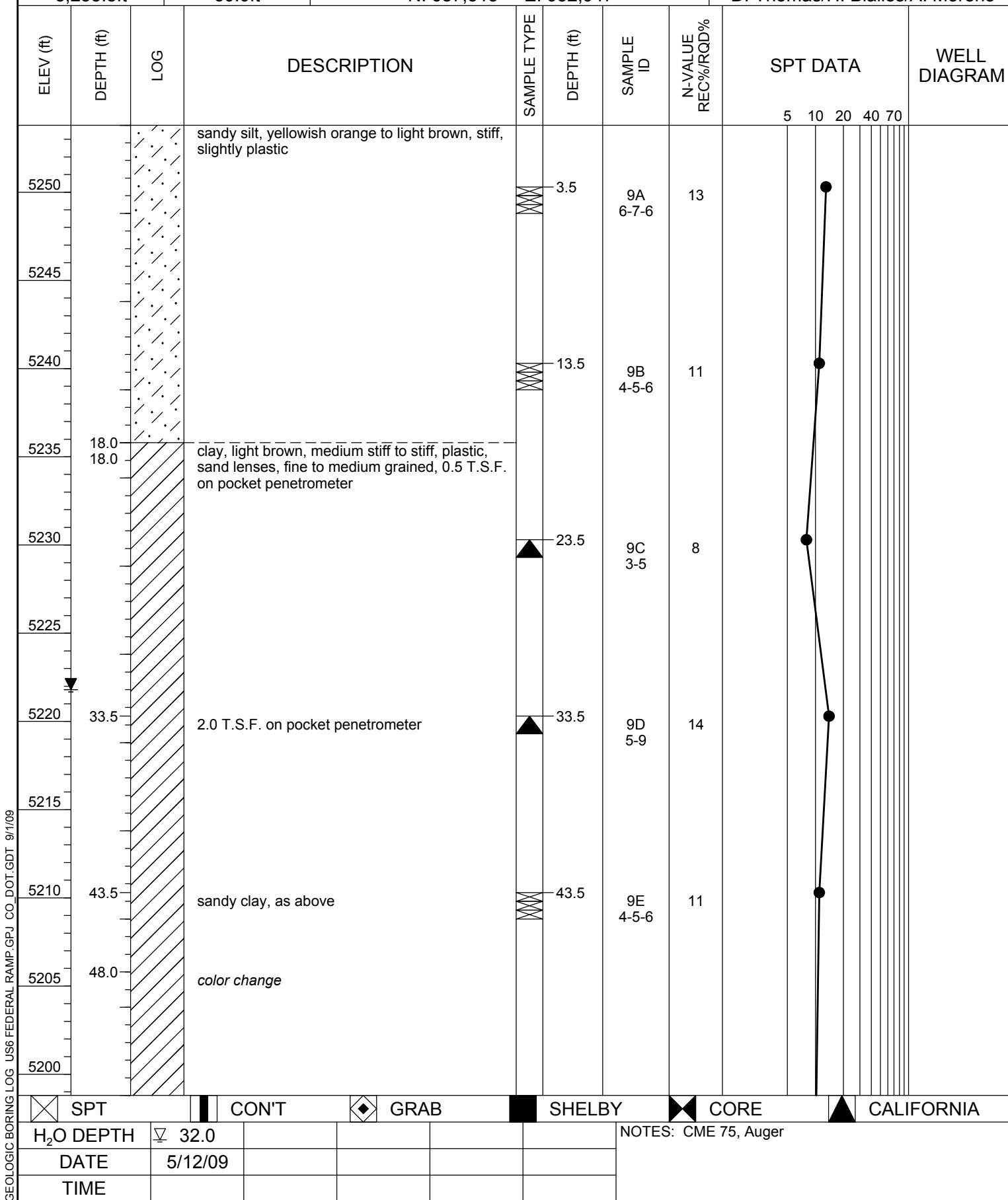
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

9

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/12/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88							
TOP HOLE ELEV 5,253.8ft		TOTAL DEPTH 60.0ft	SURVEY INFO N: 687,315 E: 952,947			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION			SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM





DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

9

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/12/09			
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88				
TOP HOLE ELEV 5,253.8ft	TOTAL DEPTH 60.0ft	SURVEY INFO N: 687,315 E: 952,947			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno				

ELEV (ft)	DEPTH (ft)	LOG	DESCRIPTION	SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM
								5	10	
5195	58.5		clay, blue gray, stiff, plastic		58.5	9F 4-5-5	10		●	
	60.0		Total Boring Depth 60.0ft							
5190										
5185										
5180										
5175										
5170										
5165										
5160										
5155										
5150										
5145										
SPT			CON'T		GRAB		SHELBY		CORE	
H ₂ O DEPTH	32.0							NOTES: CME 75, Auger		
DATE	5/12/09									
TIME										



DEPARTMENT OF TRANSPORTATION

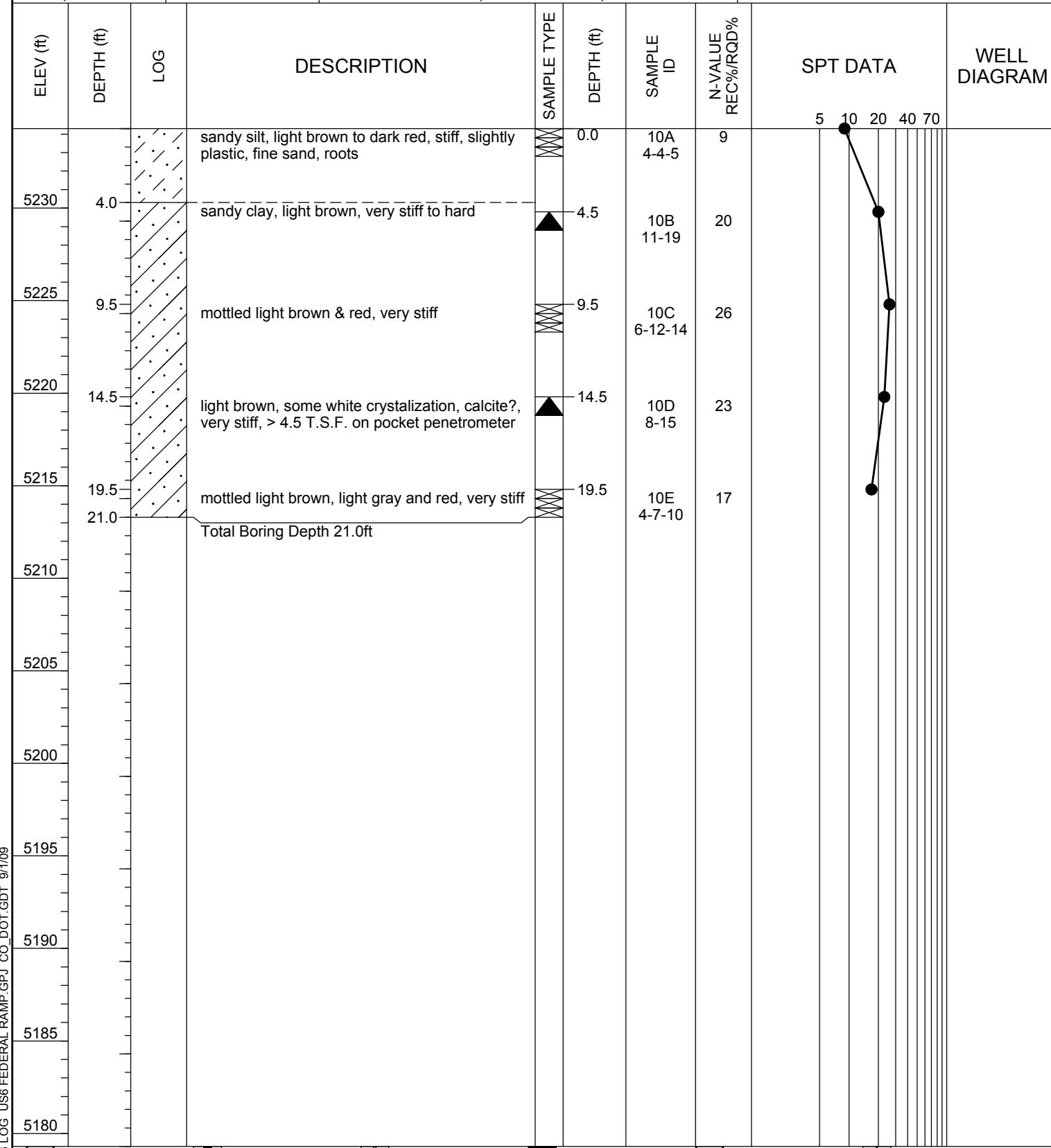
GEOLOGICAL BORING LOG

BORING #

10

PROJECT ID	SA 16628	PROJECT NAME US 6 off ramp to Federal	DATE DRILLED 5/13/09
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ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /	LOCATION at SH 88
TOP HOLE ELEV 5,234.3ft	TOTAL DEPTH 21.0ft	SURVEY INFO N: 687,338 E: 953,374	GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno



GEOLOGIC BORING LOG US6 FEDERAL RAMP GPJ CO DOT.GDT 9/1/09

SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH

DATE

TIME

NOTES: CME 550, Auger backfilled with cuttings



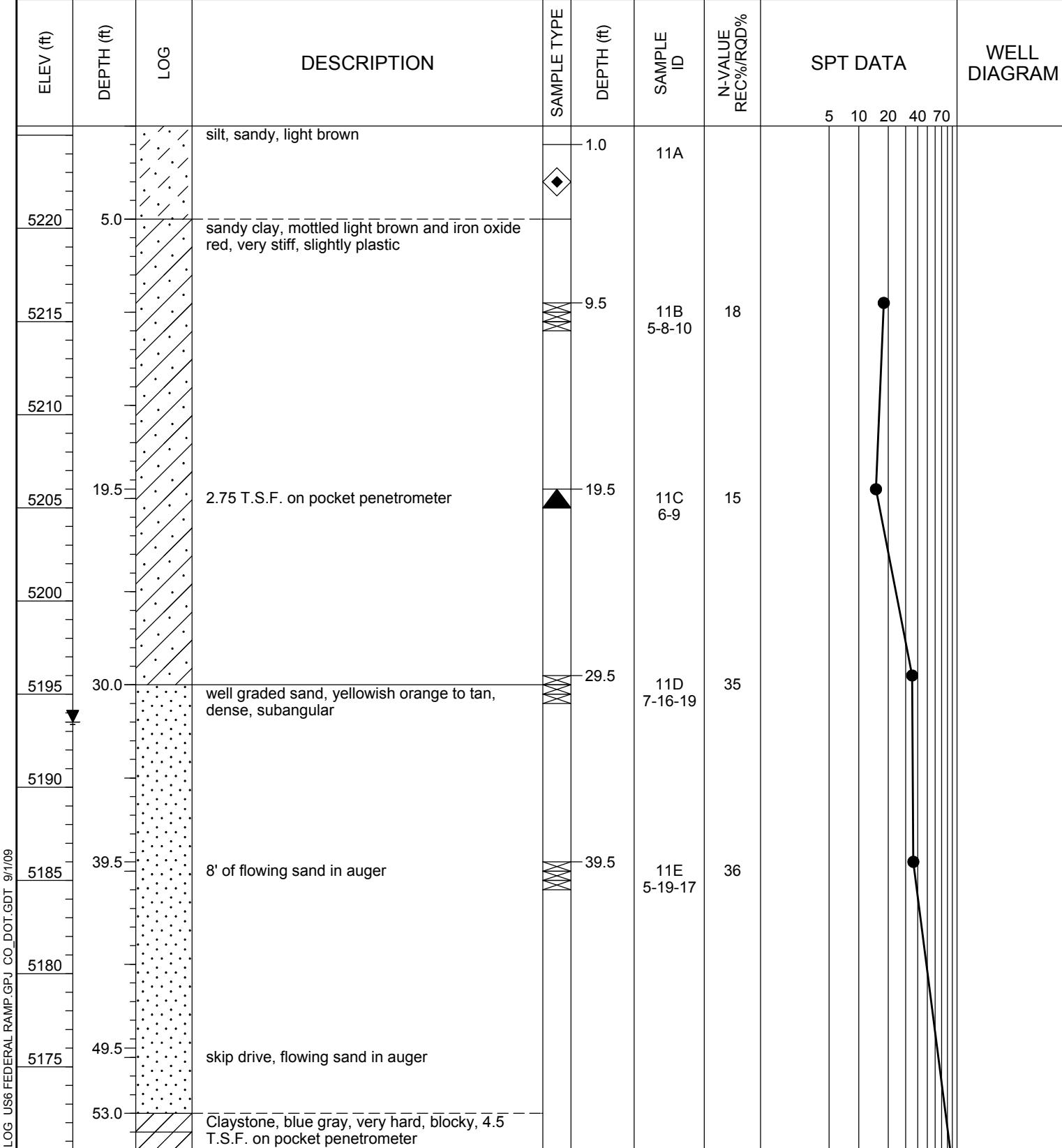
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

11

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/13/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,225.5ft		TOTAL DEPTH 60.0ft		SURVEY INFO N: 687,306 E: 953,563		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM



GEOLOGIC BORING LOG US6 FEDERAL RAMP GPJ CO DOT.GDT 9/1/09

SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 32.0

DATE 5/13/09

TIME

NOTES: CME 550, Auger backfilled with cuttings



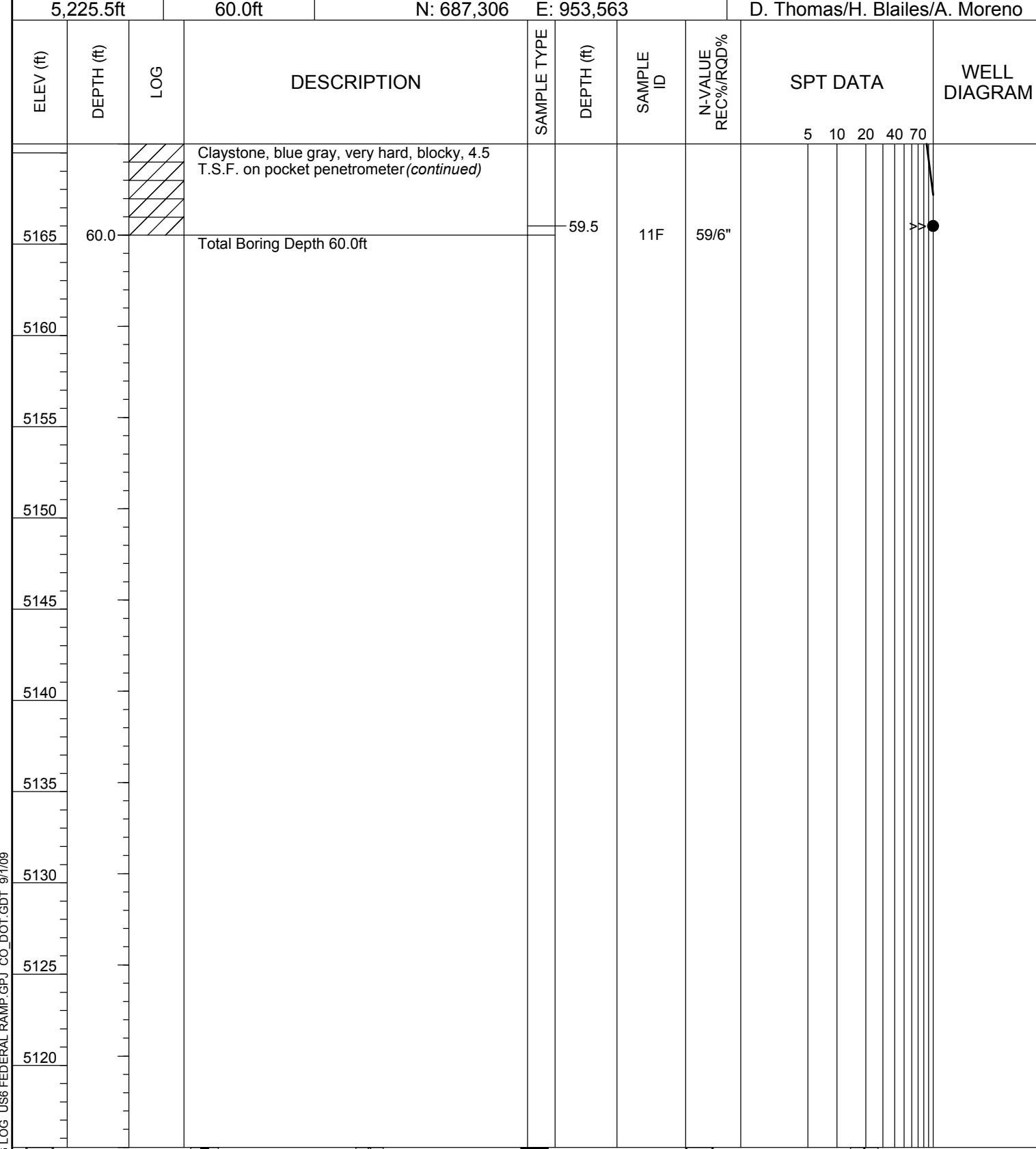
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

11

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/13/09			
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88				
TOP HOLE ELEV 5,225.5ft	TOTAL DEPTH 60.0ft	SURVEY INFO N: 687,306 E: 953,563			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno				



SPT CON'T GRAB SHELBY CORE CALIFORNIA

H₂O DEPTH 32.0

DATE 5/13/09

TIME

NOTES: CME 550, Auger backfilled with cuttings



DEPARTMENT OF TRANSPORTATION

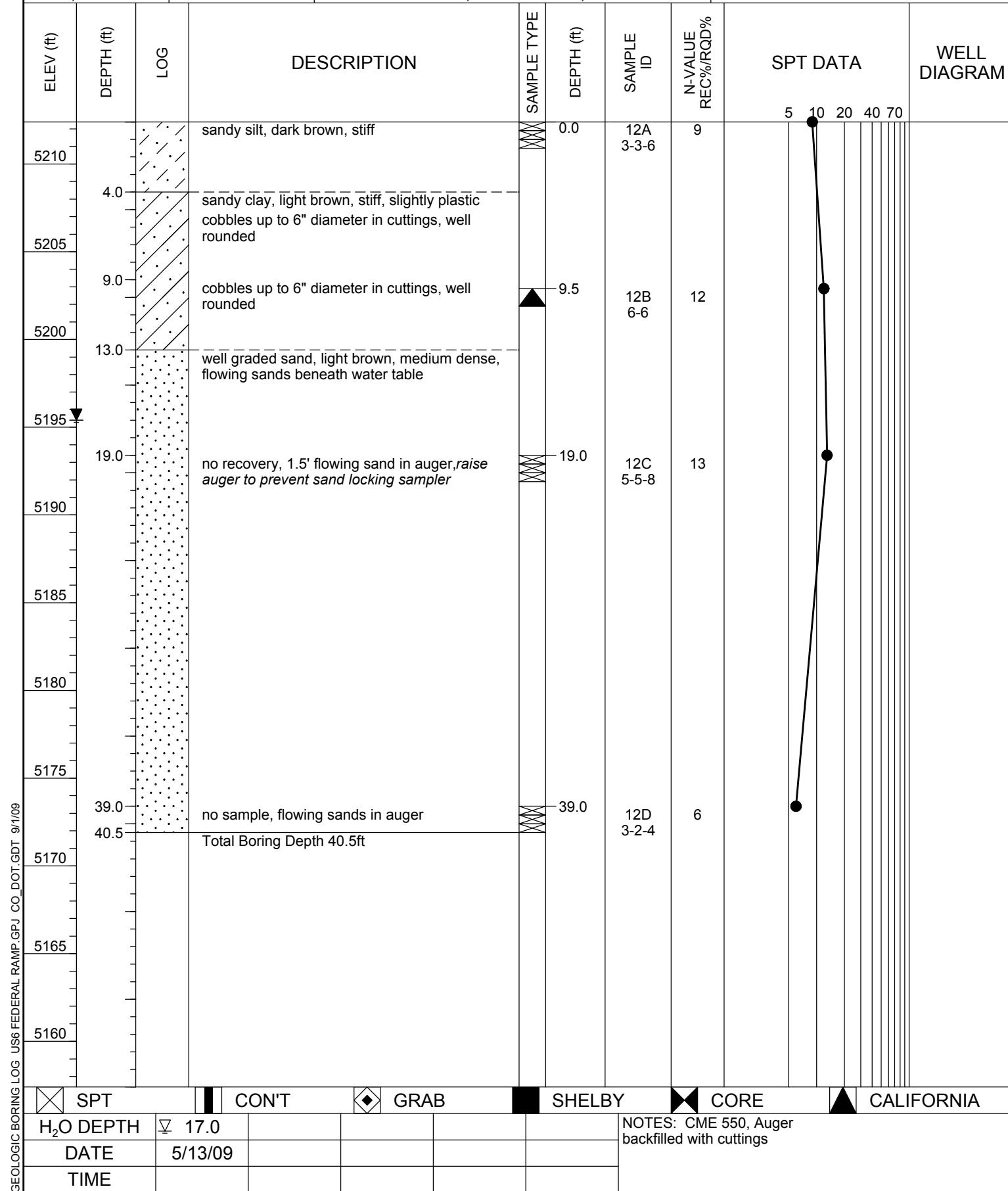
GEOLOGICAL BORING LOG

BORING #

12

PROJECT ID	SA 16628	PROJECT NAME US 6 off ramp to Federal	DATE DRILLED 5/13/09
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ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /	LOCATION at SH 88
TOP HOLE ELEV 5,212.4ft	TOTAL DEPTH 40.5ft	SURVEY INFO N: 687,122 E: 953,596	GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno





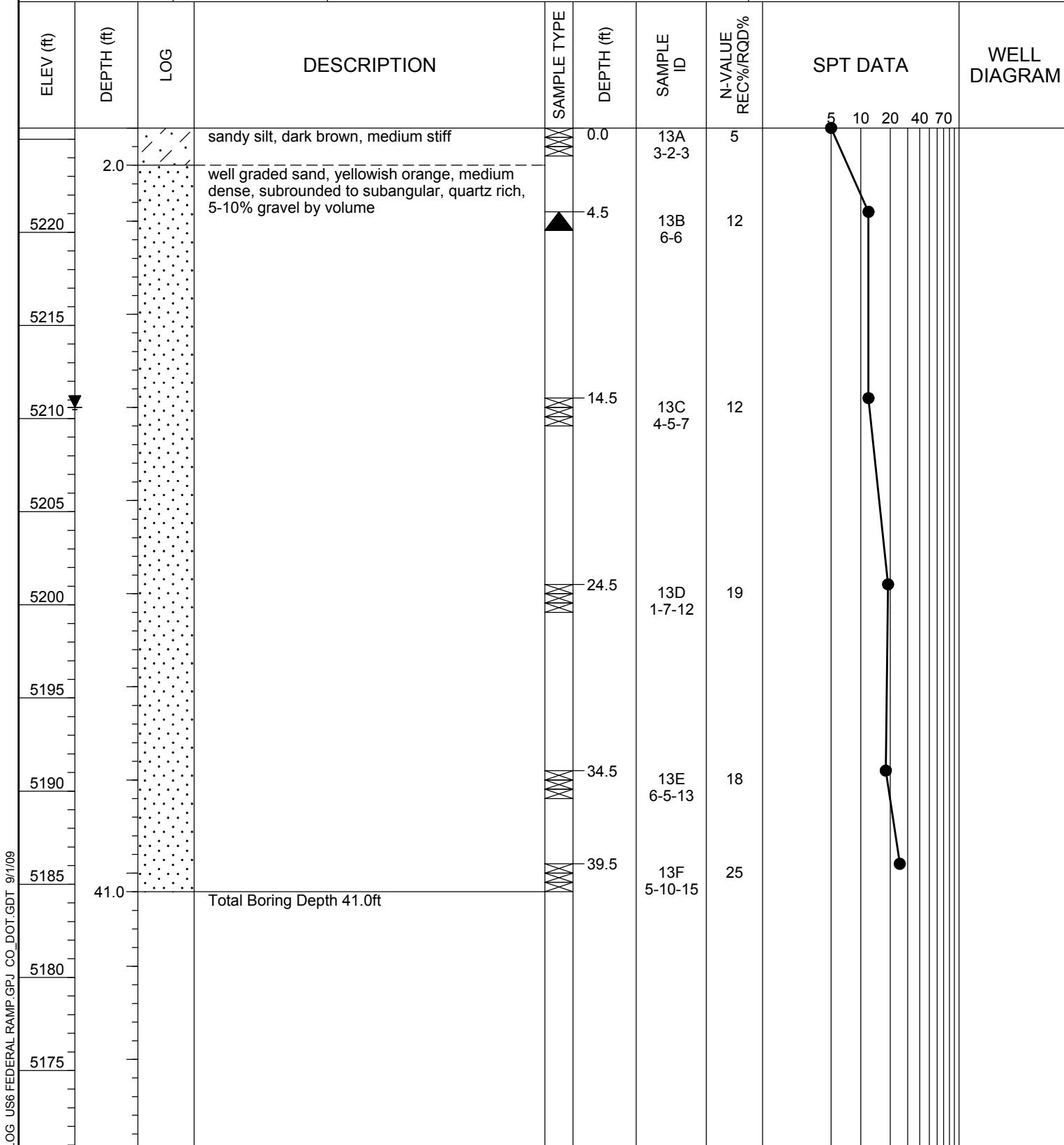
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

13

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/13/09						
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /		LOCATION at SH 88								
TOP HOLE ELEV 5,225.6ft		TOTAL DEPTH 41.0ft		SURVEY INFO N: 686,899 E: 953,596		GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno						
ELEV (ft)	DEPTH (ft)	LOG		DESCRIPTION		SAMPLE TYPE	DEPTH (ft)	SAMPLE ID	N-VALUE REC%/RQD%	SPT DATA		WELL DIAGRAM





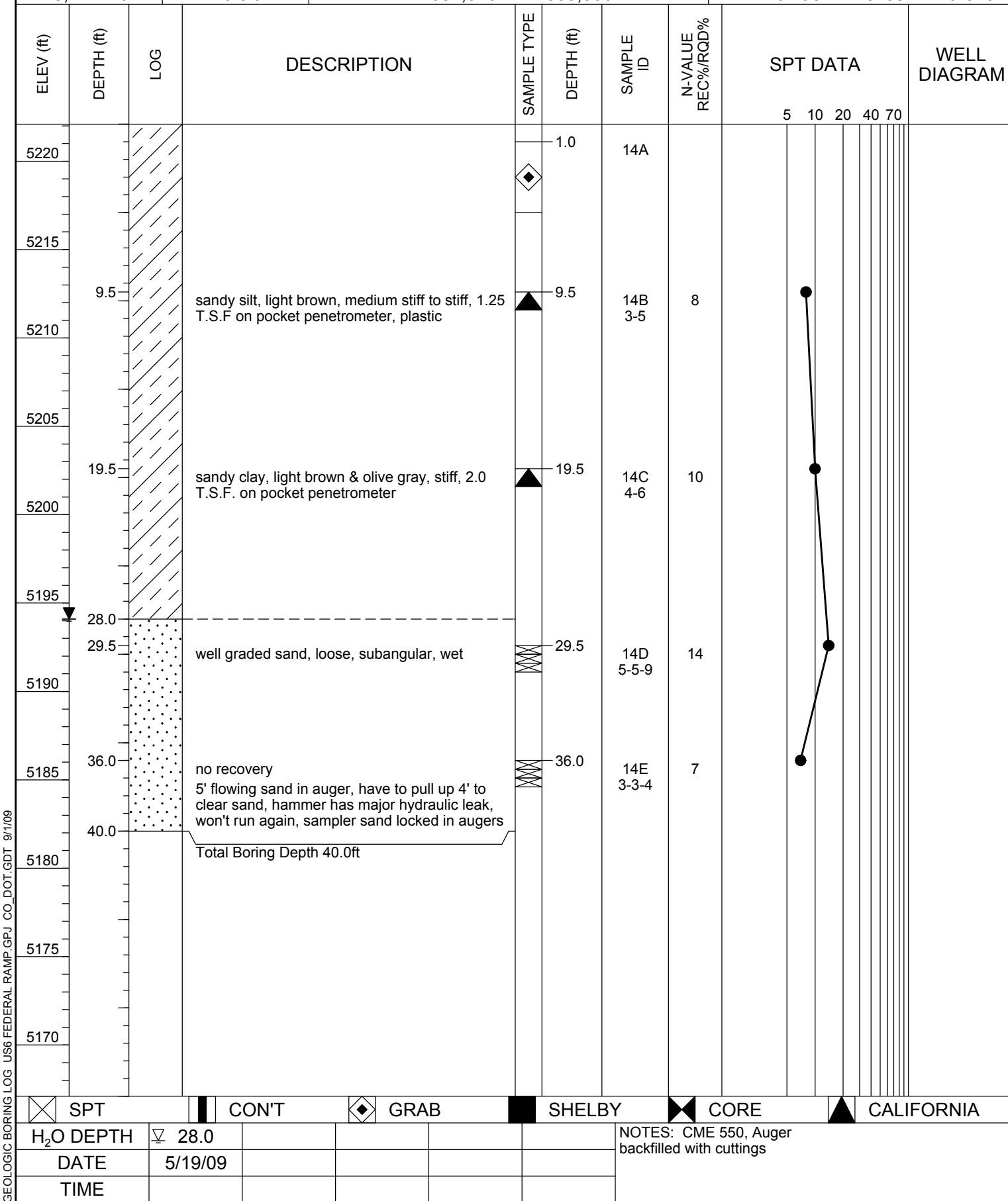
DEPARTMENT OF TRANSPORTATION

GEOLOGICAL BORING LOG

BORING #

14

PROJECT ID			SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/19/09
ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /			LOCATION at SH 88		
TOP HOLE ELEV 5,222.1ft	TOTAL DEPTH 40.0ft	SURVEY INFO N: 687,346 E: 953,806			GEOLOGIST/FOREMAN D. Thomas/H. Blailes/A. Moreno		





DEPARTMENT OF TRANSPORTATION

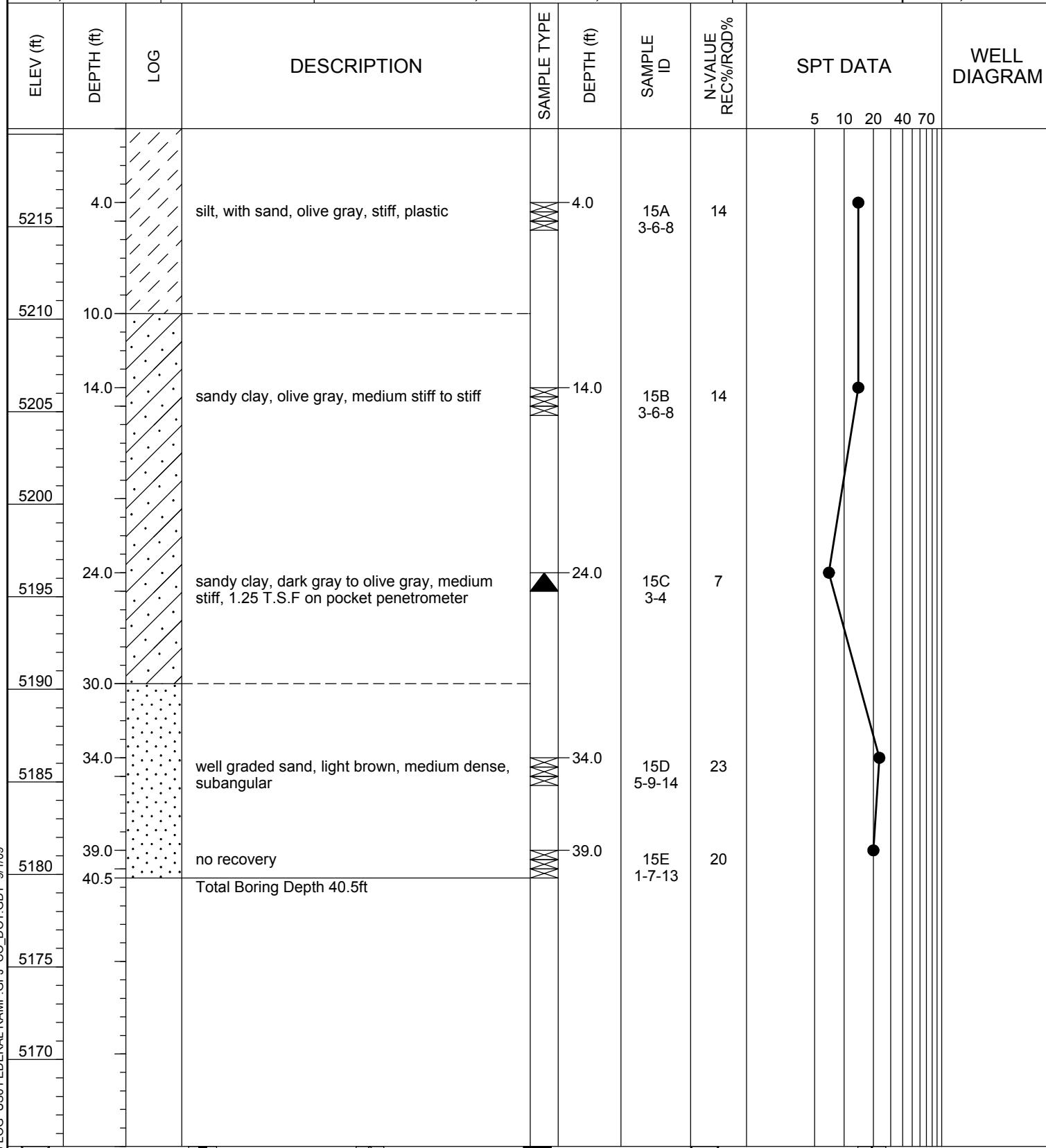
GEOLOGICAL BORING LOG

BORING #

15

PROJECT ID		SA 16628	PROJECT NAME US 6 off ramp to Federal			DATE DRILLED 5/19/09
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ROUTE US 6	COUNTY Denver	STRUCTURE/BENT /	LOCATION at SH 88
TOP HOLE ELEV 5,220.3ft	TOTAL DEPTH 40.5ft	SURVEY INFO N: 687,308 E: 954,006	GEOLOGIST/FOREMAN D. Thomas/P. Spahr/R. Brown



SPT CON'T GRAB SHELBY CORE CALIFORNIA

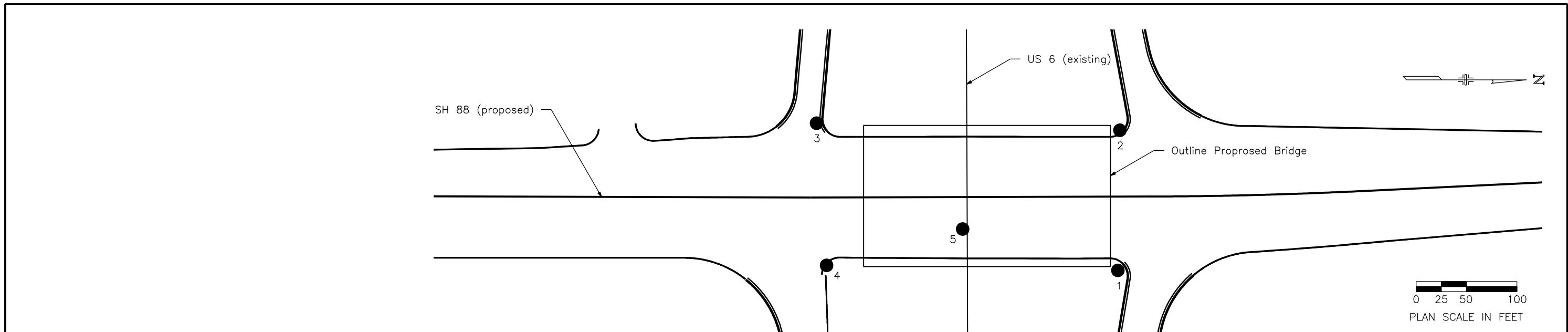
H₂O DEPTH

DATE

TIME

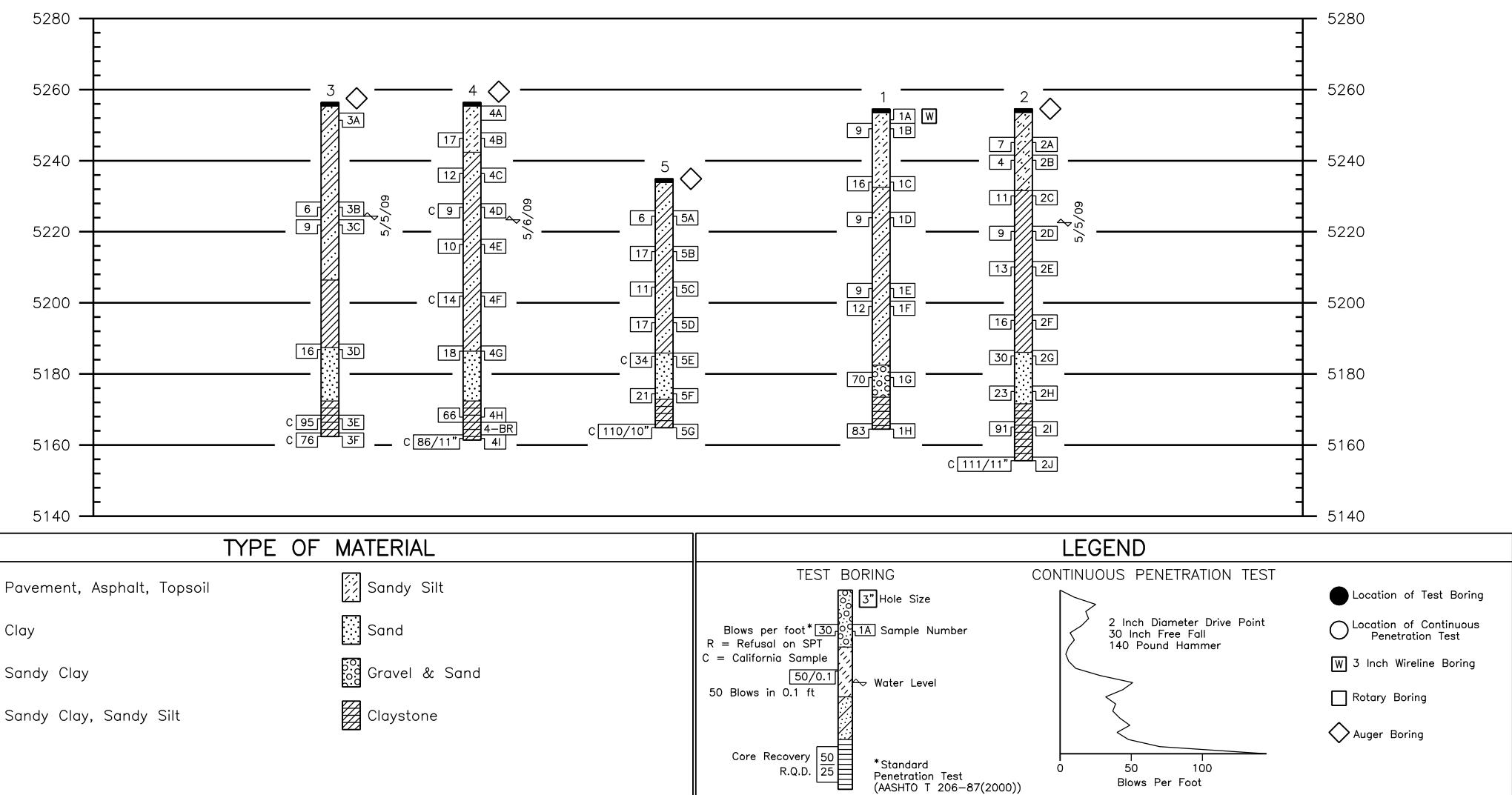
NOTES: CME 75, Auger

ATTACHMENT 2
IM 088A-024, SA 16628, FEDERAL BLVD OVER US-6
GEOLOGY SHEETS

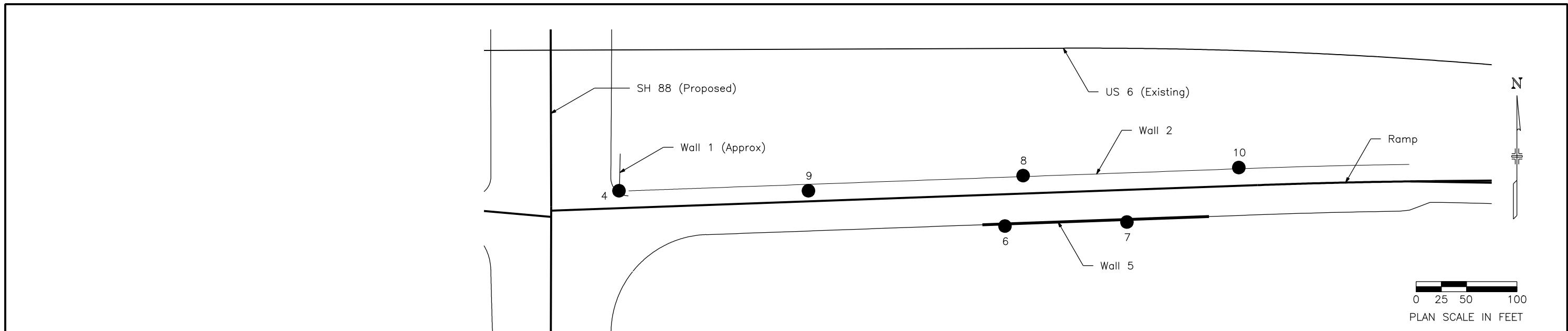


The boring logs of these test holes and geotechnical report are on file in the Geotechnical Program Office, Staff Materials and Geotechnical Branch, (303)398-6601

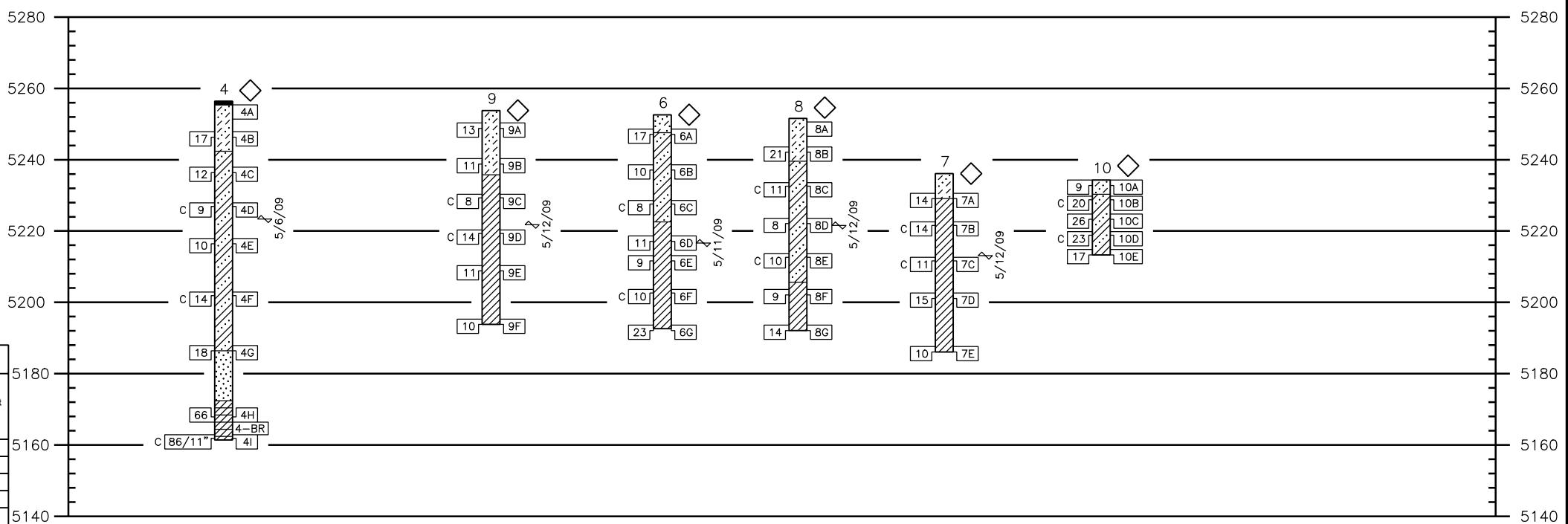
SUMMARY OF TEST RESULTS												
Sample Number	Depth (feet)	Classification			Grading Analysis (AASHTO)			Atterberg Limits			Water Content W %	
		Corps of Engrs. or Visual	USCS	AASHTO	Gravel	Coarse Sand	Fine Sand	Silt and Clay	L.L. L _w	P.L. P _w	P.I. I _w	
1B	4.0	Clay	CL	A-6(9)	4.8	8.6	30.0	56.5	38	16	22	15.6
1C	19.0	Clayey Sand	SC	A-6(1)	9.0	17.5	37.5	35.9	35	19	16	19.8
1G	74.0	Gravel	GW-GC	-	48.3	24.0	18.1	9.6	-	-	-	8.6
2C	23.0	Clay	CL	-	0.0	0.5	10.3	89.1	-	-	-	28.8
2G	68.5	Sand	SW	-	31.4	33.0	31.5	4.1	-	-	-	13.2
2J	98.0	Claystone	CH	A-7-6(30)	0.2	0.0	0.3	99.5	50	24	26	15.2
3C	33.0	Clay	CL	-	0.1	0.9	15.6	83.5	-	-	-	27.2
3F	93.0	Claystone	CL	-	0.0	0.0	0.0	100.0	-	-	-	15.1
4C	18.5	Clayey Sand	SC	-	0.6	12.2	39.3	47.9	-	-	-	19.4
4D	28.5	Clay	CH	A-7-6(31)	0.1	0.6	11.9	87.5	53	19	34	30.1
4F	53.5	Clay	CL	A-6(11)	0.3	4.7	30.5	64.5	40	19	21	28.1
4I	93.5	Claystone	CH	A-7-6(29)	0.0	0.0	0.1	99.9	50	25	25	17.1
4-BR	90.0	Claystone	-	-	-	-	-	-	-	-	-	15.3
5G	69.0	Claystone	CH	A-7-6(40)	0.0	0.0	0.1	99.9	55	19	36	15.3



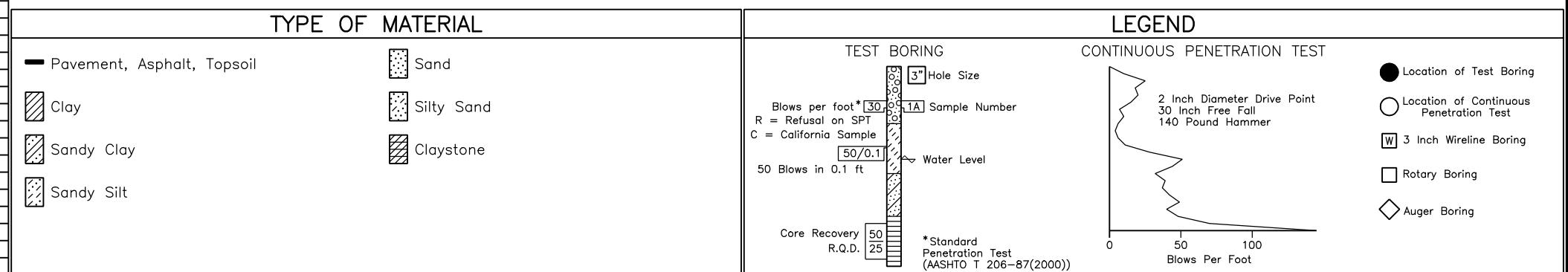
Sheet Revisions			Colorado Department of Transportation			As Constructed			ENGINEERING GEOLOGY			Project No./Code	
Date:	Comments	Init.	4670 Holly Street, Unit A Denver, CO 80216 Phone: 303-398-6601 FAX: 303-398-6504			No Revisions:			D. Thomas			IM 088A-24	
R-X			Staff Geotechnical Program	HCL		Revised:	Designer:	D. Thomas	Structure	Numbers		16628	
000						Void:	Detailer:	T. McNulty					
			Staff Geotechnical Program	HCL			Sheet Subset:	Geology	Subset Sheets:	XXX of XXX	Sheet Number	XXX	



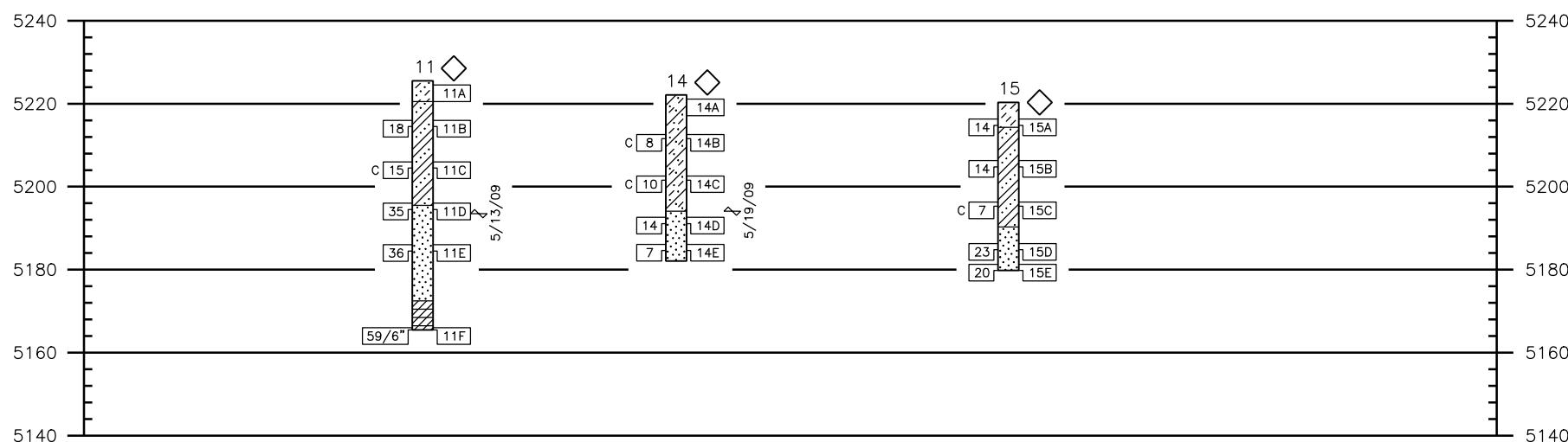
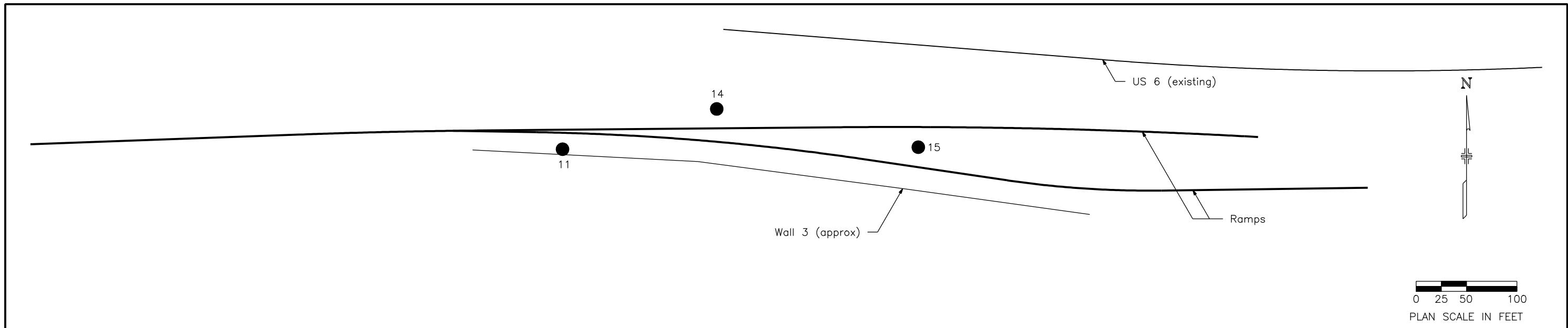
The boring logs of these test holes and geotechnical report are on file in the Geotechnical Program Office, Staff Materials and Geotechnical Branch, (303)398-6601



SUMMARY OF TEST RESULTS												
Sample Number	Depth (feet)	Classification			Grading Analysis (AASHTO)			Atterberg Limits			Water Content %	
		Corps of Engrs. or Visual	USCS	AASHTO	Percent Gravel	Coarse Sand	Fine Sand	Silt and Clay	L.L.	P.L.	I.W.	
4C	18.5	Clayey Sand	SC	—	0.6	12.2	39.3	47.9	—	—	—	19.4
4D	28.5	Clay	CH	A-7-6(31)	0.1	0.6	11.9	87.5	53	19	34	30.1
4F	53.5	Clay	CL	A-6(11)	0.3	4.7	30.5	64.5	40	19	21	28.1
4I	93.5	Claystone	CH	A-7-6(29)	0.0	0.0	0.1	99.9	50	25	25	17.1
4-BR	90.0	Claystone	—	—	—	—	—	—	—	—	—	15.3
6B	15.0	Sandy Clay	CL	A-7-6(11)	3.4	11.2	29.7	55.7	42	16	26	17.9
6C	24.0	Clay	CL	A-6(10)	4.0	5.9	30.8	59.3	40	19	21	28.4
6D	35.0	Clay	CL	—	—	—	—	76.5	—	—	—	26.9
7B	13.5	Clay	CL	A-7-6(17)	0.9	7.5	27.5	64.1	48	18	30	22.7
8C	18.0	Clay	CL	A-7-6(20)	0.0	0.2	18.7	81.1	42	17	25	25.5
8F	48.0	Clay	—	—	—	—	—	73.7	—	—	—	32.1
9C	23.5	Clay	CL	A-7-6(21)	0.0	1.7	13.9	84.4	44	19	25	31.7
9D	33.5	Clay	CL	A-7-6(17)	1.1	8.1	26.9	63.9	47	17	30	22.5
9F	58.5	Clay	CL	—	—	—	—	90.0	—	—	—	36.6
10B	4.5	Clay	CL	—	—	—	—	89.3	—	—	—	17.6
10E	14.5	Clay	—	A-7-6(11)	1.9	11.0	31.9	55.1	45	18	27	21.7

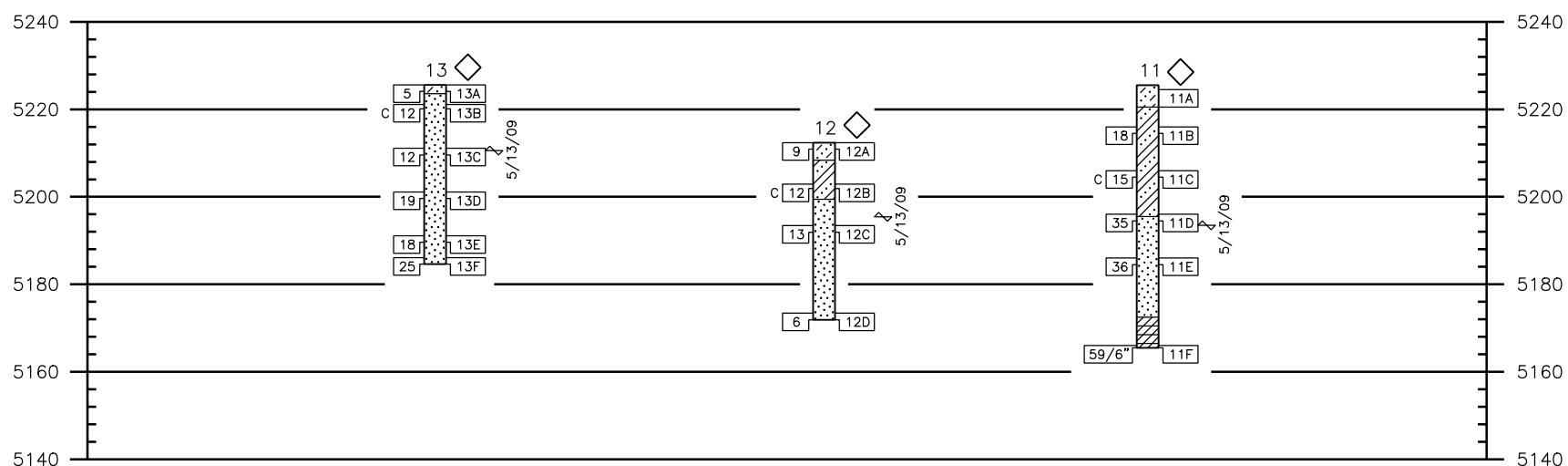
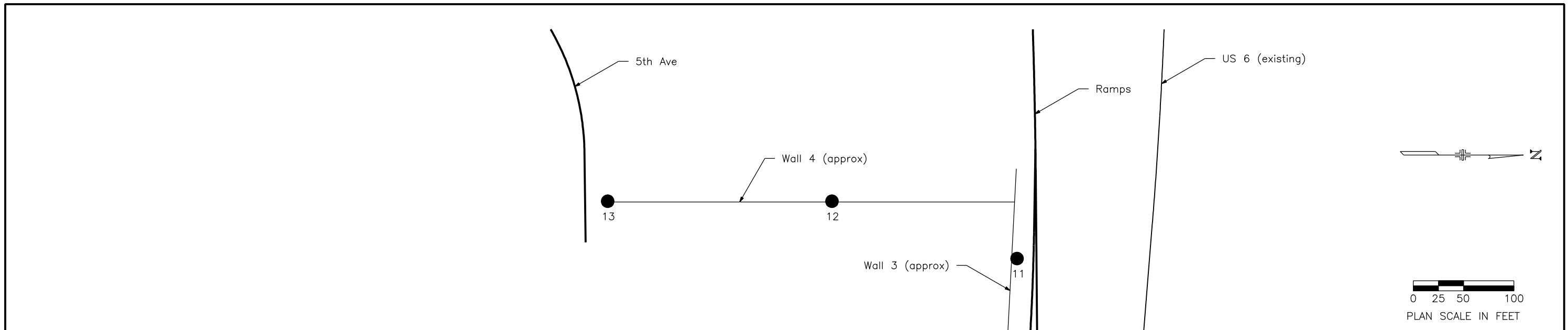


Sheet Revisions			Colorado Department of Transportation			As Constructed			ENGINEERING GEOLOGY			Project No./Code	
Date:	Comments	Init.	4670 Holly Street, Unit A Denver, CO 80216 Phone: 303-398-6601 FAX: 303-398-6504			No Revisions:			D. Thomas			IM 088A-24	
R-X									Revised:	Structure	Walls 1, 2		16628
000									Detailer:	T. McNulty	Numbers	Wall 5	
									Void:	Sheet Subset:	Geology	Subset Sheets:	XXX of XXX
												Sheet Number	XXX



The boring logs of the above test holes and geotechnical report are on file in the Geotechnical Program Office, Staff Materials and Geotechnical Branch, (303)398-6601

SUMMARY OF TEST RESULTS							TYPE OF MATERIAL					LEGEND						
Sample Number	Depth (feet)	Classification			Grading Analysis (AASHTO)		Atterberg Limits			Water Content %	TEST BORING	CONTINUOUS PENETRATION TEST			● Location of Test Boring			
		Corps of Engrs. or Visual	USCS	AASHTO	Percent	Gravel	Coarse Sand	Fine Sand	Silt and Clay			Blows per foot * 30	1A Sample Number	2 Inch Diameter Drive Point 30 Inch Free Fall 140 Pound Hammer				
11C	19.5	Clay	CL	A-7-6(30)	0.0 1.3 14.2	84.5	54	20	34	26.3	Sandy Clay	30	1A	● Location of Test Boring				
11E	39.5	Gravel	GW	—	51.2 33.4 13.6	1.8	—	—	—	10.2		30	1A Sample Number					
14B	9.5	Clay	CL	—	—	—	63.8	—	—	23.2	Sandy Silt	30	1A	● Location of Test Boring				
15C	24.0	Clay	CL	A-7-6(10)	13.8 7.5 23.5	55.2	43	18	25	11.6		30	1A Sample Number					
											TEST BORING			CONTINUOUS PENETRATION TEST				
											3" Hole Size	30	1A Sample Number	● Location of Test Boring	TEST BORING			
											Blows per foot * 30	1A Sample Number	● Location of Test Boring	30	1A Sample Number	● Location of Test Boring		
											R = Refusal on SPT	1A Sample Number	● Location of Test Boring	C = California Sample	30	1A Sample Number	● Location of Test Boring	
											50/0.1	1A Sample Number	● Location of Test Boring	50/0.1	1A Sample Number	● Location of Test Boring		
											50 Blows in 0.1 ft	1A Sample Number	● Location of Test Boring	Water Level	1A Sample Number	● Location of Test Boring		
											Core Recovery 50	1A Sample Number	● Location of Test Boring	R.Q.D. 25	1A Sample Number	● Location of Test Boring		
											* Standard Penetration Test (AASHTO T 206-87(2000))	1A Sample Number	● Location of Test Boring		1A Sample Number	● Location of Test Boring		
												0	50	100	Blows Per Foot	0	50	100
Print Date: 8/24/2009							Sheet Revisions	As Constructed			ENGINEERING GEOLOGY			Project No./Code				
Drawing File Name: I6628geosheet03_wall3.dgn								Date:	Comments	Init.	No Revisions:				IM 088A-24			
Horiz. Scale: 1:100							R-X	As Constructed			ENGINEERING GEOLOGY			Project No./Code				
Vert. Scale: As Noted								Revised:	Designer:	D. Thomas	Structure	Wall 3		16628				
Staff Geotechnical Program							HCL	As Constructed			Detailer:	T. McNulty	Numbers					
HCL								Void:	Sheet Subset:	Geology	Subset Sheets:	XXX of XXX	Sheet Number	XXX				
Colorado Department of Transportation							As Constructed			ENGINEERING GEOLOGY			Project No./Code					
4670 Holly Street, Unit A							As Constructed			ENGINEERING GEOLOGY			Project No./Code					
Denver, CO 80216							As Constructed			As Constructed			IM 088A-24					
Phone: 303-398-6601 FAX: 303-398-6504							As Constructed			As Constructed			IM 088A-24					
Staff Geotechnical Program							As Constructed			As Constructed			IM 088A-24					
HCL							As Constructed			As Constructed			IM 088A-24					



The boring logs of the above test holes and geotechnical report are on file in the Geotechnical Program Office, Staff Materials and Geotechnical Branch, (303)398-6601

SUMMARY OF TEST RESULTS										TYPE OF MATERIAL					LEGEND				
Sample Number	Depth (feet)	Classification			Grading Analysis (AASHTO)			Atterberg Limits			Water Content W %								
		Corps of Engrs. or Visual	USCS	AASHTO	Gravel	Coarse Sand	Fine Sand	Silt and Clay	L.L.	P.L.	P.W.	I.W.							
11C	19.5	Clay	CL	A-7-6(30)	0.0	1.3	14.2	84.5	54	20	34	26.3							
11E	39.5	Gravel	GW	-	51.2	33.4	13.6	1.8	-	-	-	10.2							
12B	9.5	Sandy Clay	CL	A-6(10)	3.2	6.2	25.8	64.7	37	18	19	12.7							
13C	14.5	Sand	SW-SC	-	46.5	40.9	8.4	5.1	-	-	-	2.1							
13F	39.5	Sand	SW	-	37.8	48.7	11.1	2.5	-	-	-	12.7							

TEST BORING

Blows per foot* 30 ft
R = Refusal on SPT
C = California Sample
50/0.1
50 Blows in 0.1 ft

3" Hole Size

1A Sample Number

Water Level

Core Recovery R.Q.D. 50 25

* Standard Penetration Test (AASHTO T 206-87(2000))

CONTINUOUS PENETRATION TEST

2 Inch Diameter Drive Point
30 Inch Free Fall
140 Pound Hammer

0 50 100

Blows Per Foot

Legend:

- Sandy Clay
- Sandy Silt
- Sand
- Claystone
- Location of Test Boring
- Location of Continuous Penetration Test
- 3 Inch Wireline Boring
- Rotary Boring
- Auger Boring

ATTACHMENT 3
IM 088A-024, SA 16628, Federal Blvd over US-6
2007 AASHTO Bridge Design Guidelines

AASHTO Spectrum for 7% PE in 75 years

Latitude = 39.725495

Longitude = -105.025130

Site Class B

Data are based on a 0.05 deg grid spacing.

Period (sec)	Sa (g)	
0.0	0.060	PGA - Site Class B
0.2	0.127	Ss - Site Class B
1.0	0.034	S1 - Site Class B

Map Response Spectra for Site Class B

Latitude = 39.725495

Longitude = -105.025130

Ss and S1 = Mapped Spectral Acceleration Values

Site Class B

Data are based on a 0.05 deg grid spacing.

Period (sec)	Sa (g)	Sd in.	
0.000	0.060	0.000	T = 0.0, Sa = PGA
0.054	0.127	0.004	T = To, Sa = Ss
0.200	0.127	0.050	T = 0.2, Sa = Ss
0.268	0.127	0.089	T = Ts, Sa = Ss
0.300	0.113	0.100	
0.400	0.085	0.133	
0.600	0.057	0.199	
0.800	0.042	0.266	
1.000	0.034	0.332	T = 1.0, Sa = S1
1.200	0.028	0.398	
1.400	0.024	0.465	
1.600	0.021	0.531	
1.800	0.019	0.598	
2.000	0.017	0.664	
2.200	0.015	0.730	
2.400	0.014	0.797	
2.600	0.013	0.863	
2.800	0.012	0.930	
3.000	0.011	0.996	
3.200	0.011	1.063	
3.400	0.010	1.129	
3.600	0.009	1.195	
3.800	0.009	1.262	
4.000	0.008	1.328	

Spectral Response Accelerations SDs and SD1

Latitude = 39.725495

Longitude = -105.025130

As = FpgaPGA, SDs = FaSs, and SD1 = FvS1

Site Class E - Fpga = 2.50, Fa = 2.50, Fv = 3.50

Data are based on a 0.05 deg grid spacing.

Period (sec)	Sa (g)	
0.0	0.149	As - Site Class E
0.2	0.317	SDs - Site Class E
1.0	0.119	SD1 - Site Class E

Design Response Spectra for Site Class E

Latitude = 39.725495

Longitude = -105.025130

As = FpgaPGA, SDs = FaSs, SD1 = FvS1

Site Class E - Fpga = 2.50, Fa = 2.50, Fv = 3.50

Data are based on a 0.05 deg grid spacing.

Period (sec)	Sa (g)	Sd in.	
0.000	0.149	0.000	T = 0.0, Sa = As
0.075	0.317	0.017	
0.200	0.317	0.124	T = 0.2, Sa = SDs
0.375	0.317	0.436	T = Ts, Sa = SDs
0.400	0.297	0.465	
0.600	0.198	0.697	
0.800	0.149	0.930	
1.000	0.119	1.162	T = 1.0, Sa = SD1
1.200	0.099	1.395	
1.400	0.085	1.627	
1.600	0.074	1.859	
1.800	0.066	2.092	
2.000	0.059	2.324	
2.200	0.054	2.557	
2.400	0.050	2.789	
2.600	0.046	3.022	
2.800	0.042	3.254	
3.000	0.040	3.486	
3.200	0.037	3.719	
3.400	0.035	3.951	
3.600	0.033	4.184	
3.800	0.031	4.416	
4.000	0.030	4.649	